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A Mathematical Simulation Model of a CH-47B Helicopter

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SUMMARY

A nonlinear simulation model of the CH-47B helicopter, developed by the Boeing Vertol Company (ref. 1), has been adapted for use in the NASA Ames Research Center (ARC) simulation facility. The model represents the specific configuration of the ARC variable stability CH-47B helicopter (fig. 1) and will be used in ground simulation research and to expedite and verify flight experiment design.

Modeling of the helicopter uses a total force approach in six rigid body degrees of freedom. Rotor dynamics are simulated using the Wheatley-Bailey equations, including steady-state flapping dynamics. Also included in the model is the option for simulation of external suspension, slung-load equations of motion.

Validation of the model (discussed in volume II of this report) has been accomplished using static and dynamic data from the original Boeing Vertol mathematical model and flight test data from references 2 and 3, as reproduced in reference 4. The model is appropriate for use in real-time piloted simulation and is implemented on the ARC Sigma IX computer where it may be operated with a digital cycle time of 0.03 sec.

NOMENCLATURE

ARC Ames Research Center

BV Boeing Vertol Company

c.g. center of gravity

rpm revolutions per minute

SAS stability augmentation system

INTRODUCTION

Volume II of this report contains static trim data, stability and control derivatives, and dynamic response data for the CH-47B mathematical model described in volume I. Validation of the helicopter itself (without the slung load) was highly successful for all flight conditions examined. Slung load validation was also successful with one exception. The Ames Research Center (ARC) model dynamic response of the slung-load lateral-differential cable angle, ν_L , was unlike the response of the Boeing Vertol Company (BV) model in terms of initial amplitude and damping ratio. Although it was possible to artificially modify the damping of this mode to obtain a good match at most flight conditions (as discussed in the volume I slung-load subroutine description), there is currently a mismatch in initial amplitude, presumably a result of computational differences between the ARC and BV simulation facilities.

Tables 1 through 7 provide a table of contents for the extensive validation data given in tables 8 through 45 and in figures 1 through 110.

Specifically, tables 1 and 2 give the flight conditions corresponding to the helicopter (no slung load) static trim and stability derivative data, respectively. Only ARC model static trim (tables 8-33) and stability derivative (tables 34-41) data are included in this report. During model validation, each number was compared with corresponding BV data and was found to be satisfactory.

The static trim data given in this report were produced with the CH-47B trim-sheet subroutine by selecting flag ICPRNT. Table 3 gives the static trim-sheet key in terms of math model mnemonics.

Table 4 gives the flight conditions corresponding to the dynamic response data given in figures 1-80. For each flight condition, the model was excited with a 1.0 sec pulse in each of the four control axes. Referring to the table, each response consists of four figures, illustrating kinematic, engine, and stability-augmentation-system (SAS) details of the model. Each figure provides a comparison between BV and ARC model responses, SAS on, and SAS off ARC model response.

Next, in figures 81-86, BV simulation model responses are compared with CH-47B and CH-47C flight test data from references 2 and 3, respectively. (The data extracted from ref. 3 are from a CH-47C helicopter with a CH-47B SAS, making the dynamic response data comparable with that of a CH-47B.) These comparisons were originally made in reference 4, and are reproduced for this report. Flight condition details for each of these comparison figures may be found in table 5.

Tables 6 and 7 give the flight conditions for static trim (tables 42-45) and dynamic response data (figs. 87-110) for the helicopter with the slung load attached.

REFERENCES

1. Cogan, C.; Gajkowski, B. J.; and Garnett, Jr., T. S.: Full Flight Envelope Math Model for 347/HLH Control System Analysis - Control Document. Boeing Company, Vertol Division, report D301-10148-1, 1972.
2. Yamakawa, G.; and Miller, L. G.: Airworthiness and Qualification Test, Phase D, CH-47B. USAASTA #66-23, 1970.
3. Albion, N.; Leet, J. R.; and Mollenkof, A.: Ground Based Flight Simulation of CH-47C Helicopter. Boeing Company, Vertol Division, report D8-2418-1, 1969.
4. Hackett, W. E.; Garnett, T. S.; and Borek, B. V.: Mathematical Model of the CH-47B Helicopter Capable of Real Time Simulation of the Full Flight Envelope. NASA CR-166458, 1983.

TABLE 1.- ARC MODEL STATIC TRIM DATA: FLIGHT CONDITIONS

Table number	Gross weight, lb	Moments and products of inertia, slug-ft ²	$\Delta X_{c.g.}$, (DXCG), in.	SAS configuration	Equivalent airspeed, knot	Flight condition
8	33,000	Nominal: $I_{xx} = 34,000$ $I_{yy} = 202,500$ $I_{zz} = 191,000$ $I_{xz} = 14,900$ $I_{xy} = I_{yz} = 0$	0.	OFF	0.1 (Hover)	Straight and level
9		Nominal		ON	.1 (Hover)	
10				OFF	20	
11				ON	20	
12				OFF	40	
13				ON	40	
14				OFF	60	
15				ON	60	
16				OFF	80	
17				ON	80	
18				OFF	100	
19				ON	100	
20				OFF	120	
21				ON	120	
22				OFF	130	
23				ON	130	
24			21.	ON	.1	
25			21.		80	
26			0.		80	Wings level, 1000 ft/min rate of climb
27					80	Wings level, 1000 ft/min rate of descent
28					75	Level flight, $\beta = +15^\circ$
29					75	Level flight, $\beta = -15^\circ$

TABLE 1.- CONCLUDED

Table number	Gross weight, lb	Moments and products of inertia, slug-ft ²	$\Delta X_{c.g.}$ (DXCG), in.	SAS configuration	Equivalent airspeed, knot	Flight condition
30	33,000	Nominal	0.	ON	75	Coordinated level turn, $\phi = +30^\circ$
31					75	Coordinated level turn, $\phi = -30^\circ$
32	22,000	$I_{xx} = 18,000$ $I_{yy} = 168,000$ $I_{zz} = 160,000$ $I_{xz} = 11,600$ $I_{yz} = I_{xy} = 0$.1	Straight and level
33	22,000	$I_{xx} = 18,000$ $I_{yy} = 168,000$ $I_{zz} = 160,000$ $I_{xz} = 11,600$ $I_{yz} = I_{xy} = 0$			80	Straight and level

TABLE 2.- ARC MODEL STABILITY-
AND CONTROL-DERIVATIVE DATA:
FLIGHT CONDITIONS.

Straight and level Gross weight = 33,000 lb $I_{xx} = 34,000 \text{ slug}\cdot\text{ft}^2$ $I_{yy} = 202,500 \text{ slug}\cdot\text{ft}^2$ $I_{zz} = 191,000 \text{ slug}\cdot\text{ft}^2$ $I_{xz} = 14,900 \text{ slug}\cdot\text{ft}^2$ $I_{xy} = I_{yz} = 0$ $\Delta X_{c.g.} = 0$																			
Perturbation step size: $\delta_B, \delta_A, \delta_R, \delta_C: -0.5 \text{ in.}$ $p, q, r: -.2 \text{ rad/sec}$ $u, v, w: -10 \text{ ft/sec}$																			
<table border="1"> <thead> <tr> <th>Table number</th> <th>Equivalent airspeed, knots</th> </tr> </thead> <tbody> <tr> <td>34</td> <td>0.1</td> </tr> <tr> <td>35</td> <td>20.</td> </tr> <tr> <td>36</td> <td>40.</td> </tr> <tr> <td>37</td> <td>60.</td> </tr> <tr> <td>38</td> <td>80.</td> </tr> <tr> <td>39</td> <td>100.</td> </tr> <tr> <td>40</td> <td>120.</td> </tr> <tr> <td>41</td> <td>130.</td> </tr> </tbody> </table>		Table number	Equivalent airspeed, knots	34	0.1	35	20.	36	40.	37	60.	38	80.	39	100.	40	120.	41	130.
Table number	Equivalent airspeed, knots																		
34	0.1																		
35	20.																		
36	40.																		
37	60.																		
38	80.																		
39	100.																		
40	120.																		
41	130.																		

TABLE 3.- CH-47B SIMULATION MODEL TRIM SHEET KEY

VTOT VTOTAL	U		V		W			
	UB		VB		WB		DZCG DZCG	
G.W. WAIT	RPM OMEGA	H ALT	TEMP TAMB		DXCG DXCG		DZCG DZCG	
THETA THET	PHI PHI	PSI PSI	P PB	Q QB	R RB	RHO RHO	OMEGA FR OMEGFR	OMEGA RR OMEGRR
DELB PLT DLONP	DELS PLT DLATP	DELR PLT DYAWP	DELC PLT DCOLP	DELB TOT DLONTOT	DELS TOT DLATTOT	DELR TOT DYAWTOT	DELC TOT DCOLTOT	H DOT ALTD
THETO FR 57.3×THOFR	AICFR 57.3×AICFR	BICFR 57.3×BICFR	THETO RR 57.3×THORR	IXX XIXX	IYY XIYY	IZZ XIZZ	IXZ XIXZ	D. PRES F QBAR
SIGMA FR SIGFR	SIGMA RR SIGRR	GAMMA FS GAMSFR		LAMDA FR ALAMFR	LAMDA RR ALAMRR	MU FR AMUFR	MU RR AMURR	MACH NO. XMACH
THRUST F TFR	NORMAL F HFR	SIDE F YFR	TORQUE F QAERFR	L HUB FR ALHBFR	M HUB FR AMHBFR	V TIP FR VTIPFR	DELTA FR DELFR	F FR FFR
THRUST R TRR	NORMAL R HRR	SIDE R YRR	TORQUE R QAERRR	L HUB RR ALHBRR	M HUB RR AMHBRR	V TIP RR VTIPRR	DELTA RR DELRR	FRR FRR
CT FR CTFR	CH FR CHFR	CY FR CYFR	CQ FR CQFR	A0 FR 57.3×A0FR	A1 FR 57.3×A1FR	B1 FR 57.3×B1FR	Q GOV FR QGOVFR	
CT RR CTRR	CH RR CHRR	CY RR CYRR	CQ RR CQRR	A0 RR 57.3×A0RR	A1 RR 57.3×A1RR	B1 RR 57.3×B1RR	Q GOV RR QCOVRR	
X FUSE XAERFS	X SLING XAERSL	LAMDA SL ALML	X F. ROT XAERFR	X R. ROT XAERRR	X/M AX		BD FRF BDFRF	BD FFR BDFFR
Y FUSE YAERFS	Y SLING YAERSL	NU SL ANUL	Y F. ROT YAERFR	Y R. ROT YAERRR	Y/M AY	AICF BOD 57.3×A1CFRC	BICF BOD 57.3×BICFRC	THOF BOD 57.3×THOFR
Z FUSE ZAERFS	Z SLING 0.0	MU SL AMUL	Z F. ROT ZAERFR	Z R. ROT ZAERRR	Z/M AZ	AICR BOD 57.3×A1CRRRC	BICR BOD 57.3×BICRRRC	THOR BOD 57.3×THORRC
L FUSE ALARFS	L SLING 0.0	K BAR SL SLKBAR	L F. ROT ALARFR	L R. ROT ALARRR	L/IXX TTL/XIXX	LHBF BOD ALBDFR	LHBR BOD ALBDRR	PFR PFR
M FUSE AMARFS	M SLING 0.0		M F. ROT AMARFR	M R. ROT AMARRR	M/IYY TTM/XIYY	MHBF BOD AMBDFR	MHBR BOD AMBDRR	QFR QFR
N FUSE ANARFS	N SLING ANARSL		N F. ROT ANARFR	N R. ROT ANARRR	N/IZZ TTN/XIZZ	A1FR BOD 57.3×A1BDFR	AIRR BOD 57.3×A1BDRR	PRR PRR
BETA FS 57.3×BETAFS	BETA SL 57.3×BETSL	SL WGHT WGHTSL	BETA FR BETAFR	BETA RR BETARR		B1FR BOD 57.3×B1BDFR	B1RR BOD 57.3×B1BDRR	QRR QRR
ALPH FS 57.3×ALPHFS	ALPH SL 57.3×ALPHSL	J SL BJSL				HFR BODY HFRBOD	HRR BODY HRRBOD	
VINTF VINTF	THETA SL 57.3×THESL	L SL BLSL			WIRR WIRR	YFR BODY YFRBOD	YRR BODY YRRBOD	
WIFS WIFS	SMA SL SASL	R SL BRSL					A1CRR 57.3×A1CRR	B1CRR 57.3×B1CRR

Logical flags

IECSCON
RSASP
RSASR
NSTALL
NGREFF

Table entry

FORTRAN MNEMONIC

TABLE 4.- ARC VS. B.V. MODEL DYNAMIC
RESPONSE DATA: FLIGHT CONDITIONS

Straight and level Gross weight = 33,000 lb $I_{xx} = 34,000 \text{ slug-ft}^2$ $I_{yy} = 202,500 \text{ slug-ft}^2$ $I_{zz} = 191,000 \text{ slug-ft}^2$ $I_{xz} = 14,900 \text{ slug-ft}^2$ $I_{xy} = I_{yz} = 0$ $\Delta X_{c.g.} = 0$		
Figure number	Perturbation control	Equivalent airspeed, knots
1-4	δ_B	0.1
5-8	δ_A	.1
9-12	δ_R	.1
13-16	δ_C	.1
17-20	δ_B	40.
21-24	δ_A	40.
25-28	δ_R	40.
29-32	δ_C	40.
33-36	δ_B	75.
37-40	δ_A	75.
41-44	δ_R	75.
45-48	δ_C	75.
49-52	δ_B	115.
53-56	δ_A	115.
57-60	δ_R	115.
61-64	δ_C	115.
65-68	δ_B	130.
69-72	δ_A	130.
73-76	δ_R	130.
77-80	δ_C	130.

TABLE 5.- B.V. SIMULATION VS. FLIGHT TEST DYNAMIC RESPONSE DATA: FLIGHT CONDITIONS

Figure number	Flight parameters							
	Gross weight, lb	Density altitude, ft	Rotor rpm	$\Delta X_{c.g.}$ (DXCG) in.	SAS configuration	Equivalent airspeed, knots	Flight condition	Flight test data reference
81	37,000	2400	Nominal: 230	0.5	ON	Hover	Straight and level	2
82	36,780	980	233	6.6	ON	35	Straight and level	3
83	38,470	3220	Nominal	0	ON	70	Straight and level	2
84	33,320	5440	Nominal	17.8	ON	110	Straight and level	2
85	33,320	5440	Nominal	17.2	ON	115	Straight and level	2
86	36,700	4820	236	6.0	ON	127	Straight and level	3

TABLE 6.- ARC MODEL STATIC TRIM DATA: FLIGHT CONDITIONS
— SLUNG LOAD ATTACHED —

		Flight parameters						
Table number	Helicopter weight, lb	Helicopter moments and products of inertia, slug-ft ²	$\Delta X_{C.G.}$, in.	SAS configuration	Equivalent airspeed, knots	Slung load weight, lb	Relative slung load attitude, θ_{SL} , deg	Flight condition
42	25,500	I _{xx} = 25,500 I _{yy} = 185,000 I _{zz} = 170,000 I _{xz} = 13,000 I _{xy} = I _{yz} = 0	0	ON	0.1	7500.	0	Straight and level
43		I _{xx} = 25,500 I _{yy} = 185,000 I _{zz} = 170,000 I _{xz} = 13,000 I _{xy} = I _{yz} = 0			75		0	
44		I _{xx} = 25,500 I _{yy} = 185,000 I _{zz} = 170,000 I _{xz} = 13,000 I _{xy} = I _{yz} = 0			.1		-5	
45		I _{xx} = 25,500 I _{yy} = 185,000 I _{zz} = 170,000 I _{xz} = 13,000 I _{xy} = I _{yz} = 0			75		-5	

TABLE 7.- ARC VS. B.V. MODEL DYNAMIC
RESPONSE DATA: FLIGHT CONDITIONS
— SLUNG LOAD ATTACHED —

Straight and level SAS on Helicopter weight = 25,500 lb Helicopter I_{xx} = 25,500 slug-ft ² Helicopter I_{yy} = 185,500 slug-ft ² Helicopter I_{zz} = 170,000 slug-ft ² Helicopter I_{xz} = 13,000 slug-ft ² Helicopter I_{xy} = I_{yz} = 0 $\Delta X_{c.g.}$ = 0 Slung load weight = 7500 lb θ_{SL} = 0°		
Figure number	Perturbation control	Equivalent airspeed, knots
87-89	δ_B	0.1
90-92	δ_A	.1
93-95	δ_R	.1
96-98	δ_C	.1
99-101	δ_B	75.
102-104	δ_A	75.
105-107	δ_R	75.
108-110	δ_C	75.

TABLE 8.- STATIC TRIM DATA

$V_{eq} = 0.1$ knot, SAS off

CH-47B TRIM DATA PDR 101 15									
14:41 FEB 11, '83									
WTOT = .1 FT	0	= .1 FT	0	= .0700 FT	0	= .0000 FT	0	= .0000 FT	0
G.W. = 33000.0 LBS PPN =	.04.1	0.0	.04.1	0.0	.04.1	0.0	.04.1	0.0	.04.1
THETH	PHI	Psi	R	YAW	P	ROLL	P	ROLL	P
.66120E-01	-.44531E-00	.00000E+00							
DELB PLT	DELS PLT	DELR PLT	DELP PLT	DELT PLT	DETR PLT				
-.57220E-02	.00000E+00	-.15000E-01	.00000E+00	-.15000E-01	.00000E+00	-.15000E-01	.00000E+00	-.15000E-01	.00000E+00
THETO FF	HICPP	BICPP	THETO FR	HICFR	BICFR	THETO FR	HICFR	BICFR	THETO FR
.18552E-02	.42036E-00	-.15000E-01	.10550E-01	.42036E-00	-.15000E-01	.10550E-01	.42036E-00	-.15000E-01	.10550E-01
SIGHH FF	SIGHH FR	GHITH FG	SIGHH FF	SIGHH FR	GHITH FG	SIGHH FF	SIGHH FR	GHITH FG	SIGHH FF
.66379E-01	.66979E-01	.41076E-01	.66379E-01	.66979E-01	.41076E-01	.66379E-01	.66979E-01	.41076E-01	.66379E-01
THROST F	HORNAL F	SIDE F	THROST F	HORNAL F	SIDE F	THROST F	HORNAL F	SIDE F	THROST F
.16071E-05	.44525E-03	.10440E-03	.16071E-05	.44525E-03	.10440E-03	.16071E-05	.44525E-03	.10440E-03	.16071E-05
THROST F	HORNAL R	SIDE F	THROST F	HORNAL R	SIDE F	THROST F	HORNAL R	SIDE F	THROST F
-.16698E-05	-.43515E-03	-.10394E-03	.16698E-05	-.43515E-03	-.10394E-03	.16698E-05	-.43515E-03	-.10394E-03	.16698E-05
FT FF	CH FF	CY FF	CO FF	CH FF	CY FF	CH FF	CH FF	CY FF	CH FF
.48217E-02	.10568E-03	.35440E-04	.44121E-03	.10568E-03	.35440E-04	.44121E-03	.10568E-03	.35440E-04	.44121E-03
CT FF	CH FF	CY FF	CO FF	CH FF	CY FF	CH FF	CH FF	CY FF	CH FF
-.47697E-02	-.12443E-03	-.36363E-04	.44121E-03	-.12443E-03	-.36363E-04	.44121E-03	-.12443E-03	-.36363E-04	.44121E-03
Z FUSE	Z SLING	LADFH SL	Z F.POT	Z F.POT	L F.POT	Z F.POT	L F.POT	E F.POT	Z F.POT
-.25000E-00	-.12388E-04	.00000E-00	.12001E-04	-.12388E-04	.00000E-00	.12001E-04	-.12388E-04	.00000E-00	.12001E-04
V FUSE	V SLING	MU SL	V F.POT	V F.POT	L F.POT	V F.POT	L F.POT	E F.POT	V F.POT
.20583E-00	.00000E-00	.00000E-00	.12440E-03	.00000E-00	.12440E-03	.00000E-00	.12440E-03	-.15000E-01	.12440E-03
Z FUSE	Z SLING	MU SL	Z F.POT	Z F.POT	L F.POT	Z F.POT	L F.POT	E F.POT	Z F.POT
.57088E-03	.00000E-00	-.10255E-02	-.16733E-05	-.16613E-05	-.31394E-05	-.16613E-05	-.31394E-05	-.15000E-01	-.15000E-01
L FUSE	L SLING	F BPF SL	L F.POT	E F.POT	L F.POT				
.21780E-00	.00000E-00	.10135E-01	-.52404E-04	.00000E-00	-.52404E-04	.00000E-00	-.52404E-04	-.65000E-03	.10135E-01
M FUSE	M SLING	M F.POT	E F.POT	M F.POT					
.83036E-03	.00000E-00	.00000E-00	.32757E-05	-.32757E-05	-.32757E-05	-.32757E-05	-.32757E-05	-.21910E-04	.00000E-00
N FUSE	N SLING	N F.POT	E F.POT	N F.POT					
-.50767E-00	.00000E-00	.00000E-00	.45476E-05	-.45476E-05	-.45476E-05	-.45476E-05	-.45476E-05	-.14940E-01	.00000E-00
BETA FS	BETA SL	SL WIGHT	BETA FR	E F.POT	BETA FR				
-.51618E-01	.00000E-00	.75000E-04	-.51319E-01	-.51328E-01	-.51328E-01	-.51328E-01	-.51328E-01	-.44351E-03	.00000E-00
ALPH FS	ALPH SL	J SL						HFP BODY	HFP BODY
-.89684E-02	.26000E-01	.77711E-04						-.44314E-03	-.44314E-03
VINTF	THETA SL	L SL						HFP BODY	HFP BODY
.41103E-02	.00000E-00	.20000E-02						-.12440E-03	-.12440E-03
WIFS	SMA SL	R SL						AICPP	BICPP
-.30444E-02	.20000E-02	.80000E-01						-.44359E-00	.14996E-01
CONTROL FLAGS SET UP									
ISLING	0	IECSOON	0						
IDCPT	0	PS4SP	0						
RSASQ	0	RSASR	0						
ISTEADY	1	NSTALL	1						
NTROCR	1	NGREF	0						
ISLTPM	1								

TABLE 9.- STATIC TRIM DATA

$V_{eq} = 0.1$ knot, SAS on

CH-47B TRIM DATA RUN NO. 33													
VTOT =	.1 KT	U	* .1 KT	V	* -.0 KT	W	* .0 KT	.0 IN	DZDG =	.0 IN	DZDG =	.0 IN	PRP =
G.W. =	33000.0	LBS	PPM =	24.1	H	=	97.0 FT	TEMP =	368.0 IG	DZDG =			.0
THETA	PHI	PSI	P	0	RHO	OMEGA FP	OMEGA PR						
.66120E 01	-.44531E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
DELB PLT	DELS PLT	DELP PLT	DELC PLT	DELB TOT	DELS TOT	DELF TOT	DELC TOT	H DOT					
-.57220E-02	.22617E 00	-.32292E-02	.57555E 01	-.57220E-02	.22617E 00	-.32292E-02	.57555E 01	.00000E 00					
THETO FP	AICFP	BICFP	THETO PP	INC	INC	INC	INC						
.18552E 02	.41998E 00	-.15004E 01	.18559E 02	.34000E 05	.20050E 06	.19100E 06	.14900E 05	.10971E 01					
SIGMA FP	SIGMA FP	GRMMH FS		LAMDA FP	LAMDA FP	TM FP	MU FP	MACH NO.					
.66979E-01	.66979E-01	.41076E-02		-.56893E-01	-.57525E-01	.23571E-03	.23567E-03	.15144E-03					
THPUST F	NORMAL F	SIDE F	TOPONE F	L HUB FP	M HUB FP	U TIP FP	TELLA FP	F FP					
.16871E 05	.44325E 03	.12389E 03	.48371E 05	-.41576E 03	-.40565E 04	.10770E-03	.10770E-03	.13419E 07					
THPUST P	NORMAL P	SIDE P	TOPOUP P	L HUB PP	M HUB PP	U TIP PP	DEPTH PP	F PP					
.16690E 05	-.43538E 03	-.12910E 03	.48321E 05	-.48494E 03	-.42151E 04	.02340E 03	.10724E-01	.13409E 07					
CT FP	CH FP	CY FP	CO FP	AO FP	AI FP	RI FP	O GOV FP						
.48217E-02	.12668E-03	.35408E-04	.41317E-03	.45674E 01	.15044E-01	.42114E-09	.43371E-05						
CT PP	CH PP	CY PP	CO PP	AO PP	AI PP	RI PP	O GOV PP						
.47697E-02	-.12443E-03	-.36895E-04	.41221E-03	.45255E 01	-.14950E-01	-.44249E-09	.43271E-05						
X FUSE	X SLING	LAMDA SL	X F.POT	X P.POT	X I.POT	X D.POT	X B.POT						
-.25000E 00	-.12388E 04	.00000E 00	.22616E 04	.15936E 04	.32078E 01	.32078E 01	.32078E 01	.35012E 00					
Y FUSE	Y SLING	NU SL	Y F.POT	Y P.POT	Y I.POT	Y D.POT	Y B.POT						
.20503E 00	.00000E 00	.00000E 00	.12429E 03	.12871E 03	.24707E 00	.42133E 00	.42133E 00	-.15000E 01					
Z FUSE	Z SLING	MU SL	Z F.POT	Z P.POT	Z I.POT	Z D.POT	Z B.POT						
.57088E 03	.00000E 00	-.10255E 02	-.16733E 05	-.16619E 05	-.31996E 02	-.44233E 00	-.15000E 01	.15000E 01					
L FUSE	L SLING	K BAR SL	L F.POT	L P.POT	L I.POT	L D.POT	L B.POT						
.21780E 00	.00000E 00	.18135E 01	-.52418E 04	-.52385E 04	-.38373E-02	-.61555E 03	-.65064E 03	.00000E 00					
M FUSE	II SLING		II F.POT	II P.POT	II I.POT	II D.POT	II B.POT						
.83096E 03	.00000E 00		.32757E 06	-.32841E 06	-.50000E-04	.12501E 04	.12501E 04	.21910E 04					
N FUSE	N SLING		N F.POT	N P.POT	N I.POT	N D.POT	N B.POT						
-.50767E 00	.00000E 00		.45473E 05	-.45496E 05	-.12371E-03	.15044E 01	.15044E 01	-.14944E 01					
BETA FS	BETH SL	SL WHT	BETH FP	BETH PR			BETH BOD	BETH BOD					
-.51618E-01	.00000E 00	.75000E 04	-.51319E-01	-.51328E-01			.42315E 00	.44339E 00					
ALPH FS	ALPH SL	J SL					HFP BOD	HFP BOD					
-.89684E 02	.26000E 01	.27711E 04					44214E 03	44214E 03					

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VINTF     THETA SL    L SL          WIFF      VPF BODY    VPR BODY
03E 02   .0000E 00   .2000E 02   .0000E 00   .12429E 03  -.13949E 03

UIFS      SMA SL    R SL          AICPP      BICPP
44E 02   .2000E 02   .8000E 01   -.44397E 00  .14396E 01

CONTROL FLAGS SET UP
ISLING 0  IECSCON 0
IDCPT 1   RSASP 1
RSASQ 1   RSASR 1
ISTEADY 1  NSTALL 1
NTROCR 1  NGREFF 0
ISLTPM 1

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TABLE 10.- STATIC TRIM DATA

$V_{eq} = 20$ knots, SAS off

CH-47D TRIM DATA RUN NO. 37												
14:45 FEB 11 183												
VTOT = 20.0 KT	U	= 19.9 FT	V	= -0.9 FT	M	= 1.9 FT	DPG	DEG	10 IN	PDP	=	.0
G.W. = 33000.0 LBS RPM	*	24.1	H	97.5	TMR	286.0	0	0	0	0		
THETA	PHI	PSI	F	O	R	F	C	ONEGR FP	ONEGR FP			
.54756E 01	-.38958E 00	.00000E 00	.30000E 00	.10000E 00	.00000E 00							
DELB PLT	DELS PLT	DELP PLT	DELT PLT	DELB TOT	DELT TOT	DELP TOT	DELT TOT	DELS TOT	DELT TOT	H PWT		
-.14901E 01	.21625E 00	.24915E 00	.54003E 01	-.14901E 01	.14901E 01	.14901E 01	.14901E 01	.14901E 01	.14901E 01	.00000E 00		
THETO FR	AICFR	E1CFF	THETO PP	I 00	F 00	00	00	I 00	I 00	I 00	E1CFF	
.17350E 02	.12044E 01	-.15003E 01	.19183E 02	-.34000E 05	.20274E 06	.18193E 00	.14200E 05	.14200E 05	.14200E 05	.14200E 05	.15000E 01	
SIGMA FR	SIGMA FP	GRMFR FS	LHMH FP	NU FP	NU FP	NU FP	NU FP					
.66979E-01	.66979E-01	.60054E 00	-.45390E 01	-.63117E 01	.14804E 00	.14804E 00						
THRUST F	NORMAL F	SIDE F	TOPQUE F	L HGT FP	L HGT FP	L HGT FP	L HGT FP	DELT FP	DELT FP	DELT FP	F FP	
.16633E 05	.69873E 03	.30148E 03	.30085E 05	-.11338E 04	.15378E 04	.15378E 04	.15378E 04	.10235E 01	.10235E 01	.10235E 01	.15439E 07	
THFUST P	HORMAL P	SIDE P	TOPQUE P	L HGT FP	L HGT FP	L HGT FP	L HGT FP	DELT FP	DELT FP	DELT FP	F FP	
.16775E 05	-.13963E 03	.16288E 03	.14239E 05	-.97147E 03	-.84047E 03	-.84047E 03	-.84047E 03	.10236E 01	.10236E 01	.10236E 01	.15439E 07	
CT FR	CH FR	CY FR	CO FP	HO FP	HO FP	HO FP	HO FP	0 00V FP	0 00V FP	0 00V FP		
.47537E-03	-.19969E-03	.10902E-03	.30566E-03	-.45666E-01	.12307E-01	.12307E-01	.12307E-01	.14759E-01	.14759E-01	.14759E-01	.32035E-05	
CT PR	CH PR	CY PR	CO PR	HO PR	HO PR	HO PR	HO PR	0 00V PR	0 00V PR	0 00V PR		
.47941E-03	-.39906E-04	.46551E-04	.40789E-03	-.46601E-01	.15777E-01	.15777E-01	.15777E-01	.16640E-01	.16640E-01	.16640E-01	.42801E-05	
X FUSE	Z SLING	L SLING	Y PLDT	BD FPR	BD FPR	BD FPR						
-.72448E 02	-.12388E 04	.00000E 00	.19101E 04	.13003E 04	.13003E 04	.13003E 04	.13003E 04	-.18448E 00	-.18448E 00	-.18448E 00	.29513E 00	
Y FUSE	Z SLING	M SL	F PLDT	Y PLDT	Y PLDT	Y PLDT	Y PLDT	BD FPR	BD FPR	BD FPR		
.22038E 01	.00000E 00	.00000E 00	.38193E 03	-.16037E 03	.10139E 03	.10139E 03	.10139E 03	-.15000E 01	-.15000E 01	-.15000E 01	.11750E 02	
Z FUSE	Z SLING	M SL	C PLDT	Z PLDT	Z PLDT	Z PLDT	Z PLDT	BD FPR	BD FPR	BD FPR		
.41296E 03	.00000E 00	-.10255E 03	-.10139E 03	.11034E 03	.11034E 03	.11034E 03	.11034E 03	-.15000E 01	-.15000E 01	-.15000E 01	.11750E 02	
L FUSE	L SLING	F EBF	L PLDT	BD FPR	BD FPR	BD FPR						
-.13284E 02	.00000E 00	.10155E 01	-.15784E 02	.18154E 02	.18154E 02	.18154E 02	.18154E 02	-.15000E 01	-.15000E 01	-.15000E 01	.10210E 00	
M FUSE	II SLING	II EBF	II PLDT	BD FPR	BD FPR	BD FPR						
-.14271E 04	.00000E 00	.00000E 00	.15693E 06	-.14543E 06	.166607E 04	.166607E 04	.166607E 04	-.18475E 04	-.18475E 04	-.18475E 04	.00300E 00	
N FUSE	N SLING	N EBF	N PLDT	BD FPR	BD FPR	BD FPR						
-.65996E 02	.00000E 00	.00000E 00	.58032E 05	-.59762E 05	.18867E 04	.18867E 04	.18867E 04	-.15780E 01	-.15780E 01	-.15780E 01	.10000E 00	
BETA FS	BETH SL	SLIGHT	FETH FP	BETH FP	BETH FP	BETH FP	BETH FP	BD FPR	BD FPR	BD FPR		
-.36398E-01	.00000E 00	.17600E 04	-.36436E-01	-.36436E-01	-.36436E-01	-.36436E-01	-.36436E-01	-.14774E 01	-.14774E 01	-.14774E 01	.16644E 00	
ALPH FS	ALPH SL	J SL						HPP BODY	HPP BODY	HPP BODY		
-.33697E 02	.26000E 01	.77711E 04						.163649E 03	-.13974E 03	-.13974E 03		

VINTF	THETA SL	L SL						VIFF	VIFF BODY	VIFF BODY		
.30655E 02	.00000E 00	.20000E 03						.00000E 00	.38133E 03	.16273E 03		
WIFS	SMA SL	P SL									AICPR	
-.25664E 02	.20000E 02	.80000E 01									.37829E 00	.15002E 01
CONTROL FLAGS SET UP												
ISLING 0	IECSCON 0											
IDCPT 0	RSASP 0											
RSASO 0	PSASR 0											
ISTEADY 1	NSTALL 1											
NTROCR 1	NGREFF 0											
ISLTRM 1												

TABLE 11.- STATIC TRIM DATA

$V_{eq} = 20$ knots, SAS on

CH-47B TRIM DATA RUN NO. 57												
15:17 FEB 11, '83												
WTOT = 20.0 FT	U	= 19.9 FT	V	= -0.0 FT	W	= 1.9 FT	JR IN	DCDG	JR IN	PHC	JR IN	PHC
G.W. = 33000.0 LBS RPM = 24.1 H			= 97.5 FT	TEMP = 0	= 288.0 DS	DCGNS = 0						
THETA	PHI	PSI	P	O	F	PHC	OMEGA FP	OMEGA RP				
.54760E 01	-.38616E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00				
DELB PLT	DELS PLT	DELP PLT	DELC PLT	DELD PLT	DELC TOT	DELD TOT	DELP TOT	DELC TOT				
-.14901E 01	.31587E 00	.29086E 00	.56000E 01	-.14301E 01	.00000E 00	.00000E 00	.00000E 00	.00000E 00				
THETO FR	AICFP	BICFP	THETO FP	ICF	TCF	TCF	ICF	TCF				
.17350E 02	.12075E 01	-.15000E 01	.19183E 02	* .34000E 05	.00000E 05	.00000E 05	.19100E 06	.19100E 06				
SIGMA FR	SIGMA FP	GAMMA FS		LAMBDA FP	LAMBDA FP	MU FP	MU FP	MU FP				
.66979E-01	.68379E-01	.80054E 00		-.45301E-01	-.63813E-01	.46194E-01	.46194E-01	.46194E-01				
THRUST F	NORMAL F	SIDE F	TORQUE F	L HUB FP	M HUB FP	N HUB FP	O HUB FP	P HUB FP				
.16533E 05	.69871E 03	.38238E 03	.42084E 03	.00000E 04	.00000E 04	.00000E 04	.00000E 04	.00000E 04				
THRUST P	NORMAL P	SIDE P	TORQUE P	L HUB FP	M HUB FP	N HUB FP	O HUB FP	P HUB FP				
.16774E 05	-.13964E 03	.16424E 03	.42600E 05	.00000E 03	-.04964E-05	-.04964E-05	-.04964E-05	-.04964E-05				
CT FP	CH FP	CY FP	CO FP	H0 FP	A1 FP	D1 FP	C0 GND FP					
.47536E-02	.19969E-03	.19928E-03	.30565E-03	.46000E-01	.00000E 01	.14711E 01	.14711E 01	.14711E 01				
CT PR	CH PR	CY PR	CO PR	H0 PR	A1 PR	D1 PR	C0 GND PR					
.47940E-02	-.39907E-04	.46937E-04	.40780E-03	.46000E-01	-.57765E 00	.00000E 00	.14286E 05	.14286E 05				
X FUSE	X SLING	LHDLH SL	CF.POT	X.POT	CF.DD	X.DD	CF.BOD	X.BOD				
-.72448E 02	-.12388E 04	.00000E 00	.19121E 04	.13399E 04	.00000E 00	.13399E 04	.00000E 00	.13399E 04				
Y FUSE	Y SLING	MU SL	CF.POT	Y.POT	Y.DD	Y.DD	Y.BOD	Y.BOD				
.22039E 01	.00000E 00	.00000E 00	.38293E 03	-.16432E 03	.00000E 00	.14736E 03	.00000E 00	.14736E 03				
Z FUSE	Z SLING	MU SL	CF.POT	Z.POT	Z.DD	Z.DD	Z.BOD	Z.BOD				
.41296E 03	.00000E 00	-.10255E 02	-.16535E 05	.16724E 05	-.16535E 05	.16724E 05	-.16535E 05	.16724E 05				
L FUSE	L SLING	E BHFB SL	L.F.POT	L.F.POT	L.F.DD	L.F.DD	L.HFB.BOD	L.HFB.BOD				
-.12384E 02	.00000E 00	.10135E 01	-.18274E 01	.00000E 01	.183018E 01	.186343E 01	.00000E 01	.186343E 01				
M FUSE	M SLING											
-.14270E 04	.00000E 00											
N FUSE	N SLING											
-.65995E 02	.00000E 00											
BETA FS	BETA SL	SL LIGHT	BETA FP	BETA PP			BIFP BOD	BIFP BOD				
-.37019E-01	.00000E 00	.75000E 04	-.36301E 01	-.36301E 01			.14700E 01	.14700E 01				
ALPH FS	ALPH SL	J SL					HIFP BOD	HIFP BOD				
-.33696E 02	.26000E 01	.77771E 04					.16000E 03	-.13901E 03				
VINTF	THETA SL	L SL					WIPF	WIPF BOD				
.30655E 02	.00000E 00	.20000E 02					.00000E 00	.00000E 00				
WIFS	SMA SL	R SL										
-.25663E 02	.20000E 02	.80000E 01										
CONTROL	FLAGS SET UP											
ISLING 0	IECSCON 0											
IDCPT 1	PSHSP 1											
RSASD 1	PSHSP 1											
ISTEADY 1	NSTALL 1											
NTROCR 1	NGPEFF 0											
ISLTPM 1												

TABLE 12.- STATIC TRIM DATA

$V_{eq} = 40$ knots, SAS off

CH-47B TRIM DATA PUN NO. 41												
14:49 FEB 11, '83												
VTOT = 40.0 KT	U	* 39.9 FT	V	* 40 KT	W	* 3.0 FT	X	* 280.0 KG	Y	* 1.0 KG	Z	* .0
G.W. = 33000.0 LBS PPM		24.1 H		98.0 FT	TEMP =	280.0 KG	WTG =	.0	IN	DEGS =	.0 IN	PPH = .0
THETA	PHI	PSI	P	O	R	S	T	U	V	W	X	Y
.42599E 01	-.29411E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.25400E-02	.24085E 02	.24165E 02	.0	.0
DELB PLT	DELS PLT	DELP PLT	DELC PLT	DELB TOT	DELS TOT	DELP TOT	DELC TOT	.51744E 01	.51742E 01	.51744E 01	H INT	.00000E 00
-.23407E 01	.21366E 00	.37435E 00	.51744E 01	-.23407E 01	.21367E 01	.37435E 00	.51744E 01					
THETO FP	AICFP	BICFP	THETO PP	IIC	IV	IIC	IIC					
.16035E 02	.15998E 01	-.15000E 01	.18914E 02	.34000E 05	.30000E 05	.19100E 05	.14000E 05					
SIGMA FP	SIGMA PP	GRMNA FS	LHMIA FP	LAHMF FP	LLHMF FP	LLHMF FP	LLHMF FP					
.66879E-01	.66879E-01	.12330E 01	-.10254E-01	-.10254E-01	-.10254E-01	-.10254E-01	-.10254E-01					
THRUST F	NOPNHL F	SIDE F	TOPDNE F	L HUB FP	M HUB FP	M TIP FP	M TIP FP					
.16456E 05	.90044E 03	.49549E 03	.32480E 05	.10174E 01	.41304E 01	.17214E 07	.10174E 01					
THRUST P	NOPNHL P	SIDE P	TOPDNE P	L HUB FP	M HUB FP	M TIP FP	M TIP FP					
.16884E 05	.14919E 03	.32800E 03	.32800E 05	.10174E 01	.41304E 01	.17214E 07	.10174E 01					
CT FP	CH FP	CV FP	CO FP	-O FP	-H FP	-M FP	-M FP					
.47031E-02	.25734E-03	.14161E-03	.21416E-03	.41468E 01	.29281E-01	.23130E-01	.23130E-01					
CT PP	CH PP	CV PP	CO PP	-O PP	-H PP	-M PP	-M PP					
.48254E-02	.42638E-04	.93757E-04	.50059E-03	.45555E 01	.30177E-01	.13135E 01	.13135E 01					
X FUSE	X SLING	LAHDA SL	X F.POT	X P.POT	X P.POT	X P.POT	X P.POT					
-.26260E 03	-.12388E 04	.00000E 00	.16851E 04	.10288E 04	.33510E 01	.33510E 01	.33510E 01					
Y FUSE	Y SLING	MU SL	Y F.POT									
.10885E 01	.00000E 00	.00000E 00	.43503E 03	-.32600E 03	.16487E 00	.16487E 01	.16487E 01					
Z FUSE	Z SLING	MU SL	Z F.POT									
.33934E 03	.00000E 00	-.10255E 02	-.16394E 05	-.16653E 05	-.32110E 01	.78424E 00	.78424E 00					
L FUSE	L SLING	M BAP SL	L F.POT									
-.10000E 02	.00000E 00	.10135E 01	.32579E 04	-.32480E 04	-.32000E 04	.30000E 04	.19782E 04					
M FUSE	M SLING	M BAP SL	M F.POT									
-.34349E 04	.00000E 00		.32661E 06	-.32317E 06	-.10180E 04	.14757E 04	.14423E 03					
N FUSE	N SLING	N BAP SL	N F.POT									
.70334E 02	.00000E 00		.32818E 05	-.32689E 05	-.29859E 05	.13943E 01	.30952E 00					
BETA FS	BETA SL	SL WIGHT	BETA FP	BETA PP	BETA PP	BETA PP	BETA PP					
-.21907E-01	.00000E 00	.75000E 04	-.21922E 01	-.21847E 01	.1143E 01	.13496E 01	.10000E 00					
ALPH FS	ALPH SL	J SL										
-.10154E 02	.26000E 01	.77711E 04										
VINTF	THETA SL	L SL										
.18152E 02	.00000E 00	.20000E 02										
WIFS	SMA SL	R SL										
-.17096E 02	.20000E 02	.80000E 01										
CONTROL FLAGS SET UP												
ISLING 0	IECSCON 0											
IDCPT 0	RSASP 0											
RSAS0 0	RSASR 0											
ISTEADY 1	HSTALL 1											
NTROCR 1	NGREFF 0											
ISLTRM 1												

TABLE 13.- STATIC TRIM DATA

$V_{eq} = 40$ knots, SAS on

CM-473 TRIM DATA PUN NO. 29											
14:36 FEB 11, 1983	VTOT = 40.0 FT	U	= 39.9 FT	V	= 38.9 FT	W	= 38.0 FT	X	= 38.0 FT	Z	= 38.0 FT
G.W. = 33000.0 LBS PPM =	24.1	H	.00000E 00								
THETA	PHI	PSI	P	Q	R	S	T	U	V	W	Z
.42600E 01	-.29424E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
DELB PLT	DELS PLT	DELP PLT	DELC PLT	DELB TOT	DELS TOT	DELC TOT	DELP TOT	DELT TOT	DELT TOT	DELT TOT	DELT TOT
-.23407E 01	.21360E 00	.37636E 00	.39174E 01	-.15407E 01	.21360E 00	.37636E 00	.39174E 01	.37636E 00	.39174E 01	.37636E 00	.39174E 01
THETO FP	HICFP	BICFP	THETO PR	L1	L2	L3	L4	L5	L6	L7	L8
.16035E 02	.16000E 01	-.15000E 01	.13914E 02	.14000E 05							
SIGMA FP	SIGMA FP	GHMIA FS		1400A FP	1400C FP	1400D FP	1400E FP	1400F FP	1400G FP	1400H FP	1400I FP
.66979E-01	.66979E-01	.12320E 01		-.18000E-01							
THRUST F	NORMAL F	SIDE F	TOPOF F	L HUB FP	M HUB FP	N HUB FP	O HUB FP	P HUB FP	Q HUB FP	R HUB FP	S HUB FP
.16456E 05	.80045E 03	.43554E 03	.22480E 05	-.30146E 04	-.42964E 04						
THRUST F	NORMAL F	SIDE F	TOPOF F	L HUB FP	M HUB FP	N HUB FP	O HUB FP	P HUB FP	Q HUB FP	R HUB FP	S HUB FP
.16884E 05	.14919E 03	.33818E 03	.38901E 05	-.19704E 04	-.41814E 04						
CT FP	CH FP	CV FP	CO FP	A0 FP	A1 FP	A2 FP	A3 FP	A4 FP	A5 FP	A6 FP	A7 FP
.47031E-02	.35735E-03	.14162E-03	.21416E-03	-.41469E 01	.12919E 01	.12919E 01	.12919E 01	.12919E 01	.12919E 01	.12919E 01	.12919E 01
CT PR	CH PR	CV PR	CO PR	A0 PR	A1 PR	A2 PR	A3 PR	A4 PR	A5 PR	A6 PR	A7 PR
.48255E-02	.42639E-04	.93793E-04	.37060E-03	-.45556E 01	.13057E 01	.13057E 01	.13057E 01	.13057E 01	.13057E 01	.13057E 01	.13057E 01
X FUSE	X SLING	LANDA SL	Y F.POT	Z F.POT	A F.POT	B F.POT	C F.POT	D F.POT	E F.POT	F F.POT	G F.POT
-.26260E 03	-.12388E 04	.00000E 00	.16851E 04	-.10039E 04	-.10039E 04	-.10039E 04	-.10039E 04	-.10039E 04	-.10039E 04	-.10039E 04	-.10039E 04
Y FUSE	Y SLING	NU SL	Y F.POT	Z F.POT	A F.POT	B F.POT	C F.POT	D F.POT	E F.POT	F F.POT	G F.POT
.10885E 01	.00000E 00	.00000E 00	.49588E 03	-.32317E 03	-.16347E 03						
Z FUSE	Z SLING	NU SL	Z F.POT	A F.POT	B F.POT	C F.POT	D F.POT	E F.POT	F F.POT	G F.POT	H F.POT
.33934E 03	.00000E 00	-.10255E 02	-.16394E 05								
L FUSE	L SLING	K BAR SL	L F.POT	M F.POT	N F.POT	O F.POT	P F.POT	Q F.POT	R F.POT	S F.POT	T F.POT
-.10000E 02	.00000E 00	.10135E 01	.32986E 04	-.32501E 04	-.44513E 04						
M FUSE	M SLING		M F.POT	N F.POT	O F.POT	P F.POT	Q F.POT	R F.POT	S F.POT	T F.POT	U F.POT
-.34349E 04	.00000E 00		.32661E 06	-.32318E 06	-.17559E 06						
N FUSE	N SLING		N F.POT	O F.POT	P F.POT	Q F.POT	R F.POT	S F.POT	T F.POT	U F.POT	V F.POT
.70334E 02	.00000E 00		.32819E 05	-.32887E 05	-.12414E 04						
BETA FS	BETA SL	SL WHT	BETA FP	BETA PR							
-.21917E-01	.00000E 00	.75000E 04	-.21932E-01	-.21957E-01							
ALPH FS	ALPH SL	J SL									
-.10154E 02	.26000E 01	.77711E 04									
VINTF	THETA SL	L SL									
.18152E 02	.00000E 00	.20000E 02									
WIFS	SMA SL	P SL									
-.17096E 02	.20000E 02	.80000E 01									
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IDCPT 1	RSHSP 1										
RSASQ 1	RSASR 1										
ISTEADY 1	NSTALL 1										
NTROCR 1	NGREFF 0										
ISLTRM 1											
VITPP	VTPP BODY	VTPP BODY									
.00000E 00	.49588E 03	.32823E 03									
RICPP	BICPP	BICPP									
.78407E 00	.15000E 01	.15000E 01									

TABLE 14.- STATIC TRIM DATA

$V_{eq} = 60$ knots, SAS off

CH-47B TRIM DATA RUN NO. 57											
15:21 FEB 11, '83											
VTOT = 60.0 FT U	= 60.0 FT	W = 0.0 FT	= 0.0 FT	Z = 0.0 FT	= 0.0 FT	U = 0.0 FT	= 0.0 FT	V = 0.0 FT	= 0.0 FT	W = 0.0 FT	= 0.0
G.W. = 33000.0 LBS RPM = 24.1	R	P	Q	R	P	Q	R	P	Q	R	P
THETA	PHI	PSI	R	P	Q	R	P	Q	R	OMEGA FP	OMEGA FP
.29602E 01	-.24453E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT
-.10341E 01	.19214E 00	.00000E 00	.47451E 01	.10341E 01	.19214E 00	.19214E 01	.19214E 00	.19214E 01	.19214E 01	.19214E 01	.19214E 00
THETO FR	HICFP	BICFP	THETO FP	DCP	DRCFR						
.15555E 02	.11995E 01	-.15003E 01	.17730E 02	.15400E 05	.15025E 04	.15100E 04	.15100E 06	.15400E 05	.15400E 05	.15400E 05	.15400E 02
SIGMA FR	SIGMA FP	SIGMA FS	SIGMA FP	SIGMA FP	SIGMA FS	SIGMA FP	TAUH 001				
.66979E-01	.66979E-01	.13537E 01									
THRUST F	NORMHL F	SIDE F	TORQUE F	L-HDPL FP	F FP						
.16270E 05	.10886E 04	.37894E 03	.13800E 05	.14337E 04	.15168E 04	.15168E 04	.15168E 05	.15168E 05	.15168E 05	.15168E 05	.15168E 04
THRUST P	NORMAL P	SIDE P	TORQUE P	L-HDPL FP	F FP						
.17092E 05	.38409E 03	.10395E 03	.13800E 05	.14337E 04	.15168E 04	.15168E 04	.15168E 05	.15168E 05	.15168E 05	.15168E 05	.15168E 04
CT FP	CH FP	CF FP	CF FP	AD FP							
.46502E-01	.31111E-03	.10341E-03									
CT FP	CH FP	CF FP	CF FP	AD FP							
.43848E 00	.10341E-03										
X FUSE	X SLING	LHDPL SL	C FLIGHT								
-.57495E 03	-.12388E 04	.00000E 00	.14701E 03								
Y FUSE	Y SLING	NO SL	C FLIGHT								
.82002E 00	.00000E 00	.00000E 00	.14701E 03								
Z FUSE	Z SLING	NO SL	C FLIGHT								
.36168E 03	.00000E 00	.00000E 00	.14701E 03								
L FUSE	L SLING	L-B4R SL	C FLIGHT								
-.22574E 02	.00000E 00	.00000E 00	.14701E 03								
M FUSE	M SLING	L-B4R SL	C FLIGHT								
-.23243E 04	.00000E 00	.00000E 00	.13748E 05								
N FUSE	N SLING	L-B4R SL	C FLIGHT								
-.40111E 02	.00000E 00	.00000E 00	.13748E 05								
BETA FS	BETA SL	SL LIGHT	BETA FP								
-.12645E-01	.00000E 00	.75000E 04	-.11669E 01								
ALPH FS	ALPH SL	T SL									
-.36807E 01	.26000E 01	.77771E 04									
VINTF	THETA SL	L SL									
.11577E 02	.00000E 00	.20000E 02									
WIFS	SMA SL	R SL									
-.11752E 02	.20000E 02	.80000E 01									
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IDCPT 0	RSASP 0										
RSASQ 0	RSASPR 0										
ISTEADY 1	NSTALL 1										
NTRODR 1	INGREFF 0										
ISLTRM 1											

TABLE 15.- STATIC TRIM DATA

$V_{eq} = 60$ knots, SAS on

CH-47B TRIM DATA FNU NO. 57											
15:14 FEB 11, '83											
VTOT = 60.0 FT 0	= 60.0 FT	V = 60.0 FT	-0.0 FT 0	0.0 FT 0	+ 3.1 FT 0	-0.0 FT 0	0.0 FT 0	+ 0.0 FT 0	-0.0 FT 0	+ 0.0 FT 0	-0.0 FT 0
G.W. = 33000.0 LBS PPM =	24.1 H	Psi	P	P	P	P	P	P	P	P	P
THETH	PHI	PSI	P	P	P	P	P	P	P	P	P
.29602E 01	-.24446E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
DELB PLT	DELS PLT	DELP PLT	DELP PLT	DELP TLT							
-.22232E 01	.18714E 00	.26046E 00	.47456E 01	.18041E 01							
THETO FP	RICFP	BIFP	THETO FP								
.15555E 02	.11996E 01	-.15000E 01	.17730E 02	.34000E 05	.30050E 06						
SIGMA FP	SIGNH FP	GRINA FS		LHINDA FP							
.66579E-01	.66579E-01	.13537E 01		-.30700E 01	-.42810E 01						
THRUST F	NORMAL F	SIDE F	TOPRUE F	L HUB FP	L HUB FP	L HUB FP	M TIP FP				
.16271E 05	.10886E 04	.37309E 03	.18600E 05	.18379E 04	.18379E 04	.18379E 04	.17204E 03	.19621E 01	.19621E 01	.19621E 01	.19621E 01
THRUST P	NORMAL P	SIDE P	TOPRUE P	L HUB FP	L HUB FP	L HUB FP	M TIP P				
.17092E 05	.38409E 03	.28866E 03	.28036E 05	.18550E 04	.18464E 04	.18464E 04	.12114E 03	.16313E 01	.16313E 01	.16313E 01	.16313E 01
CT FP	CH FP	CV FP	CD FP	CD FP	CD FP	CD FP	CF FP				
.46502E-02	.31111E-03	.10834E-03	.16930E-03	.16930E-03	.16930E-03	.16930E-03	.18946E 01				
CT FP	CH FP	CV FP	CD FP	CD FP	CD FP	CD FP	CF FP				
.48848E-02	.10447E-03	.60407E-04	.30156E-03	.34116E-03	.34116E-03	.34116E-03	.15634E-03	.15634E-03	.15634E-03	.15634E-03	.15634E-03
X FUSE	X SLING	LHINDA SL	X F.POT	X F.POT	X F.POT	X F.POT					
-.57495E 03	-.12388E 04	.00000E 00	.14700E 04	.18688E 04	.18688E 04	.18688E 04					
Y FUSE	Y SLING	NU SL	Y F.POT	Y F.POT	Y F.POT	Y F.POT					
.82200E 00	.00000E 00	.00000E 00	.37293E 03	-.12955E 03	-.12955E 03	-.12955E 03					
Z FUSE	Z SLING	NU SL	Z F.POT	Z F.POT	Z F.POT	Z F.POT					
.36168E 03	.00000E 00	-.10255E 02	-.16241E 05	-.11307E 05	-.11307E 05	-.11307E 05					
L FUSE	L SLING	F.FAP AL	L F.POT	L F.POT	L F.POT	L F.POT					
-.22257E 02	.00000E 00	.10135E 01	.25479E 04	.19529E 04	.19529E 04	.19529E 04					
M FUSE	M SLING		M F.POT	M F.POT	M F.POT	M F.POT					
-.23243E 04	.00000E 00		.32055E 06	-.15302E 06	-.15302E 06	-.15302E 06					
N FUSE	N SLING		N F.POT	N F.POT	N F.POT	N F.POT					
-.40111E 02	.00000E 00		.27750E 05	-.11700E 05	-.11700E 05	-.11700E 05					
BETA FS	BETH SL	SL LIGHT	BETH FP	BETH FP	BETH FP	BETH FP					
-.12641E 01	.00000E 00	.75000E 04	-.12635E 01	-.12635E 01	-.12635E 01	-.12635E 01					
ALPH FS	ALPH SL	J SL									
-.36807E 01	.26000E 01	.77711E 04									
VINTF	THETA SL	L SL									
.11577E 02	.00000E 00	.20000E 02									
WIFS	SMA SL	R SL									
-.11752E 02	.20000E 02	.80000E 01									
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IDCPT 1	PSHSP 1										
PSAS0 1	PSHSP 1										
ISTEADY 1	NSTALL 1										
NTPOCP 1	NGREFF 0										
ISLTPM 1											

TABLE 16.- STATIC TRIM DATA

$V_{eq} = 80$ knots, SAS off

CH-47B TRIM DATA FILE NO. 67											
15:23 FEB 11 1983											
VTOT = 80.0 FT U	* 80.0 FT	V = -80.0 FT	W = -80.0 FT	M = 060.0 IN MNG	N = 000.0 IN MNG	O = 000.0 IN MNG	P = 000.0 IN MNG	Q = 000.0 IN MNG	R = 000.0 IN MNG	S = 000.0 IN MNG	T = 000.0 IN MNG
G.W. = 33000.0 LBS RPM = 24.1 H	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
THETA	PHI	PSI	P	Q	R	S	T	U	V	W	X
.29508E 01	-.24199E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
DELB PLT	DELS PLT	DELP PLT	DELC PLT	DELR PLT	DELB TOT	DELC TOT	DELR TOT	DELB TOT	DELC TOT	DELR TOT	DELB TOT
-.11228E 01	.17539E 00	.11530E 00	.14633E 01	-.11228E 01	.17539E 00	.14633E 01	-.11228E 01	.17539E 00	.14633E 01	-.11228E 01	.17539E 00
THETO FP	AICFP	BICFP	THETO FP	THETO FP	THETO FP	THETO FP	THETO FP	THETO FP	THETO FP	THETO FP	THETO FP
.15768E 02	.70133E 00	-.10408E 03	.17149E 02	.17149E 02	.17149E 02	.17149E 02	.17149E 02	.17149E 02	.17149E 02	.17149E 02	.17149E 02
SIGMA FP	SIGMA FP	GHMMA FS		LH10R FP							
.66979E-01	.66979E-01	.14014E 01		.14014E 01							
THPUST F	NORMAL F	SIDE F	TOFDNE F	L THUB FP	THUB FP	THUB FP	THUB FP	THUB FP	THUB FP	THUB FP	F FP
.16411E 05	.89806E 03	.25639E 03	.10079E 05	.17448E 04							
THPUST P	NORMAL P	SIDE P	TOFDNE P	L THUB FP	THUB FP	THUB FP	THUB FP	THUB FP	THUB FP	THUB FP	P FP
.16385E 05	.15186E 03	.11881E 03	.10893E 05	.15694E 04							
CT FP	CH FP	CY FP	CO FP	HO FP	H1 FP	O GOV FP					
.46904E-02	.25667E-03	.73379E-04	.19775E-03	.13429E 01	.13718E 01	.20757E 05					
CT PR	CH PR	CY PR	CO PR	HO PR	H1 PR	O GOV PR					
.48543E-02	.43401E-04	.33955E-04	.12678E-03	.14241E 01	.11129E 00	.28036E 05					
X FUSE	X SLING	LANDA SL	X F.POT	X P.POT	BD FPP						
-.10147E-04	-.12388E-04	.00000E 00	.16804E 04	.10332E 04	.10332E 04	.10332E 04	.10332E 04	.10332E 04	.10332E 04	.10332E 04	.16574E 01
Y FUSE	Y SLING	NU SL	Y F.POT	Y P.POT	THOF BOD						
.14545E 01	.00000E 00	.00000E 00	.25659E 03	-.11877E 03	-.11877E 03	-.11877E 03	-.11877E 03	-.11877E 03	-.11877E 03	-.11877E 03	.15768E 02
Z FUSE	Z SLING	MU SL	Z F.POT	Z P.POT	THOP BOD						
.34819E 03	.00000E 00	-.10255E 02	-.16350E 05	-.16354E 05	-.16354E 05	-.16354E 05	-.16354E 05	-.16354E 05	-.16354E 05	-.16354E 05	.31578E-01
L FUSE	L SLING	K BHP SL	L F.POT	L P.POT	PFP						
-.39639E 02	.00000E 00	.10135E 01	.10837E 04	-.10540E 04	-.10540E 04	-.10540E 04	-.10540E 04	-.10540E 04	-.10540E 04	-.10540E 04	.00000E 00
M FUSE	M SLING	M F.POT	M F.POT	M F.POT	M F.POT	M F.POT	M F.POT	M F.POT	M F.POT	M F.POT	OPP
-.58710E 02	.00000E 00		.32544E 06	-.32537E 06	-.32537E 06	-.32537E 06	-.32537E 06	-.32537E 06	-.32537E 06	-.32537E 06	.00000E 00
N FUSE	N SLING		N F.POT	N F.POT	N F.POT	N F.POT	N F.POT	N F.POT	N F.POT	N F.POT	PPP
-.24125E 03	.00000E 00		.36126E 05	-.25885E 05	-.25885E 05	-.25885E 05	-.25885E 05	-.25885E 05	-.25885E 05	-.25885E 05	.00000E 00
BETA FS	BETA SL	SL WHT	BETA FP	BETA PP	OPP						
-.12474E-01	.00000E 00	.75000E 04	-.12527E-01	-.12459E-01	.00000E 00						
ALPH FS	ALPH SL	J SL									HPP BODY
-.85260E 00	.26000E 01	.77711E 04									.89800E 03
VINTF	THETA SL	L SL									VPP BODY
.87476E 01	.00000E 00	.20000E 02									.11884E 03
WIFS	SMA SL	R SL									AICRR
-.89700E 01	.20000E 02	.80000E 01									.30685E-01
CONTROL FLAGS SET UP											BICRR
ISLING 0	IECSCON 0										
IDCPT 0	RSASP 0										
RSASQ 0	RSASR 0										
ISTEADY 1	NSTALL 1										
NTROCR 1	NGREFF 0										
ISLTRM 1											

TABLE 17.- STATIC TRIM DATA

$V_{eq} = 80$ knots, SAS on

CH-47B TRIM DATA PNU NO. 57											
-15:12 FEB 11. '83											
VTOT = 80.0 FT U	= 80.0 FT	V = 98.6 FT	-0.0 FT	M = 080.0 ING	N = 4.1 FT	P =	Q =	R =	S =	T =	U =
G.W. = 33000.0 LBS PPM	.24.1 H	.00000E 00	.00000E 00	.00000E 00	.00000E 00						
THETA	PHI	PSI	P	Q	R						
.29508E 01	-.24208E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00						
DELB PLT	DELS PLT	DELP PLT	DELC PLT	DELB TLT	DELP TLT						
-.20212E 01	.17539E 00	.11562E 00	.14628E 01	-.11523E 01	.11577E 00						
THETO FP	AICFP	BICFP	THETO FP	L	P						
.15768E 02	.70111E 00	-.16230E-03	.17139E 02	.34264E 05	.10159E 06						
SIGNH FP	SIGNR FP	SHINH PS		LHONH FP	CHINH FP						
.66979E-01	.66979E-01	.14014E 01		-.10278E-01	-.10278E-01						
THRUST F	NORMHL F	SIDE F	TOURQUE F	HUB FP	MEPPF F						
.16412E 05	.89011E 03	.25633E 03	.20175E 05	.15438E 04	.35471E-04						
THRUST P	NORMHL P	SIDE P	TOURQUE P	L HUG FP	MEPPF P						
.16985E 05	.15188E 03	.11877E 02	.25633E 05	.15690E 04	.10175E-04						
CT FP	CH FP	CV FP	CC FP	CD FP	CE FP						
.45905E-02	.25633E-03	.73321E-04	.13075E-03	.25429E-01	.25738E-01						
CT PP	CH PP	CV PP	CC PP	CD PP	CE PP						
.48544E-02	.43407E-04	.33946E-04	.20210E-03	.14241E-01	.11593E-01						
X FUSE	Y SLING	Z SLING	LADPH SL	C F.POT	C P.POT						
-.10147E-04	-.12388E-04	.00000E 00	.00000E 00	.16004E 04	.16332E 04	.16511E 02					
Y FUSE	Y SLING	NU SL	Y F.POT	Y P.POT	Y T						
.14545E 01	.00000E 00	.00000E 00	.25656E 03	-.11524E 03	.12514E 03						
Z FUSE	Z SLING	NU SL	Z F.POT	Z P.POT	Z T						
.34819E 03	.00000E 00	-.10255E 02	-.16350E 05	-.16564E 05	-.17151E 05						
L FUSE	L SLING	F BHF SL	L F.POT	L P.POT	L T						
-.39639E 02	.00000E 00	.10135E 01	.10333E 04	-.10534E 04	.10535E-04						
M FUSE	M SLING		M F.POT	M P.POT	M T						
-.58710E 02	.00000E 00		.32545E 06	-.72537E 06	.10115E 06						
N FUSE	N SLING		N F.POT	N P.POT	N T						
-.24125E 03	.00000E 00		.26126E 05	-.25888E 05	.14417E 05						
BETA FS	BETA SL	SL WHT	BETA FP	BETA PP							
-.12479E-01	.00000E 00	.75000E 04	-.12532E-01	-.12464E-01							
ALPH FS	ALPH SL	J SL									
-.85271E 09	.26000E 01	.77711E 04									
VINTF	THETA SL	L SL									
.87400E 01	.00000E 00	.20000E 02									
WIFS	SMA SL	P SL									
-.89704E 01	.20000E 02	.00000E 01									
CONTROL FLAGS SET UP											
ISLING 0	IECSOON 0										
IDCPT 1	PSHSP 1										
RSASD 1	PSHSP 1										
ISTEADY 1	NSTHLL 1										
NTRODR 1	NGPEFF 0										
ISLTRM 1											
VIPPF											
.00000E 00											
EFF_BUDY											
.12565E 03											
VPP_BUDY											
.11881E 03											
AICPP											
.30558E-01											
BICPP											
.30000E 01											

TABLE 18.- STATIC TRIM DATA

$V_{eq} = 100$ knots, SAS off

VINTF	THETH SL	L SL		TEP	TEP BOD	TEP GUI
.71923E 01	.00000E 00	.20000E 02		.00000E 00	.19500E 03	.39657E 02
WIFS	SMA SL	P SL				RICPR
- .72641E 01	.20000E 02	.80000E 01				.30846E 00
CONTROL FLAGS SET UP						
ISLING	0	IECSCON	0			
IDCFT	0	PSHSP	0			
PSHSQ	0	PSHSP	0			
ISTEADY	1	NSTHLL	1			
NTPOCR	1	NGREFF	0			
ISITRM	1					

TABLE 19.- STATIC TRIM DATA

$V_{eq} = 100$ knots, SAS on

CH-47B TRIM DATA FOR 100 KNOTS											
15:09 FEB 11 1985											
WTOT = 100.0 LIT U		100.0 FT	M	100.0 FT	M	100.0 FT	M	100.0 FT	M	100.0 FT	M
G.W. = 33000.0 LBS PFM	0	0	0	0	0	0	0	0	0	0	0
THE TH	PHI	POL	R	ROLL POL	THROTTLE	DEFL	DEFL	DEFL	DEFL	DEFL	DEFL
.76348E 01	-.29423E 00	.001000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
DELB PLT	DELB PLT	DELP PLT	DELC PLT	DELB PLT	DELC PLT	DELB PLT	DELC PLT	DELP PLT	DELC PLT	DELP PLT	DELC PLT
-.12958E 01	.17454E 00	.02753E 00	.04781E 01	.02753E 00	.04781E 01	.02753E 00	.04781E 01	.02753E 00	.04781E 01	.02753E 00	.04781E 01
THE T0 FP	HICFP	BICFP	THE T0 FP	100	100	100	100	100	100	100	100
.16346E 02	.35006E 00	.14399E 01	.17114E 03	.13400E 05							
SIGMA FP	SIGMA FP	GAMMA FS	LAMBDA FP	SIGMA FP	LAMBDA FP	SIGMA FP	LAMBDA FP	SIGMA FP	LAMBDA FP	SIGMA FP	LAMBDA FP
.66379E-01	.66379E-01	.14176E 01	.02566E 01	.66379E 01	.02566E 01	.66379E 01	.02566E 01	.66379E 01	.02566E 01	.66379E 01	.02566E 01
THRUST F	NORMAL F	SIDE F	TOURQUE F	L ROLL FP							
.16553E 05	.73323E 03	.19545E 03	.04937E 05	.17704E 04							
THRUST P	NORMAL P	SIDE P	TOURQUE P	L ROLL FP							
.15928E 05	-.53433E 02	.03820E 02	.09333E 05	.10103E 04							
CT FP	CH FP	CY FP	CD FP	CH FP	CH FP	CH FP	CH FP	CH FP	CH FP	CH FP	CH FP
.47308E-02	.20956E-03	.55919E-04	.027000E 03	.029000E 01							
CT FP	CH FP	CY FP	CD FP	CH FP	CH FP	CH FP	CH FP	CH FP	CH FP	CH FP	CH FP
.48382E-02	-.15357E-04	.11301E-04	.06493E-03	.01103E 01							
X FUSE	X SLING	LHMPH SL	CL F.POT	PL POT							
-.15823E-04	-.12338E-04	.00000E 00	.10657E 04	.11244E 04	.11244E 04	.11244E 04	.11244E 04	.11244E 04	.11244E 04	.11244E 04	.11244E 04
Y FUSE	Y SLING	BL SL	YL F.POT	YL F.POT	YL F.POT	YL F.POT	YL F.POT	YL F.POT	YL F.POT	YL F.POT	YL F.POT
-.19508E 01	.00000E 00	.00000E 00	.19581E 02	.01391E 02	.01391E 02	.01391E 02	.01391E 02	.01391E 02	.01391E 02	.01391E 02	.01391E 02
Z FUSE	Z SLING	ML SL	ZL F.POT	ZL F.POT	ZL F.POT	ZL F.POT	ZL F.POT	ZL F.POT	ZL F.POT	ZL F.POT	ZL F.POT
.38102E 03	.00000E 00	-.10255E 02	-.16448E 05	-.11649E 05	-.11649E 05	-.11649E 05	-.11649E 05	-.11649E 05	-.11649E 05	-.11649E 05	-.11649E 05
L FUSE	L SLING	TL BHP SL	TL F.POT	TL F.POT	TL F.POT	TL F.POT	TL F.POT	TL F.POT	TL F.POT	TL F.POT	TL F.POT
-.74345E 02	.00000E 00	.10103E 01	-.42485E 02	-.11557E 03	-.13705E 04						
M FUSE	M SLING	TM SL	TM F.POT	TM F.POT	TM F.POT	TM F.POT	TM F.POT	TM F.POT	TM F.POT	TM F.POT	TM F.POT
.23203E 04	.00000E 00		.32553E 06	-.32769E 06							
N FUSE	N SLING	TR SL	NR F.POT	NR F.POT	NR F.POT	NR F.POT	NR F.POT	NR F.POT	NR F.POT	NR F.POT	NR F.POT
-.47013E 03	.00000E 00		.02809E 05	-.027624E 05	-.027624E 05	-.027624E 05	-.027624E 05	-.027624E 05	-.027624E 05	-.027624E 05	-.027624E 05
BETA FS	BETA SL	SLIGHT	BETA FP	BETA FP	BETA FP	BETA FP	BETA FP	BETA FP	BETA FP	BETA FP	BETA FP
-.12390E-01	.00000E 00	.75000E 04	-.12453E-01	-.12338E-01							
ALPH FS	HLPH SL	J SL									
.17146E 00	.02600E 01	.77711E 04									
VINTF	THETA SL	L SL									
.71926E 01	.00000E 00	.20000E 02									
WIFS	SMA SL	R SL									
-.72644E 01	.02000E 02	.00000E 01									
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IDCPT 1	PSASCP 1										
PSASD 1	PSHSP 1										
ISTEADY 1	NSTALL 1										
NTROCP 1	NGPEFF 0										
ISLTPM 1											
VINTF	THETA SL	L SL									
.71926E 01	.00000E 00	.20000E 02									
WIFS	SMA SL	R SL									
-.72644E 01	.02000E 02	.00000E 01									
AIRCRAFT DATA											
WIFS	SMA SL	R SL									
-.72644E 01	.02000E 02	.00000E 01									
AIRCRAFT DATA											
WIFS	SMA SL	R SL									
-.72644E 01	.02000E 02	.00000E 01									

TABLE 20.- STATIC TRIM DATA

$V_{eq} = 120$ knots, SAS off

CRAFT TRIM DATA FUN NO. 57											
15:27 FEB 11, '83											
VTOT = 120.0 FT U	= 120.0 FT	V = 0.0 FT	W = 0.0 FT	U = 0.0 FT	V = 0.0 FT	W = 0.0 FT	U = 0.0 FT	V = 0.0 FT	W = 0.0 FT	U = 0.0 FT	V = 0.0 FT
G.W. = 33000.0 LBS RPM *	24.1 R	= .00000E 00	PSI	P	0	P	0	P	0	P	0
THETA	PHI	= .19842E 01	- .33413E 00	.00000E 00	,00000E 00	,00000E 00	,00000E 00	,00000E 00	,00000E 00	,00000E 00	,00000E 00
DELB.FLT	DELB.PUT	= .31433E 00	,19336E 00	- .10736E 00	,51573E 01	,19336E 00					
THETO.FP	HICFF	= .17250E 02	,38527E 01	,59000E 01	,17250E 02	,59000E 01	,17250E 02	,59000E 01	,17250E 02	,59000E 01	,17250E 02
SIGMA.FP	SIGMA.FP	= .66979E -01	,66979E -01	,14100E -01	GRNDL.FP	,14100E -01					
THRUST.F	NORTHL.F	= .16747E 05	,60640E 03	,16415E 03	TORUL.F	,16415E 03					
THRUST.P	NORTHL.P	= .16934E 05	- .22056E 03	- .30873E 03	SIDE.F	,16934E 05					
CT.FP	CH.FP	= .47964E -02	,17331E -03	,46911E -04	CO.FP	,46911E -03	,46911E -04				
CT.PP	CH.PP	= .48398E -02	- .63039E -04	- .88139E -05	CO.PP	,48398E -03	,40062E -01	,41343E -01	,41343E -01	,41343E -01	,41343E -01
Z.FUSE	Z.SLING	= .22794E 04	- .12388E 04	,001000E 00	CH.POT	,14612E 04					
Y.FUSE	Y.SLING	= .28270E 01	,00000E 00	,00000E 00	CH.POT	,16422E 03	,30794E 02	,18471E 03	,18471E 03	,18471E 03	,18471E 03
Z.FUSE	Z.SLING	= .53248E 03	,00000E 00	- .10255E 02	CH.POT	,16630E 05					
L.FUSE	L.SLING	= .11212E 03	,00000E 00	,10135E 01	CH.POT	,14564E 04	,15653E 04	,14564E 04	,14564E 04	,14564E 04	,14564E 04
M.FUSE	M.SLING	= .36774E 04	,00000E 00		CH.POT	,32689E 06	,33057E 06	,13315E 05	,13315E 05	,13315E 05	,13315E 05
N.FUSE	N.SLING	= .68976E 03	,00000E 00		CH.POT	,33844E 05	,33158E 05	,16199E 04	,16199E 04	,16199E 04	,16199E 04
BETA.FS	BETA.SL	= .11575E -01	,00000E 00	,75000E 04	BETH.FP	,11656E 01	,11575E 01	,11656E 01	,11656E 01	,11656E 01	,11656E 01
ALPH.FS	ALPH.SL	= .25088E 00	,26000E 01	,77711E 04						HPP.BOD	HPP.BOD
VINTF	THETA.SL	= .61096E 01	,00000E 00	,20000E 02						WPP.BOD	WPP.BOD
WIFS	SMA.SL	= -.61347E 01	,20000E 02	,80000E 01						WPP.BODY	WPP.BODY
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IDCPT 0	RSASP 0										
RSASD 0	RSASR 0										
ISTEADY 1	NSTALL 1										
NTROCR 1	NGREFF 0										
ISLTPM 1											

TABLE 21.- STATIC TRIM DATA

$V_{eq} = 120$ knots, SAS on

CH-47B - TRIM DATA RUN NO. 57											
15:00 FEB 11 '83											
WTOT = 120.0 + T U	= 120.1	WT	= 120.0	FT	= 120.0	TEMP = 36.0	DELT	DELT	DELT	DELT	DELT
G.W. = 33000.0 LBS RPM = 24.1	-8	PSI	-0.0000E+00								
THETA	PHI	PSE	P	Q	R	T	U	V	W	X	Y
.19923E+01	-.33620E+00	.00000E+00									
DELB PLT	DELS PLT	DELP PLT	DELU PLT	DELB TTP	DELS TTP	DELP TTP	DELU TTP	DELB TTP	DELS TTP	DELP TTP	DELU TTP
-.19628E+01	.19322E+00	-.10620E+00	.10198E+01	-.11120E+00	.11921E+01	-.11120E+00	.11921E+01	-.11120E+00	.11921E+01	-.11120E+00	.11921E+01
THETO FP	HICPR	BICPR	TRFCR FP	1	2	3	4	5	6	7	8
.17251E+02	.26623E-01	.30000E+01	.17623E+02								
SIGMA FP	SIGMA FP	SIGMA FS	GRMKA FP	1	2	3	4	5	6	7	8
.66373E-01	.66373E-01	.14185E+01	-.42751E+01	-.32751E+01							
THRUST F	NOMINAL F	SIDE F	TOPHOR F	L HUB FF	M HUB FF	N HUB FF	O HUB FF	P HUB FF	Q HUB FF	R HUB FF	S HUB FF
.16748E+05	.60655E+03	.16365E+03	.16365E+03	.16365E+04	.16365E+03						
THRUST P	NOMINAL P	SIDE P	TOPHOP P	L HUB PP	M HUB PP	N HUB PP	O HUB PP	P HUB PP	Q HUB PP	R HUB PP	S HUB PP
.16934E+05	-.22047E+03	-.71001E+03	-.30500E+03	-.16779E+04	-.16779E+03						
CT FP	CH FP	CL FP	CH FP								
.47867E+02	.17336E+03	.46772E+04	.17336E+03	.17336E+04	.17336E+03						
CT PR	CH PR	CL PR	CH PR								
.48399E+02	-.65012E+04	-.78417E+05	-.65012E+03								
X FUSE	Y SLING	Z SLING	Y F.POT								
-.32749E+04	-.12388E+04	.60000E+00	.12000E+04	.14413E+04							
Y FUSE	Y SLING	Z SLING	Y F.POT								
-.26259E+01	.00000E+00	.00000E+00	.16365E+03	.16365E+02							
Z FUSE	Z SLING	Y SLING	Z F.POT								
.53252E+03	.00000E+00	-.10255E+02	-.16637E+05								
L FUSE	L SLING	E BHP SL	L F.POT								
-.11212E+03	.00000E+00	.10135E+01	-.14637E+04								
M FUSE	M SLING		M F.POT								
.36715E+04	.00000E+00		.32691E+06	-.32691E+06							
N FUSE	N SLING		N F.POT								
-.58937E+03	.00000E+00		.58937E+05	-.58937E+05							
BETH FS	BETH SL	SLIGHT	BETH FP								
-.11637E+01	.00000E+00	.75000E+04	-.11717E+01	-.11637E+01							
ALPH FS	ALPH SL	I SL									
.24895E+00	.26000E+01	.77721E+04									
VINTF	THETA SL	L SL									
.61099E+01	.00000E+00	.20000E+02									
WIFS	SMA SL	P SL									
-.61351E+01	.20000E+02	.80000E+01									
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IDCPT 1	PSHSP 1										
PSASD 1	PSASR 1										
ISTERDY 1	NSTALL 1										
NTROCP 1	NGREFF 0										
ISLTPM 1											
VIRE	SPER BODY	DPF BODY									
.00000E+00	.16377E+03	-.31345E+02									
AICPR	BICPR										
-.71331E+00	.59938E+01										

TABLE 22.- STATIC TRIM DATA

$V_{eq} = 130$ knots, SAS off

CH-47B TRIM DATA RUN NO. 53											
15:01 FEB 11, 1983											
WTGT = 138,000 LBS	T U	+ 170,000 FT	M V	+ 29,500 FT	D D	+ 2,000 FT	W W	+ 1000 FT	Z Z	P P	R R
G.W. = 330000.0 LBS RPM = 34.1 18	F S	+ 100000F 00	E T	+ 10000T 00	C C	+ 10000C 00	G G	+ 10000G 00	I I	J J	K K
THETA	PHI	PSI	Q	Q	Q	Q	Q	Q	Q	Q	Q
.74947E 00	- .38533E 00	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
DELB FLT	DELS FLT	DELF FLT	DELC FLT	DELSL FLT	DELCI FLT	DELCI	DELCI	DELCI	DELCI	DELCI	DELCI
+.127489E 00	.109383E 00	+.109383E 00	+.109383E 00	+.109383E 00	+.109383E 00	+.109383E 00	+.109383E 00	+.109383E 00	+.109383E 00	+.109383E 00	+.109383E 00
THET0 FP	HICOFF	STOUFF	THETO FP	FP	FP	FP	FP	FP	FP	FP	FP
.17841E 00	- .10233E 00	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
SIGMA FR	SIGMA FP	GENMA FP	GENMA								
.66879E 01	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00	.100000S 00
THEFUST F	NOFLNL F	NOFLNL	THEFUST								
.14886E 05	.178013E 05	.117000E 05	.100000E 05								
THRUST P	NORMT R	TIME R									
.17114E 05	+.53451E 05	- .43700E 05	.100000E 05	.100000E 05	.100000E 05	.100000E 05	.100000E 05	.100000E 05	.100000E 05	.100000E 05	.100000E 05
CT FP	CH FP	CH FP	0 FP	0 FP	0 FP	0 FP	0 FP	0 FP	0 FP	0 FP	0 FP
.48212E 00	.122299E 05	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
CT FP	CH FP	CH FP	0 FP	0 FP	0 FP	0 FP	0 FP	0 FP	0 FP	0 FP	0 FP
.49013E 00	- .142491E 04	+.13893E 04	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000P 00	.100000Q 00	.100000R 00
X FUSE	X SLING	LAMIN	CFOT								
+.26853E 04	- .123883E 04	.100000E 00									
Y FUSE	Y SLING	NO SL	CFOT								
.11018E 00	.100000E 00	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
Z FUSE	Z SLING	NO SL	CFOT								
.88877E 03	.100000E 00	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
L FUSE	L SLING	L ERF									
-.11295E 03	.100000E 00	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
H FUSE	H SLING	H ERF									
.38182E 03	.100000E 00	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
N FUSE	N SLING	N ERF									
-.64027E 03	.100000E 00	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
BETH FS	BETH SL	SL THF	BETH FP								
-.50145E 02	.100000E 00	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
ALPH FS	ALPH SL	J SL	ALPH FP								
-.73805E 00	.100000E 01	.100000F 00	.100000T 00	.100000C 00	.100000G 00	.100000I 00	.100000J 00	.100000K 00	.100000P 00	.100000Q 00	.100000R 00
VINTF	THETA SL	L SL	WPSA								
.56652E 01	.100000E 00	.100000E 00	.100000E 00	.100000E 00	.100000E 00	.100000E 00	.100000E 00	.100000E 00	.100000E 00	.100000E 00	.100000E 00
WIFS	SMA SL	R SL	WPSA								
-.57043E 01	.120000E 02	.100000E 01	.100000E 00								
CONTROL FLAGS SET UP											
ISLING 0	IECSQN 0										
IDCPT 0	PSHSP 0										
PSASD 0	PSHSP 0										
ISTEADY 1	NSTHLL 1										
NTPOCR 1	NGREFF 0										
ISLTRN 1											

TABLE 23.- STATIC TRIM DATA

$V_{eq} = 130$ knots, SAS on

CP-476 TRIM DATA RUN NO. 57											
15:04 FEB 11 1983											
WTOT = 130,0 FT	U	- 130,0 FT	V	- 99,5 FT	W	- 130,0 FT	X	- 130,0 FT	Y	- 130,0 FT	Z
G.W. = 33000.0 LBS RPM	0	24,1	0	0	0	0	0	0	0	0	0
THETH	PHI	PST	P	O	F	PST	P	O	F	PST	P
.7443E 00	-.38364E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
DELB PLT	DELS PLT	DELP PLT	DELP PLT	DELB PLT							
-.20335E 01	.20988E 00	-.15750E 01	.15450E 01	-.15550E 02	.15550E 02						
THETO FP	WICFP	BICFP	THETO RP	E	T	THETO RP	E	T	THETO RP	E	T
.17844E 02	-.10305E 00	.00000E 01	.00000E 02	.00000E 05	.00000E 05	.00000E 02					
SIGMA FP	SIGMA RP	GRMME FS		HMLA FP	TRGME FP		HMLA FP	TRGME FP		HMLA FP	TRGME FP
.66979E-01	.66979E-01	.14013E 01		.15013E 01	.15013E 01		.15013E 01	.15013E 01		.15013E 01	.15013E 01
THRUST F	NORML F	CINE F	FORCER F	TRGME F	TRGME F	FORCER F	TRGME F	TRGME F	FORCER F	TRGME F	TRGME F
.16871E 05	.08065E 03	.11205E 03	.15444E 03								
THRUST P	NORMAL P	STIFF F	FORCER F	TRGME P	TRGME P	FORCER P	TRGME P	TRGME P	FORCER P	TRGME P	TRGME P
.17151E 05	-.52087E 02	-.47694E 02	.15065E 02	.15065E 02	.15065E 02	.15065E 02	.15065E 02	.15065E 02	.15065E 02	.15065E 02	.15065E 02
CT FP	CH FP	CY FP	CO FP	HR FP	EL FP	CT FP	CH FP	CO FP	HR FP	EL FP	CT FP
.48220E-02	.22312E-03	.48432E-04	.00000E 03	.00000E 01							
CT PP	CH PP	CY PP	CO PP	HR PP	EL PP	CT PP	CH PP	CO PP	HR PP	EL PP	CT PP
.49019E-02	-.14098E-04	-.19632E-04	.00000E 03	.00000E 01							
X FUSE	SL SING	LANDL SL	L F.POT	L F.POT	L F.POT	X FUSE	SL SING	LANDL SL	L F.POT	L F.POT	X FUSE
-.26854E 04	-.12388E 04	.00000E 00	.18688E 04	.10481E 04	.14291E 04	-.26854E 04	-.12388E 04	.00000E 00	.18688E 04	.10481E 04	-.26854E 04
Y FUSE	Y SLING	NU SL	Y F.POT	Y F.POT	Y F.POT	Y FUSE	Y SLING	NU SL	Y F.POT	Y F.POT	Y FUSE
.10949E 00	.00000E 00	.00000E 00	.18730E 03	.14746E 03	.18150E 03	.10949E 00	.00000E 00	.00000E 00	.18730E 03	.14746E 03	.10949E 00
Z FUSE	Z SLING	DO SL	Z F.POT	Z F.POT	Z F.POT	Z FUSE	Z SLING	DO SL	Z F.POT	Z F.POT	Z FUSE
.89066E 03	.00000E 00	-.10255E 02	-.16190E 05	-.17105E 05	-.17227E 05	.89066E 03	.00000E 00	-.10255E 02	-.16190E 05	-.17105E 05	.89066E 03
L FUSE	L SLING	F BHF SL	L F.POT	L F.POT	L F.POT	L FUSE	L SLING	F BHF SL	L F.POT	L F.POT	L FUSE
-.11295E 03	.00000E 00	.10135E 01	-.20374E 04	.12148E 04	-.14065E 04	-.11295E 03	.00000E 00	.10135E 01	-.20374E 04	.12148E 04	-.14065E 04
M FUSE	M SLING		M F.POT	M F.POT	M F.POT	M FUSE	M SLING		M F.POT	M F.POT	M FUSE
.25601E 03	.00000E 00		.33180E 05	-.33184E 06	.32617E 04	.25601E 03	.00000E 00		.33180E 05	-.33184E 06	.32617E 04
N FUSE	N SLING		N F.POT	N F.POT	N F.POT	N FUSE	N SLING		N F.POT	N F.POT	N FUSE
-.63670E 03	.00000E 00		.37084E 05	-.37084E 05	.37125E 04	-.63670E 03	.00000E 00		.37084E 05	-.37084E 05	.37125E 04
BETA FS	BETH SL	SL NIGHT	BETH FP	BETH FP	BETH FP	BETA FS	BETH SL	SL NIGHT	BETH FP	BETH FP	BETA FS
-.49841E-02	.00000E 00	.75000E 04	-.50250E 02	.14391E 02	.14391E 02	-.49841E-02	.00000E 00	.75000E 04	-.50250E 02	.14391E 02	-.49841E-02
ALPH FS	ALPH SL	J SL				ALPH FS	ALPH SL	J SL			ALPH FS
-.74341E 00	.26000E 01	.77711E 04				-.74341E 00	.26000E 01	.77711E 04			-.74341E 00
VINTF	THETA SL	L SL				VINTF	THETA SL	L SL			VINTF
.56659E 01	.00000E 00	.20000E 02				.56659E 01	.00000E 00	.20000E 02			.56659E 01
WIFS	SMR SL	R SL				WIFS	SMR SL	R SL			WIFS
-.57051E 01	.20000E 02	.80000E 01				-.57051E 01	.20000E 02	.80000E 01			-.57051E 01
CONTROL FLAGS SET UP											
ISLING 0	IECSCHN 0					ISLING 0	IECSCHN 0				ISLING 0
IDCPT 1	PSHSP 1					IDCPT 1	PSHSP 1				IDCPT 1
PSASD 1	PSASP 1					PSASD 1	PSASP 1				PSASD 1
ISTEADY 1	INSTALL 1					ISTEADY 1	INSTALL 1				ISTEADY 1
NTPOCP 1	NGPEFF 0					NTPOCP 1	NGPEFF 0				NTPOCP 1
ISLTRM 1						ISLTRM 1					ISLTRM 1

TABLE 24.- STATIC TRIM DATA

$V_{eq} = 0.1$ knot, SAS on
 $\Delta X_{c.g.} = 21$ in.

CH-47B TRIM DATA											
RUN ID: 57											
15:56 FEB 11, '83											
VTOT = .1 FT	U	.24.1	.1 FT	W	.96.3 FT	-1.6 FT	M	.286.0 FT	-1.6 FT	C.00	PCOF = .0
G.W. = 33000.0 LBS	PPM	.00000E 00	H	.00000E 00	P	.00000E 00	O	.00000E 00	F	.00000E 00	POOF = .0
THETA	PHI	.67078E 01	PSI	.42129E 00	R	.00000E 00	S	.00000E 00	T	.00000E 00	POOF = .0
DELB FLT	DELS FLT	.87360E 00	DELP FLT	.25159E 00	DELT FLT	.23833E 00	DELB TOT	.57564E 01	DELT TOT	.12736E 00	DELT = .0
THETO FP	AICFP	.19094E 02	BICFP	.27903E 00	THETO FP	.14998E 01	THETO FP	.10020E 02	.54400E 03	.12014E 02	.14998E 01
SIGMA FP	SIGMH FP	.66979E-01	GHMIA PS	.29563E-02	GRADLH FP	.00000E 00	GRADLH PS	.00000E 00	GRADLH FP	.00000E 00	GRADLH PS
THPUSL F	HOFTWL F	.18358E 05	SIDE F	.48220E 03	TOPDUE F	.48137E 03	TOPDUE F	.48077E 03	TOPDUE F	.48110E 03	TOPDUE F
THPUSL P	HOFTWL P	.15227E 05	SIDE P	.39713E 03	TOPDUE P	.39444E 03	TOPDUE P	.39384E 03	TOPDUE P	.39417E 03	TOPDUE P
CT FR	CH FP	.52465E-02	C FP	.13781E-02	CO FP	.25474E-04	CO FP	.14514E-03	CO FP	.14550E-01	CO FP
CT PR	CH FP	.43518E-02	C FP	.11134E-02	CO FP	.94136E-04	CO FP	.13908E-03	CO FP	.14136E-01	CO FP
X FUSE	Z SLING	.25691E 00	LANDH SL	.12388E 04	X F.POT	.00000E 00	X F.POT	.28750E 04	X F.POT	.00000E 00	X F.POT
Y FUSE	Y SLING	.21743E 00	NU SL	.00000E 00	Y F.POT	.88720E 02	Y F.POT	.29050E 03	Y F.POT	.00000E 00	Y F.POT
Z FUSE	Z SLING	.60328E 03	MU SL	.00000E 00	Z F.POT	.10255E 02	Z F.POT	.18207E 05	Z F.POT	.15162E 05	Z F.POT
L FUSE	L SLING	.23013E 00	I BHP SL	.00000E 00	L F.POT	.10135E 01	L F.POT	.85383E 04	L F.POT	.10266E 04	L F.POT
M FUSE	M SLING	.19341E 04	II BHP SL	.00000E 00	M F.POT	.62450E 06	M F.POT	.32636E 06	M F.POT	.32450E 06	M F.POT
N FUSE	N SLING	.91704E 00	III BHP SL	.00000E 00	N F.POT	.45468E 05	N F.POT	.45476E 05	N F.POT	.44486E 05	N F.POT
BETA FS	BETA SL	.49548E-01	SL WIGHT	.75000E 04	BETA FR	.49348E-01	BETA FR	.49264E-01	BETA FR	.49211E 00	BETA FR
ALPH FS	ALPH SL	.89692E 02	J SL	.26000E 01					HPP BODY	.48278E 03	HPP BODY
VINTF	THETA SL	.42252E 02	L SL	.20000E 02					WIPP BODY	.00000E 00	WIPP BODY
WIFS	SMA SL	.31295E 02	R SL	.20000E 01					YPP BODY	.00000E 00	YPP BODY
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IDCPT 1	RSASP 1										
RSASD 1	PSASP 1										
ISTEADY 1	NSTALL 1										
NTROCR 1	NGREFF 0										
ISLTRM 1											

TABLE 25.- STATIC TRIM DATA

$$V_{eq} = 80 \text{ knots, SAS on } \Delta X_{c.g.} = 21 \text{ in.}$$

TABLE 26.- STATIC TRIM DATA

$V_{eq} = 80$ knots, SAS on
 $h = +1000$ ft/min

CH-47B TRIM DATA												
RUN NO. 57												
15:51 FEB 11, 1983												
WTOT = 80.0 KT	B = 79.9 KT	M = 38.8 KT	G.C.T = 66.4 KT	10 IN PHD = 10	10 IN PHC = 10	10 IN PHR = 10	10 IN PHP = 10	10 IN PHM = 10	10 IN PHF = 10	10 IN PHG = 10	10 IN PHB = 10	10 IN PHV = 10
G.W. = 33000.0 LBS	PPM = 24.1	H = .0000E 00	F = .0000E 00	P = .0000E 00	R = .0000E 00	S = .0000E 00	T = .0000E 00	U = .0000E 00	V = .0000E 00	W = .0000E 00	X = .0000E 00	Z = .0000E 00
THETA PHI	.2540E 01	+.3443E 00	.PSI	.0000E 00								
DELB PLT	-.2030E 01	.2330E 00	DELB PLT	.7147E 00	DELB PLT	.7724E 01	.7714E 01					
THETO FP	.1784E 02	.4776E 00	EICFP	.1784E 02	THETO FP	.1784E 02						
SIGMA FP	.6697E 01	.6697E 01	SIGMA FP	.6697E 01	SIGMA FP	.6697E 01						
THRUST P	.1696E 05	.1067E 04	NOMAL P	.1696E 05	SIDE P	.1696E 05	TOPDIF P	.1696E 05	TOPDIF P	.1696E 05	TOPDIF P	.1696E 05
THRUST P	.1721E 05	.2983E 03	NOMAL P	.1721E 05	SIDE P	.1721E 05	TOPDIF P	.1721E 05	TOPDIF P	.1721E 05	TOPDIF P	.1721E 05
CT FP	.4850E 02	.2051E 02	CH FP	.4850E 02	CL FP	.4850E 02	CR FP	.4850E 02	CR FP	.4850E 02	CR FP	.4850E 02
CT FP	.4919E 02	.8527E 04	CH FP	.4919E 02	CL FP	.4919E 02	CR FP	.4919E 02	CR FP	.4919E 02	CR FP	.4919E 02
X FUSE	-.1039E 04	-.1238E 04	ISLING	.0000E 00	LNG	.0000E 00	C F.POT	.0000E 00	C F.POT	.0000E 00	C F.POT	.0000E 00
Y FUSE	-.5730E 01	.0000E 00	ISLING	.0000E 00	LNG	.0000E 00	C F.POT	-.7576E 01	C F.POT	-.7576E 01	C F.POT	-.7576E 01
Z FUSE	.1150E 04	.0000E 00	ISLING	.0000E 00	LNG	.0000E 00	C F.POT	-.1025E 05	C F.POT	-.1025E 05	C F.POT	-.1025E 05
L FUSE	-.4995E 02	.0000E 00	ISLING	.0000E 00	LNG	.0000E 00	C F.POT	-.8001E 03	C F.POT	-.8001E 03	C F.POT	-.8001E 03
M FUSE	-.1111E 05	.0000E 00	ISLING	.0000E 00	LNG	.0000E 00	C F.POT	-.1074E 06	C F.POT	-.1074E 06	C F.POT	-.1074E 06
N FUSE	.2284E 03	.0000E 00	ISLING	.0000E 00	LNG	.0000E 00	C F.POT	-.1743E 05	C F.POT	-.1743E 05	C F.POT	-.1743E 05
BETH FS	.2746E 01	.0000E 00	SLIGHT	.2746E 01	BETH FP	.2746E 01						
HLPH FS	-.8419E 01	.2600E 01	J SL	-.8419E 01								
VINTF	.9056E 01	.0000E 00	THETA SL	.0000E 00	L SL	.0000E 02						
WIFS	-.9201E 01	.2000E 02	SMA SL	.0000E 00	R SL	.0000E 01						
CONTROL FLAGS SET UP												
ISLING	0	IECSCON	0									
IDCPT	1	PSASP	1									
RSASQ	1	PSASR	1									
ISTEADY	1	NSTALL	1									
NTROCR	1	NGREFF	0									
ISLTRM	1											

TABLE 27.- STATIC TRIM DATA

$V_{eq} = 80$ knots, SAS on

$\dot{h} = -1000$ ft/min

CH-47B TRIM DATA RUN NO. 57											
15:53 FEB 11, '83											
VTOT = 80.0 FT	U	78.7 FT	V	-96.3 FT	M	14.9 FT	W	12.1 IN	ZCOS	10.1 IN	PHI = .0
G.W. = 33000.0 LBS RPM =	24.1	H	0.0000E 00	0.0000E 00	263.0 DG	1.00	0.0000E 00	.0000E 00	.0000E 00	.0000E 00	.0000E 00
THETA	PHI	Psi	P	O	P	Q	RCOS	RDOT	MDOT	RDOT	MDOT
.35195E 01	-.86624E-01	.0000E 00									
DELB PLT	DELS PLT	DELP PLT	DELP PLT	DELR TOT	DELR PLT	DELR TOT					
-.19523E 01	.12547E 00	.16644E 00	.16644E 00	-.10046E 01	-.12547E 00						
THETO FP	AICFP	BIFPF	THETO FP	P	T	U	TCOS	TDOT	TCOS	TDOT	TCOS
.13583E 02	.76309E 00	-.20219E-05	.14191E 00	.0000E 05	.0000E 00						
SIGMA FP	SIGMA FP	GAMMA FP		CHI00H FP	CHI00L FP	CHI00R FP	CHI00L FP	CHI00R FP	CHI00L FP	CHI00R FP	CHI00L FP
.66979E-01	.46970E-01	.19536E 01		-.09044E-02							
THRUST F	NORTH F	SINE F	TOPDF F	L HUB FP	L HUB FP	R HUB FP	N HUB FP	N HUB FP	P HUB FP	P HUB FP	P HUB FP
.15838E 05	.71757E 02	.10293E-03	.06330E-04	-.11171E-04							
THRUST P	NORTH P	SINE P	TOPDP P	L HUB FP	L HUB FP	R HUB FP	N HUB FP	N HUB FP	P HUB FP	P HUB FP	P HUB FP
.16841E 05	-.21849E 02	.10150E-03	.06350E-04	-.11259E-04							
CT FP	CH FP	CV FP	CO FP	RD FP	RD FP	RL FP	CL FP	CL FP	CR FP	CR FP	CR FP
.45266E-02	.20508E-03	.55144E-04	.00178E-04	.00178E-01							
CT PR	CH PR	CV PR	CO PR	RD PR	RD PR	RL PR	CL PR	CL PR	CR PR	CR PR	CR PR
.48131E-02	-.62444E-05	.29294E-04	.14193E-03	.0000E 01							
X FUSE	X SLING	LAMBDA SL	C F.POT	C P.POT	C P.POT	C P.POT	E F.POT				
-.93967E 03	-.12388E 04	.00000E 00	.10690E-04	.11195E-04							
Y FUSE	Y SLING	NU SL	C F.POT	C P.POT	C P.POT	C P.POT	E F.POT				
-.41025E 02	.00000E 00	.00000E 00	.10313E 03	-.10200E 03	-.10200E 03	-.10200E 03	.49490E-01	.49490E-01	.49490E-01	.49490E-01	.49490E-01
Z FUSE	Z SLING	NU SL	C F.POT	C P.POT	C P.POT	C P.POT	E F.POT				
-.38438E 03	.00000E 00	-.10255E 02	-.15756E 05	-.16798E 05	-.16798E 05	-.16798E 05	.72159E-02	.72159E-02	.72159E-02	.72159E-02	.72159E-02
L FUSE	L SLING	K BAR SL	L F.POT	L P.POT	L P.POT	L P.POT	E F.POT				
-.30375E 03	.00000E 00	.10135E 01	.23285E 04	-.20250E 04	-.20250E 04	-.20250E 04	.54570E-05	.54570E-05	.54570E-05	.54570E-05	.54570E-05
M FUSE	M SLING		M F.POT	M P.POT	M P.POT	M P.POT	E F.POT				
.13509E 05	.00000E 00		.31182E 06	-.32933E 06	-.32933E 06	-.32933E 06	.10000E-04	.10000E-04	.10000E-04	.10000E-04	.10000E-04
N FUSE	N SLING		N F.POT	N P.POT	N P.POT	N P.POT	E F.POT				
-.53991E 03	.00000E 00		.13833E 05	-.13296E 05	-.13296E 05	-.13296E 05	.61150E-05	.61150E-05	.61150E-05	.61150E-05	.61150E-05
BETA FS	BETA SL	SL WHT	BETA FP	BETA FP	BETA FP	BETA FP					
-.16242E-01	.00000E 00	.75000E 04	-.15978E-01	-.16217E-01	-.16217E-01	-.16217E-01					
ALPH FS	ALPH SL	J SL									
.69388E 01	.26000E 01	.77711E 04									
VINTF	THETA SL	L SL					MPP	MPP BODY	MPP BODY		
.88548E 01	.00000E 00	.20000E 02					.00000E 00	.19313E 03	.10245E 03		
WIFS	SMA SL	R SL								AICPR	BICRR
-.87440E 01	.20000E 02	.00000E 01								.28295E 00	.30001E 01
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IBCPT 1	PSHSP 1										
RSASO 1	PSHSP 1										
ISTEADY 1	NSTHLL 1										
NTROCR 1	NGPEFF 0										
ISLTPM 1											

TABLE 28.- STATIC TRIM DATA

 $V_{eq} = 75 \text{ knots, SAS on}$ $\beta = +15^\circ$

CH-47B TRIM DATA RUN NO. 57											
15:50 FEB 11, 1983											
VTOT = 75.0 FT	U	+ 72.4 FT	V	+ 18.5 FT	W	+ 0.7 FT	AP (N)	DP(N)	AP (W)	DP(W)	AP (E)
G.W. = 33000.0 LBS RPM	F	34.1 H	R	98.5 FT	T	2600 RPM	10000	10000	10000	10000	10000
THETA	PHI	PSI	P	O	R	S	PHI	PSI	PHI	PSI	PHI
.30664E 01	.34472E 01	.00000E 00									
DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT
-.16372E 01	.81068E 00	-.13829E 01	.45832E 01	-.13072E 00	.16157E 01	-.16157E 01	.16157E 01	-.16157E 01	.16157E 01	-.16157E 01	.16157E 01
THETO FP	AICFP	BICFP	THETO FP	AICFP	BICFP	THETO FP	AICFP	BICFP	THETO FP	AICFP	BICFP
.15831E 02	.16346E 01	.50270E 01	.16840E 02	.17399E 05							
SIGMA FP	SIGMA FP	GAMMA FP	SIGMA FP	SIGMA FP	GAMMA FP	SIGMA FP	SIGMA FP	GAMMA FP	SIGMA FP	SIGMA FP	SIGMA FP
.66879E-01	.66879E-01	.13676E 01									
THRUST F	NOPHIL F	SIDE F	TOPHIL F	NOPHIL F	SIDE F	TOPHIL F	NOPHIL F	SIDE F	TOPHIL F	NOPHIL F	SIDE F
.16228E 05	.81948E 03	.51863E 03	.21561E 03	.13779E 03							
THRUST R	NOPHIL R	SIDE R	TOPHIL R	NOPHIL R	SIDE R	TOPHIL R	NOPHIL R	SIDE R	TOPHIL R	NOPHIL R	SIDE R
.16632E 05	.84017E 03	-.13004E 03	.26581E 03	.12700E 03	-.11503E 03	.12700E 03	-.11503E 03	.12700E 03	-.11503E 03	.12700E 03	-.11503E 03
CT FP	CH FP	CV FP	CO FP	CH FP	CV FP	CO FP	CH FP	CV FP	CO FP	CH FP	CV FP
.46379E-02	.23421E-03	.14814E-03	.13015E-03	.19956E-03	.19956E-03	.13015E-03	.19956E-03	.13015E-03	.19956E-03	.13015E-03	.19956E-03
CT PP	CH PP	CV PP	CO PP	CH PP	CV PP	CO PP	CH PP	CV PP	CO PP	CH PP	CV PP
.47535E-02	.24070E-04	-.37167E-04	.25932E-03	.14150E-03	-.18420E-03	.14150E-03	-.18420E-03	.14150E-03	-.18420E-03	.14150E-03	-.18420E-03
X FUSE	Z SLING	L SLING	M F.POT	Z F.POT	L F.POT	M F.POT	Z F.POT	L F.POT	M F.POT	Z F.POT	L F.POT
-.90283E 03	-.12388E 04	.00000E 00	.16200E 04								
Y FUSE	Z SLING	H SLING	N F.POT	Z F.POT	L F.POT	M F.POT	Z F.POT	L F.POT	M F.POT	Z F.POT	H F.POT
-.23691E 04	.00000E 00	.00000E 00	.28435E 03	.11034E 03							
Z FUSE	Z SLING	H SLING	C F.POT	Z F.POT	C F.POT	C F.POT	Z F.POT	C F.POT	C F.POT	Z F.POT	C F.POT
-.12257E 03	.00000E 00	-.10255E 02	-.16173E 05								
L FUSE	L SLING	F BAF SL	L F.POT	F BAF SL							
-.42770E 04	.00000E 00	.10135E 01	.13956E 04	.12878E 04							
M FUSE	H SLING	H SLING	I F.POT	H F.POT	I F.POT						
-.33965E 04	.00000E 00	.00000E 00	.32278E 06	-.31954E 06	.32278E 06						
N FUSE	H SLING	H SLING	N F.POT	H F.POT	N F.POT						
-.12290E 04	.00000E 00	.00000E 00	.27219E 05	-.28442E 05	.27219E 05						
BETA FS	BETA SL	SL LIGHT	BETH FR								
.15167E 02	.00000E 00	.75000E 04	.15261E 02	.15164E 02							
ALPH FS	ALPH SL	J SL								HPP BODY	HPP BODY
-.22836E 01	.26000E 01	.77711E 04								.93701E 03	.42736E 02
VINTF	THETA SL	L SL								VPP BODY	VPP BODY
.87069E 01	.00000E 00	.20000E 02								.26435E 03	-.14755E 03
WIFS	SMA SL	P SL								AICPP	BICPP
-.94411E 01	.20000E 02	.80000E 01								-.76565E 00	.29372E 01
CONTROL FLAGS SET UP											
ISLING	0	IECSOM	0								
IDCPT	1	RSHSP	1								
RSASD	1	RSASR	1								
ISTEADY	1	NSTALL	1								
HTROCR	1	NGPEFF	0								
ISLTRM	1										

TABLE 29.- STATIC TRIM DATA

$V_{eq} = 75$ knots, SAS on

$\beta = -15^\circ$

CH-47B TRIM DATA P/N NO. 1											
19:26 FEB 22, '83											
VTOT = 75.0 FT U	= 72.4 FT	V = 49.7 FT	W = 030.0 TS	S,5 + T							
G.W. = 33000.0 LBS RPM = 24.1 H	= 36.5 FT RPM = 030.0 TS	T,0 S +									
THETHA PHI PSI P D E F RHO DMGRFF DRGRFF	.30659E-01 -.40507E-01 .00000E+00 .00000E+00 .41160E-01 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00										
DELB PLT DELB PLT DELB FT DELB PLT DELB TOT	.17022E-01 -.47153E-01 .14101E-01 .49553E-01 -.47153E-01 -.47153E-01 .14101E-01 .49553E-01 -.47153E-01 .14101E-01 .49553E-01 .47153E-01										
THETO FR HICFR BICFR THETO FR	.15293E-02 -.82239E-02 -.21844E-02 .15293E-02 -.15293E-02 -.15293E-02 -.21844E-02 .15293E-02 -.15293E-02 -.21844E-02 .15293E-02 -.15293E-02										
SIGMA FR SIGMA FR GAMA TS	.66979E-01 .86979E-01 .18697E-01										
THRUST F HORIZONTAL F SIDE F TORQUE F C ID F	.16205E-05 .09337E-05 -.13331E-05 .12192E-05 .14165E-05 .14165E-05 .14165E-05 .14165E-05 .14165E-05 .14165E-05 .14165E-05 .14165E-05										
THRUST P HORIZONTAL P SIDE P TORQUE P C ID P	.16589E-05 .14050E-05 .14717E-05 .15170E-05 .15170E-05 .15170E-05 .15170E-05 .15170E-05 .15170E-05 .15170E-05 .15170E-05 .15170E-05										
CT FR CH FR CV FR TO FP HO FP HI FR CT FR CH FR CV FR TO FP HO FP HI FR CT FR CH FR CV FR TO FP HO FP HI FR	.46316E-02 .25533E-03 -.13490E-04 .10067E-03 .10067E-03 .10067E-03 .10067E-03 .10067E-03 .10067E-03 .10067E-03 .10067E-03 .10067E-03										
CT PR LH PR CT PR EO PR HO PR HI PR CT PR LH PR CT PR EO PR HO PR HI PR CT PR LH PR CT PR EO PR HO PR HI PR	.47639E-02 .30495E-04 .78660E-04 .10562E-05 .10562E-05 .10562E-05 .10562E-05 .10562E-05 .10562E-05 .10562E-05 .10562E-05 .10562E-05										
X FUSE II SLING LAMBDA SL II F.POT	-.88404E-03 .80000E-00 .100000E-00 .14521E-04 .14521E-04 .14521E-04 .14521E-04 .14521E-04 .14521E-04 .14521E-04 .14521E-04 .14521E-04										
Y FUSE V SLING MU SL V F.POT	.24190E-04 .00000E-00 .100000E-00 .11173E-03 .11173E-03 .11173E-03 .11173E-03 .11173E-03 .11173E-03 .11173E-03 .11173E-03 .11173E-03										
Z FUSE Z SLING MU SL Z F.POT	-.62575E-02 .00000E-00 .100000E-00 -.16144E-05 -.16144E-05 -.16144E-05 -.16144E-05 -.16144E-05 -.16144E-05 -.16144E-05 -.16144E-05										
L FUSE L SLING L BPL SL L F.POT	.37516E-04 .00000E-00 .100000E-00 -.96409E-03 -.96409E-03 -.96409E-03 -.96409E-03 -.96409E-03 -.96409E-03 -.96409E-03 -.96409E-03										
M FUSE M SLING MU SL M F.POT	-.22225E-04 .00000E-00 .100000E-00 .32130E-06 .32130E-06 .32130E-06 .32130E-06 .32130E-06 .32130E-06 .32130E-06 .32130E-06										
N FUSE N SLING MU SL N F.POT	-.46051E-03 .00000E-00 .100000E-00 .273447E-05 .273447E-05 .273447E-05 .273447E-05 .273447E-05 .273447E-05 .273447E-05 .273447E-05										
BETH FS BETH SL SL LIGHT BETH FR BETH RH	-.15182E-02 .00000E-00 .75000E-04 -.15038E-02 -.15182E-02 -.15182E-02 .15038E-02 .15182E-02 .15038E-02 .15182E-02 .15038E-02 .15182E-02										
ALPH FS ALPH SL J SL ALPH BPL	-.24396E-01 .00000E-00 .77711E-04 .00000E-00 .00000E-00 .00000E-00 .00000E-00 .00000E-00 .00000E-00 .00000E-00 .00000E-00 .00000E-00										
VINTF THETA SL L SL WIPR WIPR BODY YIPR BODY	.36814E-01 .80000E-00 .20000E-02 .00000E-00 .11075E-03 .26644E-03										
WIFS SMA SL P SL AICPR BICPR	-.94229E-01 .20000E-02 .80000E-01 .52634E-00 .29529E-01										
CONTROL FLAGS SET UP											
ISLING 0 IEDCON 0											
IDCFT 1 PSASP 1											
PSASD 1 PSASP 1											
ISTEADY 1 NSTALL 1											
NTPOCP 1 NGREFF 0											
ISLTPII 0											

TABLE 30.- STATIC TRIM DATA

$V_{eq} = 75$ knots, SAS on
Coordinated, level turn $\phi = +30^\circ$

CH-47B TRIM DATA RUN NO. 1											
19:48 FEB 22, '83											
VTOT = 75.1 KT	U	= 75.1 KT	V	= 1.4 KT	W	= 4.2 KT	.0 IN	DZCG	.0 IN	PHR	= .0
G.W. = 33000.0 LBS RPM	= 24.1	H	= 98.4 FT	TEMP =	288.0 DG	TROG =					
THETA	PHI	PSI	P	O	R	PHB	OMEGA FP	OMEGA RP			
.32988E 01	.29980E 02	.00000E 00	-.93015E-02	.72680E-01	.12631E-01	.20711E-02	.23950E-01	.2412E-02			
DELB PLT	DELS PLT	DELF PLT	SELG PLT	DELB TOT	DELS TOT	DELF TOT	DELB TOT	DELS TOT	H DOT		
-.19848E 01	.22591E 00	.55957E-01	.51250E 01	-.11717E 01	.18410E 00	.17498E 00	.51550E 01	-.24155E-01			
THETO FP	AICFP	BICFP	THETO RP	OIC	OIC	1.0	1.0	1.0	I.PPF > R		
.16680E 02	.10280E 01	-.32338E 00	.18120E 02	.34100E 05	.20000E 05	.17000E 05	.14400E 05	.13443E 05	.13443E 05		
SIGMA FP	SIGMA RP	SIMH FS		LAMDA FP	1.4010E 00	1.1110E 00	1.1110E 00	1.1110E 00	1.1110E 00	MATH 901	
.66979E-01	.66979E-01	.13754E 01		-.34529E-01	-.42110E-01	.11100E 00	.11100E 00	.11100E 00	.11100E 00		
THRUST F	NORMAL F	SIDE F	TORQUE F	L HNB FP	M HNB FP	N HNB FP	O HNB FP	P HNB FP	Q HNB FP	R HNB FP	
.19320E 05	.10798E 04	.35786E 03	.29089E 05	.12606E 04	.14311E 04						
THRUST P	NORMAL P	SIDE P	TOPLOS P	L HNB FP	M HNB FP	N HNB FP	O HNB FP	P HNB FP	Q HNB FP	R HNB FP	
.19577E 05	.21476E 07	.12875E 03	.34113E 05	.10172E 04	.14311E 04						
CT FP	LH FP	CH FP	CO FP	CH FP							
.54644E-02	.31186E-03	.10336E-03	.74156E-03	.14140E-01	.129541E-01	.129541E-01	.129541E-01	.129541E-01	.129541E-01	.129541E-01	
CT PP	CH PP	CY PP	CO PP	CH PP							
.55367E-02	.60738E-04	.36417E-04	.34160E-03	.140511E 01	.139075E 01						
X FUSE	X SLING	LADHR SL	O FLPDT								
-.90882E 03	.00000E 00	.00000E 00	.18603E 04	.11513E 04	.11513E 04	.106711E 04				.13317E 01	.11703E 01
Y FUSE	Y SLING	MU SL	O FLPDT								
-.19110E 03	.00000E 00	.00000E 00	.31559E 03	-.12665E 03	-.14051E 03	.10686E 02					
Z FUSE	Z SLING	MU SL	C FLPDT								
.38254E 03	.00000E 00	.00000E 00	-.10863E 05	-.19544E 05	-.19544E 05	-.17709E 05	-.19544E 05	-.19544E 05	-.19544E 05	-.19544E 05	.18120E 02
L FUSE	L SLING	F BAF SL	L FLPDT								
-.31229E 03	.00000E 00	.00000E 00	.12029E 04	-.19924E 03	-.19924E 03	-.18486E 03	-.19924E 03	-.19924E 03	-.19924E 03	-.19924E 03	.14306E-01
M FUSE	M SLING		O FLPDT								
-.12638E 04	.00000E 00		.37556E 06	-.37435E 06	-.37435E 06	-.35483E 06	-.37435E 06	-.37435E 06	-.37435E 06	-.37435E 06	.12388E-01
N FUSE	N SLING		O FLPDT								
.15062E 03	.00000E 00		.31665E 05	-.31708E 05	-.31708E 05	-.30787E 05	-.31708E 05	-.31708E 05	-.31708E 05	-.31708E 05	-.40942E-03
BETH FS	BETH SL	SL LIGHT	BETH FP	LCTR FP							
.10694E 01	.00000E 00	.75000E 04	.22287E 01	-.31335E 01							
ALPH FS	ALPH SL	J SL									
-.17776E 01	.00000E 00	.77711E 04									
VINTF	THETA SL	L SL									
-.10659E 02	.00000E 00	.20000E 02									
WIFS	SMA SL	R SL									
-.11025E 02	.20000E 02	.80000E 01									
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IDCPT 1	PSRGF 1										
PSASD 1	PSASR 1										
ISTEADY 0	NSTALL 1										
HTROCR 1	NGPEFF 0										
ISLTRM 0											

TABLE 31.- STATIC TRIM DATA

$V_{eq} = 75$ knots, SAS on
Coordinated, level turn $\phi = -30^\circ$

CH-47B TRIM DATA RUN NO. 1												
19:52 FEB 22, '83												
VTOT = 75.1 KT	U	75.1 KT	V	1.4 KT	W	4.2 KT						
G.W. = 33000.0 LBS RPM *	24.1	H	98.9 FT	TEMP =	288.0 DG	DMG =	.0 IN	DZDG =	.0 IN	PHR =	.0	
THETA	PHI	PSI	P	O	R	PHD	OMEGA FR	OMEGA PR				
.22435E 01	-.29912E 02	.00000E 00	.57015E-02	.73042E-01	-.12631E 00	.23703E-02	.24711E 02	.23959E 02				
DELB PLT	DELS PLT	DELP PLT	DELC PLT	DELB TOT	DELS TOT	DELP TOT	DELC TOT	H DOT				
-.21801E 01	.23625E 00	.46082E-02	.51301E 01	-.13670E 01	.23530E 00	.12131E 00	.51301E 01	-.17163E-02				
THETO FP	AICFR	BICFP	THETO FP	IXX	ITY	IIC	IIC	IIC				
.16551E 02	.82479E 00	-.37030E 00	.18233E 02	.54000E 05	.20258E 05	.19409E 05	.14500E 05	.17642E 05				
SIGMA FR	SIGMA PR	GRMHR FS		THMHR FP	LHMHR FP	THMHR FP	THMHR FP	THMHR FP				
.66979E-01	.66979E-01	.13751E 01		-.34143E-01	-.42171E-01	.17370E 00	.17370E 00	.17370E 00				
THRUST F	NOMINAL F	SIDE F	TOPQUE F	L HUB FP	M HUB FP	N HUB FP	O TIP FP	P TIP FP	F PS			
.18930E 05	.10466E 04	.52271E 03	.24843E 05	.28730E 04	.42630E 04	.37130E 04	.11171E 03	.11171E 03	.25459E 03			
THRUST P	NOMINAL P	SIDE P	TOPQUE P	L HUB FP	M HUB FP	N HUB FP	O TIP FP	P TIP FP	F PR			
.19593E 05	.24384E 03	.11971E 03	.34165E 05	.17509E 04	.54414E 02	.17140E 03	.11185E 03	.11185E 03	.34412E 03			
CT FR	CH FR	CY FR	CO FR	CD FR	CI FR	CT FR	CD FR	CI FR	CH FR			
.53566E-02	.30168E-03	.91276E-04	.23423E-03	.46367E-01	.15817E-01	.15449E-01	.15449E-01	.15449E-01	.15449E-01			
CT PR	CH PR	CY PR	CO PR	CD PR	CI PR	CT PR	CD PR	CI PR	CH PR			
.56592E-02	.76427E-04	.34576E-04	.32889E-03	.50370E-01	.177517E-01	.14037E-01	.134105E-01	.134105E-01	.134105E-01			
X FUSE	X SLING	LANDA SL	X F.POT	X P.POT	X R.POT	X S	X T	X U	X V			
-.30882E 03	.00000E 00	.00000E 00	.19096E 04	.11081E 04	.20072E 04					.420294E-01	.17098E 01	
Y FUSE	Y SLING	NU SL	Y F.POT	Y P.POT	Y R.POT	Y T	Y U	Y V	Y W			
-.19110E 03	.00000E 00	.00000E 00	.32418E 03	-.12883E 03	.14140E-02	.40364E 00	.40364E 00	.40364E 00	.40364E 00	.16551E 02		
Z FUSE	Z SLING	MU SL	Z F.POT	Z P.POT	Z R.POT	Z T	Z U	Z V	Z W			
.38317E 03	.00000E 00	.00000E 00	-.18272E 05	-.19562E 05	-.13712E 05	.42746E 02	.42746E 02	.42746E 02	.42746E 02	.16338E 02		
L FUSE	L SLING	K BAR SL	L F.POT	L P.POT	L R.POT	L T	L U	L V	L W			
-.31214E 03	.00000E 00	.00000E 00	.13911E 04	-.97439E 03	.12230E 02	.29842E 04	.29842E 04	.29842E 04	.29842E 04	.17591E 04	.41422E-01	
M FUSE	M SLING		M F.POT	M P.POT	M R.POT	M T	M U	M V	M W			
-.12698E 04	.00000E 00		.37551E 06	-.37436E 06	-.37436E 06	.61451E-03	.61451E-03	.61451E-03	.61451E-03	.73402E-01	.73402E-01	
N FUSE	N SLING		N F.POT	N P.POT	N R.POT	N T	N U	N V	N W			
.15061E 03	.00000E 00		.31612E 05	-.31829E 05	-.31829E 05	.34973E-03	.34973E-03	.34973E-03	.34973E-03	.42128E 00	.36136E-03	
BETA FS	BETH SL	SL WHT	BETA FP	BETA FP	BETA FP					B1FF BOD	B1FF BOD	PPR
.10694E 01	.00000E 00	.75000E 04	-.79001E-01	.21542E 01					.19470E 01	.13128E 01	.73108E-01	
ALPH FS	ALPH SL	J SL							HFF BODY	HFF BODY	PPR	
-.17825E 01	.00000E 00	.77711E 04							.10661E 04	.24818E 03		
VINTF	THETA SL	L SL				WIPR	WIPR BODY	WIPR BODY				
.10673E 02	.00000E 00	.20000E 02				.00000E 00	.32419E 03	.11041E 03				
WIFS	SMA SL	R SL								AICRR	BICRR	
.11036E 02	.20000E 02	.80000E 01							.61544E-01	.26304E 01		
CONTROL FLAGS SET UP												
#SLING # TELSONCON #												
IDCPT 1	PSASP 1											
PSASD 1	PSASR 1											
ISTEADY 1	NSTALL 1											
NTROCR 1	NGREFF 0											
ISLTPM 0												

TABLE 32.- STATIC TRIM DATA

$V_{eq} = 0.1$ knot, SAS on
Gross weight = 22,000 lb

CH-47C TRIM DATA											
F06 Rev. 37											
15:58 FEB 11, 83											
VTOT = .1 FT U	.041	.1 FT R	.041	.1 FT D	.041	.1 FT L	.041	.1 FT ROLL	.041	.1 FT PITCH	.041
G.W. = 22000.0 LBS FPM =											
THETA	PHI	Psi	P	ROLL	PITCH	YAW	CDP	CDFP	CDP	CDFP	CDP
.66128E 01	-.34981E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
DELB PLT	DELS PLT	DELP PLT	DELP PLT								
-.10606E 01	.17989E 00	-.23663E 00	.14400E 00	-.14400E 00	.14400E 00						
THET0 FP	AICFP	BICFP	TIDE0 FP	TD0 FP	TD0 FP	TD0 FP	TD0 FP	TD0 FP	TD0 FP	TD0 FP	TD0 FP
.16103E 02	.33233E 00	-.15007E 01	-.11313E 01	.11313E 01	-.11313E 01	.11313E 01	-.11313E 01	.11313E 01	-.11313E 01	.11313E 01	-.11313E 01
SIGMA FP	SIGH FP	GHIGH FP	SIGH FP	SIGH FP	SIGH FP	SIGH FP	SIGH FP	SIGH FP	SIGH FP	SIGH FP	SIGH FP
.66979E 01	.66979E 01	.56310E 01	.56310E 01								
THRUST F	HORIZONTAL F	SIDE F	HORIZONTAL F	SIDE F	HORIZONTAL F	SIDE F	HORIZONTAL F	SIDE F	HORIZONTAL F	SIDE F	HORIZONTAL F
.11246E 05	.29524E 03	-.67917E 03	.29524E 03								
THPUSL F	HORIZONTAL P	SIDE F	THPUSL F								
.11126E 05	-.29048E 03	-.67917E 03	-.29048E 03								
CT FP	CH FP	CV FP	CD FP	CP FP	CR FP	CL FP	CDP FP	CDP FP	CDP FP	CDP FP	CDP FP
.32141E 02	.84376E 04	-.19643E 04	-.19344E 03	.19344E 03	-.19344E 03						
CT PP	CH PP	CV PP	CD PP	CP PP	CR PP	CL PP	CDP PP	CDP PP	CDP PP	CDP PP	CDP PP
.31737E 02	-.83016E 04	-.19442E 04	.25050E 03	-.25050E 03	.25050E 03						
X FUSE	C SLING	LANDA SL	C FUPOT	C FUPOT	C FUPOT						
-.20441E 00	-.12388E 04	.00000E 00	-.14672E 04	.16059E 04	-.14672E 04						
Y FUSE	C SLING	NO SL	C FUPOT	C FUPOT	C FUPOT						
.13716E 00	.00000E 00	.00000E 00	-.16502E 02	.26179E 02	-.16502E 02						
Z FUSE	C SLING	NO SL	Z FUPOT	Z FUPOT	Z FUPOT						
.38017E 03	.00000E 00	-.10255E 02	-.11154E 05	-.11154E 05	-.11154E 05						
L FUSE	L SLING	L BHPL SL	L FUPOT	L FUPOT	L FUPOT						
.13943E 00	.00000E 00	.10135E 01	-.31803E 04	.31520E 04	-.31803E 04						
M FUSE	M SLING	M BHPL SL	M FUPOT	M FUPOT	M FUPOT						
.55240E 03	.00000E 00	-.21909E 06	-.21909E 06								
N FUSE	N SLING	N BHPL SL	N FUPOT	N FUPOT	N FUPOT						
-.38400E 00	.00000E 00	-.27666E 05	-.27666E 05								
BETA FS	BETA SL	SL MNGT	BETA FP	BETA FP	BETA FP						
-.40555E 01	.00000E 00	.75000E 04	-.40518E 01	.40518E 01	-.40518E 01						
ALPH FS	ALPH SL	J SL									
-.89615E 02	.26000E 01	.77711E 04									
VINTF	THETA SL	L SL									
.33558E 02	.00000E 00	.20000E 02									
WIFS	SMA SL	R SL									
-.24856E 02	.20000E 02	.80000E 01									
CONTROL FLAGS SET UP											
ISLING 0	IECSCON 0										
IDCFT 1	RSHSP 1										
RSHSO 1	RSHSR 1										
ISTERDY 1	NSTALL 1										
HTROCR 1	NGREFF 0										
ISLTRM 1											

TABLE 33.- STATIC TRIM DATA

$V_{eq} = 80$ knots, SAS on
Gross weight = 22,000 lb

TH-475 TERM DATA											
TERM NO. 50											
15:59 FEB 11 1983		VTTOT = 80.0 FT U		G.W. = 20000.0 LBS PPN = 24.1 H		W = 200.0 FT		E = 200.0 FT		N = 200.0 FT	
THETH	PHI	Psi 1	Psi	THETH	PHI	THETH	PHI	THETH	PHI	THETH	PHI
.28229E-01	-.22475E-00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
DELB PLT	DELS PLT	DELP PLT	DELP PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB PLT
-.15087E-01	.14963E-00	.17120E+00	.17120E+00	.15087E-01	.14963E-00	.17120E+00	.17120E+00	.15087E-01	.14963E-00	.17120E+00	.17120E+00
THETO FP	ALCFP	BLFP	BLFP	THETO FP	ALCFP	THETO FP	ALCFP	THETO FP	ALCFP	THETO FP	ALCFP
.14073E-02	.49076E-00	-.10496E-00	.10496E-00	.14073E-02	.49076E-00	.10496E-00	.10496E-00	.14073E-02	.49076E-00	.10496E-00	.10496E-00
SIGMA FP	SIGMIFP	GREENFS	GREENFS	SIGMA FP	SIGMIFP	SIGMA FP	SIGMIFP	SIGMA FP	SIGMIFP	SIGMA FP	SIGMIFP
.66979E-01	.66979E-01	.14115E-01	.14115E-01	.66979E-01	.66979E-01	.14115E-01	.14115E-01	.66979E-01	.66979E-01	.14115E-01	.14115E-01
THRUST F	NORMF	CABR F	CABR F	THRUST F	NORMF	THRUST F	NORMF	THRUST F	NORMF	THRUST F	NORMF
.11024E-05	.48317E-03	.11027E-03	.11027E-03	.11024E-05	.48317E-03	.11027E-03	.11027E-03	.11024E-05	.48317E-03	.11027E-03	.11027E-03
THRUST P	NORMF	SLINP	SLINP	THRUST P	NORMF	THRUST P	NORMF	THRUST P	NORMF	THRUST P	NORMF
.11277E-05	-.66565E-02	.12337E-02	.12337E-02	.11277E-05	-.66565E-02	.12337E-02	.12337E-02	.11277E-05	-.66565E-02	.12337E-02	.12337E-02
CT FP	CH FP	CV FP	CV FP	CT FP	CH FP	CT FP	CH FP	CT FP	CH FP	CT FP	CH FP
.31507E-02	.13339E-03	.31633E-03	.31633E-03	.31507E-02	.13339E-03	.31633E-03	.31633E-03	.31507E-02	.13339E-03	.31633E-03	.31633E-03
CT PP	CH PP	CV PP	CV PP	CT PP	CH PP	CT PP	CH PP	CT PP	CH PP	CT PP	CH PP
.32229E-02	-.17390E-04	.16617E-04	.16617E-04	.32229E-02	-.17390E-04	.16617E-04	.16617E-04	.32229E-02	-.17390E-04	.16617E-04	.16617E-04
X FUSE	.. SLING	CHINR SL	CHINR SL	X FUSE	.. SLING	X FUSE	.. SLING	X FUSE	.. SLING	X FUSE	.. SLING
-.10111E-04	-.12588E-04	.00000E+00	.00000E+00	-.10111E-04	-.12588E-04	.00000E+00	.00000E+00	-.10111E-04	-.12588E-04	.00000E+00	.00000E+00
Y FUSE	.. SLING	HU SL	HU SL	Y FUSE	.. SLING	Y FUSE	.. SLING	Y FUSE	.. SLING	Y FUSE	.. SLING
-.12590E-01	.00000E+00	.00000E+00	.00000E+00	-.12590E-01	.00000E+00	.00000E+00	.00000E+00	-.12590E-01	.00000E+00	.00000E+00	.00000E+00
Z FUSE	.. SLING	HU SL	HU SL	Z FUSE	.. SLING	Z FUSE	.. SLING	Z FUSE	.. SLING	Z FUSE	.. SLING
.23562E-03	.00000E+00	-.10255E-02	.10064E-09	.23562E-03	.00000E+00	-.10255E-02	.10064E-09	.23562E-03	.00000E+00	.00000E+00	.00000E+00
L FUSE	.. SLING	E BHF SL	E BHF SL	L FUSE	.. SLING	E BHF SL	E BHF SL	L FUSE	.. SLING	E BHF SL	E BHF SL
-.50114E-02	.00000E+00	.10135E-01	-.12134E-02	-.50114E-02	.00000E+00	.10135E-01	-.12134E-02	-.50114E-02	.00000E+00	.10135E-01	-.12134E-02
M FUSE	.. SLING			M FUSE	.. SLING			M FUSE	.. SLING		
.16501E-04	.00000E+00			.16501E-04	.00000E+00			.16501E-04	.00000E+00		
N FUSE	.. SLING			N FUSE	.. SLING			N FUSE	.. SLING		
-.30618E-03	.00000E+00			-.30618E-03	.00000E+00			-.30618E-03	.00000E+00		
BETH FS	BETH SL	CL NIGHT	CL NIGHT	BETH FS	BETH SL	CL NIGHT	CL NIGHT	BETH FS	BETH SL	CL NIGHT	CL NIGHT
-.11082E-01	.00000E+00	.75000E-04	-.11113E-01	-.11082E-01	.00000E+00	.75000E-04	-.11113E-01	-.11082E-01	.00000E+00	.75000E-04	-.11113E-01
ALPH FS	ALPH SL	J SL	J SL	ALPH FS	ALPH SL	J SL	J SL	ALPH FS	ALPH SL	J SL	J SL
.25971E-00	.26000E-01	.77711E-04		.25971E-00	.26000E-01	.77711E-04		.25971E-00	.26000E-01	.77711E-04	
VINTF	THETH SL	L SL		VINTF	THETH SL	L SL		VINTF	THETH SL	L SL	
.59853E-01	.00000E+00	.20000E-02		.59853E-01	.00000E+00	.20000E-02		.59853E-01	.00000E+00	.20000E-02	
WIFS	SMA SL	R SL		WIFS	SMA SL	R SL		WIFS	SMA SL	R SL	
.60468E-01	.20000E-02	.00000E+01		.60468E-01	.20000E-02	.00000E+01		.60468E-01	.20000E-02	.00000E+01	
CONTROL FLAGS SET UP											
ISLING 0	IECSQN 0			ISLING 0	IECSQN 0			ISLING 0	IECSQN 0		
IDEPT 1	PSASF 1			IDEPT 1	PSASF 1			IDEPT 1	PSASF 1		
PSASD 1	PSASP 1			PSASD 1	PSASP 1			PSASD 1	PSASP 1		
ISTEADY 1	NSTHLL 1			ISTEADY 1	NSTHLL 1			ISTEADY 1	NSTHLL 1		
NTRODR 1	NGREFF 0			NTRODR 1	NGREFF 0			NTRODR 1	NGREFF 0		
ISLTPM 1				ISLTPM 1				ISLTPM 1			

TABLE 34.- STABILITY AND CONTROL DERIVATIVES, $V_{eq} = 0.1$ KNOT.

	L	M	N	X	Y	Z
SAS off						
δ_B	-0.34640E-01	0.32816E 00	0.54072E-01	0.57000E-01	-0.48486E-03	0.49865E-01
δ_A	.48630E 00	.74250E-05	.97491E-02	.10006E-04	.10917E 01	-.76234E-04
δ_R	-.12634E 00	.00000E 00	.19269E 00	-.47646E-06	.98684E-02	.00000E 00
δ_C	-.17040E-01	-.14318E-02	-.55263E-03	.98157E 00	.65680E-01	-.84737E 01
p	-.12795E 01	.29530E-01	-.14808E-01	.42600E-01	-.28362E 01	-.12520E 00
q	.87128E-01	-.10973E 01	-.13378E 00	.27807E 01	-.73125E-02	-.26472E 00
r	-.90288E 01	-.26861E 00	-.89168E-01	-.15904E 00	-.33045E 00	-.52506E-01
u	-.53257E-03	.11090E-01	.73452E-03	-.19998E-01	-.27807E-03	.31149E-01
v	-.10771E-01	.94978E-05	.58132E-03	-.45945E-03	-.10704E 00	.40019E-02
w	.39976E-03	.63815E-03	.42493E-04	.30085E-01	.22338E-02	-.29831E 00
SAS on						
δ_B	-0.34638E-01	0.32817E 00	0.54074E-01	0.56998E-01	-0.47325E-03	0.49895E-01
δ_A	.48630E 00	.61875E-06	.97481E-02	-.47646E-06	.10917E 01	.00000E 00
δ_R	-.12634E 00	.61875E-06	.19269E 00	.00000E 00	.98734E-02	-.76234E-05
δ_C	-.17013E-01	-.14349E-02	-.54782E-03	.98214E 00	.65751E-01	-.84789E 01
p	-.21634E 01	.29517E-01	-.22771E-01	.42658E-01	-.48053E 01	-.12531E 00
q	.86503E-01	-.10992E 01	-.13382E 00	.27653E 01	-.84882E-02	-.11685E 00
r	.59843E-01	-.26865E 00	-.32381E 00	-.15908E 00	-.35487E 00	-.52430E-01
u	-.53341E-03	.11090E-01	.73457E-03	-.20019E-01	-.27930E-03	.31343E-01
v	-.10786E-01	.86934E-05	.60258E-03	-.45872E-03	-.10704E 00	.39943E-02
w	.39204E-03	.64854E-03	.40124E-04	.29589E-01	.22011E-02	-.29380E 00

TABLE 35.- STABILITY AND CONTROL DERIVATIVES, $V_{eq} = 20$ KNOTS.

	L	M	N	X	Y	Z
SAS off						
δ_B	-0.10461E-01	0.33548E 00	0.52540E-01	0.42182E-01	0.63174E-01	0.25168E 00
δ_A	.48558E 00	-.21656E-04	.86124E-02	.93387E-04	.10867E 01	-.10444E-02
δ_R	-.13097E 00	.21038E-03	.19173E 00	-.72899E-04	-.77150E-02	.12274E-02
δ_C	-.21810E-01	-.83005E-02	.20635E-02	.72384E 00	.53387E-01	-.84539E 01
p	-.88622E 00	.17136E-01	-.58689E-02	.27653E-01	-.15122E 01	-.10570E 00
q	.23866E-01	-.16339E 01	-.15186E 00	.28998E 01	-.15524E 00	-.27731E 01
r	-.64698E-01	-.24771E 00	-.76432E-01	-.11116E 00	-.20182E 00	.17641E 00
u	.36675E-03	.15577E-01	.93359E-03	-.12844E-01	.20535E-02	-.40523E-01
v	-.87699E-02	-.87330E-03	.23044E-03	.14363E-03	-.46031E-01	.44315E-02
w	.83370E-03	.16648E-01	.71363E-03	.26766E-01	.43533E-02	-.28244E 00
SAS on						
δ_B	-0.10458E-01	0.33549E 00	0.52542E-01	0.42205E-01	0.63190E-01	0.25147E 00
δ_A	.48558E 00	.50737E-04	.86163E-02	-.19535E-04	.10867E 01	.28207E-03
δ_R	-.13097E 00	.11632E-03	.19173E 00	-.86717E-04	-.77228E-02	.11588E-02
δ_C	-.21808E-01	-.83098E-02	.20679E-02	.72385E 00	.53403E-01	-.84541E 01
p	-.17699E 01	.17608E-01	-.11083E-01	.27304E-01	-.34746E 01	-.10080E 00
q	.23845E-01	-.16340E 01	-.15184E 00	.29000E 01	-.15530E 00	-.27756E 01
r	.94610E-01	-.24799E 00	-.31011E 00	-.11104E 00	-.19343E 00	.17427E 00
u	.36832E-03	.15576E-01	.93124E-03	-.12845E-01	.20536E-02	-.40519E-01
v	-.11932E-01	-.87052E-03	.45401E-02	.14368E-03	-.46926E-01	.44441E-02
w	.83532E-03	.16647E-01	.71129E-03	.26766E-01	.43535E-02	-.28244E 00

TABLE 36.- STABILITY AND CONTROL DERIVATIVES, $V_{eq} = 40$ KNOTS.

	L	M	N	X	Y	Z
SAS off						
δ_B	0.16262E-01	0.37444E 00	0.36975E-01	0.35347E-01	0.10732E 00	0.64975E 00
δ_A	.48558E 00	.74250E-05	.76233E-02	.30970E-04	.10845E 01	-.41167E-03
δ_R	-.13531E 00	.10642E-03	.19126E 00	.95293E-05	-.23260E-01	.19059E-03
δ_C	-.95659E-02	.12353E 00	.53661E-02	.49135E 00	.65350E-01	-.79678E 01
p	-.95132E 00	.12811E-01	-.48200E-02	.26064E-01	-.17385E 01	-.93921E-01
q	-.70335E-01	-.17676E 01	-.82320E-01	.28099E 01	-.26218E 00	-.32915E 01
r	-.83902E-01	-.25619E 00	-.68326E-01	-.91516E-01	-.24125E 00	.31847E-01
u	-.27828E-03	.73133E-03	.25274E-03	-.14508E-01	-.45629E-03	-.10797E 00
v	-.89953E-02	-.15318E-02	.32037E-03	.71239E-03	-.59403E-01	.15510E-02
w	.27440E-02	.25877E-01	.24907E-04	.28541E-01	.71078E-02	-.34978E 00
SAS on						
δ_B	0.16266E-01	0.37447E 00	0.36974E-01	0.35376E-01	.10733E 00	0.64948E 00
δ_A	.48558E 00	.16706E-04	.76228E-02	.33829E-04	.10845E 01	-.41167E-03
δ_R	-.13531E 00	.10147E-03	.19126E 00	.76234E-05	-.23263E-01	.19059E-03
δ_C	-.95641E-02	.12354E 00	.53671E-02	.49134E 00	.65357E-01	-.79677E 01
p	-.18352E 01	.12746E-01	-.82783E-02	.25948E-01	-.36978E 01	-.92587E-01
q	-.70338E-01	-.17676E 01	-.82320E-01	.28099E 01	-.26219E 00	-.32914E 01
r	-.83904E-01	-.25619E 00	-.68327E-01	-.91541E-01	-.24125E 00	.32076E-01
u	-.16688E-03	.30276E-02	.47155E-03	-.14280E-01	.20976E-03	-.10406E 00
v	-.15384E-01	-.15291E-02	.88345E-02	.71267E-03	-.61624E-01	.15575E-02
w	.27579E-02	.26180E-01	.53823E-04	.28559E-01	.71934E-02	-.34916E 00

TABLE 37.- STABILITY AND CONTROL DERIVATIVES, $V_{eq} = 60$ KNOTS.

	L	M	N	X	Y	Z
SAS off						
δ_B	0.20527E-01	0.41184E 00	0.29139E-01	0.47545E-01	0.94130E-01	0.84306E 00
δ_A	.48669E 00	.14850E-04	.62967E-02	.23823E-04	.10852E 01	-.35830E-03
δ_R	-.14165E 00	.10457E-03	.19128E 00	.95293E-05	-.44399E-01	.25920E-03
δ_C	-.18126E-02	.23377E 00	.45609E-02	.32755E 00	.63338E-01	-.81505E 01
P	-.10201E 01	.19924E-01	-.45460E-02	.21280E-01	-.19788E 01	-.62703E-01
q	-.66438E-01	-.15813E 01	-.50139E-01	.26308E 01	-.13403E 00	-.64037E 00
r	-.88795E-01	-.27361E 00	-.63247E-01	-.69984E-01	-.24875E 00	-.18037E 00
u	-.77862E-03	-.72600E-02	.27577E-03	-.89043E-02	-.13639E-02	-.75485E-01
v	-.92920E-02	-.12844E-02	.74233E-03	.45669E-03	-.72300E-01	.23884E-02
w	.20447E-02	.14508E-01	-.30937E-03	.34278E-01	.43612E-02	-.56357E 00
SAS on						
δ_B	0.20524E-01	0.41183E 00	0.29137E-01	0.47545E-01	0.94120E-01	0.84314E 00
δ_A	.48669E 00	.43313E-05	.62940E-02	.19059E-04	.10852E 01	-.38880E-03
δ_R	-.14166E 00	.10333E-03	.19128E 00	.12865E-04	-.44434E-01	.18296E-03
δ_C	-.18128E-02	.23375E 00	.45590E-02	.32753E 00	.633311E-01	-.81503E 01
P	-.19063E 01	.20035E-01	-.55991E-02	.21198E-01	-.39406E 01	-.60911E-01
q	-.66423E-01	-.15813E 01	-.50141E-01	.26308E 01	-.13399E 00	-.64041E 00
r	-.88790E-01	-.27361E 00	-.63247E-01	-.69969E-01	-.24874E 00	-.18052E 00
u	-.49027E-03	-.14984E-02	.68419E-03	-.82746E-02	-.48504E-04	-.63429E-01
v	-.18995E-01	-.12780E-02	.13316E-01	.45590E-03	-.76522E-01	.24044E-02
w	.20616E-02	.14837E-01	-.28640E-03	.34319E-01	.44362E-02	-.56292E 00

TABLE 38.- STABILITY AND CONTROL DERIVATIVES, $V_{eq} = 80$ KNOTS.

	L	M	N	X	Y	Z
SAS off						
δ_B	0.18186E-01	0.43017E 00	0.25086E-01	0.49940E-01	0.69011E-01	0.72319E 00
δ_A	.48646E 00	.19800E-04	.71456E-02	.42405E-04	.10864E 01	-.57176E-03
δ_R	-.13782E 00	.13118E-03	.19154E 00	.11435E-04	-.31017E-01	.22870E-03
δ_C	-.32358E-02	.22604E 00	.50223E-02	.41855E 00	.47280E-01	-.93412E 01
p	-.10358E 01	.26438E-01	-.11789E-01	.20552E-01	-.20591E 01	-.53021E-01
q	-.58419E-01	-.16518E 01	-.27933E-01	.26311E 01	-.41224E-01	-.40780E 00
r	-.86358E-01	-.27552E 00	-.62181E-01	-.64663E-01	-.24425E 00	-.18331E 00
u	-.72031E-03	-.80721E-02	.29346E-03	-.57070E-02	-.85947E-03	.23015E-01
v	-.10178E-01	-.77693E-03	.13452E-02	-.73144E-03	-.87794E-01	.48923E-02
w	.18117E-02	.11446E-01	-.55603E-03	.42780E-01	.24069E-02	-.63679E 00
SAS on						
δ_B	0.18185E-01	0.43017E 00	0.25085E-01	0.49938E-01	0.69008E-01	0.72302E 00
δ_A	.48646E 00	.80437E-05	.71494E-02	.41929E-04	.10864E 01	-.59463E-03
δ_R	-.13780E 00	.13179E-03	.19154E 00	.17153E-04	-.30952E-01	.18296E-03
δ_C	-.32329E-02	.22606E 00	.50244E-02	.41854E 00	.47293E-01	-.93412E 01
p	-.19214E 01	.26402E-01	-.14384E-01	.20525E-01	-.40223E 01	-.52983E-01
q	-.58435E-01	-.16518E 01	-.27931E-01	.26312E 01	-.41266E-01	-.40757E 00
r	-.86361E-01	-.27561E 00	-.62185E-01	-.64679E-01	-.24427E 00	-.18317E 00
u	-.46929E-03	-.20446E-02	.64880E-03	-.50124E-02	.10565E-03	.33220E-01
v	-.16872E-01	-.78216E-03	.10384E-01	-.73635E-03	-.89888E-01	.49240E-02
w	.18230E-02	.11717E-01	-.53788E-03	.42811E-01	.24501E-02	-.63634E 00

TABLE 39.- STABILITY AND CONTROL DERIVATIVES, $V_{eq} = 100$ KNOTS.

	L	M	N	X	Y	Z
SAS off						
δ_B	0.90613E-02	0.44705E 00	0.37866E-01	0.50019E-01	0.56612E-01	0.61777E 00
δ_A	.48682E 00	.13612E-04	.78353E-02	.62417E-04	.10891E 01	-.78521E-03
δ_R	-.13497E 00	.15283E-03	.19208E 00	.10482E-04	-.20293E-01	.31256E-03
δ_C	-.96637E-02	.19979E 00	.82407E-02	.48930E 00	.57241E-01	-.10341E 02
p	-.10130E 01	.32085E-01	-.17801E-01	.21528E-01	-.20089E 01	-.48580E-01
q	-.21003E-01	-.17096E 01	-.60791E-01	.26825E 01	.25619E-01	-.52836E 00
r	-.82925E-01	-.28395E 00	-.60608E-01	-.64930E-01	-.24014E 00	-.18054E 00
u	-.65926E-03	-.68107E-02	.85861E-04	-.12636E-01	-.75137E-03	.77988E-01
v	-.11280E-01	-.35758E-03	.17701E-02	-.13568E-02	-.10514E 00	.66061E-02
w	.13236E-02	.11651E-01	-.70293E-03	.49820E-01	.84167E-03	-.67691E 00
SAS on						
δ_B	0.90609E-02	0.44708E 00	0.37866E-01	0.50063E-01	0.56606E-01	0.61809E 00
δ_A	.48681E 00	.16706E-04	.78342E-02	.54793E-04	.10891E 01	-.71660E-03
δ_R	-.13497E 00	.17758E-03	.19208E 00	.16676E-04	-.20313E-01	.29731E-03
δ_C	-.96468E-02	.19983E 00	.82411E-02	.48935E 00	.57290E-01	-.10341E 02
p	-.18992E 01	.32175E-01	-.21583E-01	.21556E-01	-.39764E 01	-.47151E-01
q	-.21047E-01	-.17095E 01	-.60784E-01	.26824E 01	.25607E-01	-.52264E 00
r	-.82966E-01	-.28400E 00	-.60604E-01	-.64910E-01	-.24013E 00	-.18054E 00
u	-.57006E-03	-.22004E-02	.47949E-03	-.12140E-01	-.21226E-03	.84532E-01
v	-.16821E-01	-.35272E-03	.94919E-02	-.13535E-02	-.10633E 00	.66145E-02
w	.13294E-02	.11841E-01	-.68916E-03	.49846E-01	.86571E-03	-.67667E 00

TABLE 40.- STABILITY AND CONTROL DERIVATIVES, $V_{eq} = 120$ KNOTS.

	L	M	N	X	Y	Z
SAS off						
δ_B	0.44967E-02	0.45113E 00	0.41217E-01	0.52785E-01	0.33761E-01	0.51063E 00
δ_A	.48837E 00	.80437E-05	.85038E-02	-.26682E-04	.10958E 01	-.86907E-03
δ_R	-.13277E 00	.17263E-03	.19330E 00	-.73376E-04	-.10244E-01	.16772E-03
δ_C	-.12798E-01	.18235E 00	.13521E-01	.51532E 00	.64276E-01	-.10988E 02
p	-.96118E 00	.38905E-01	-.25580E-01	.23660E-01	-.18659E 01	-.39966E-01
q	.28512E-02	-.17035E 01	-.64121E-01	.27440E 01	.12582E 00	-.47326E 00
r	-.69907E-01	-.29838E 00	-.66858E-01	-.70063E-01	-.20300E 00	-.21412E 00
u	-.47924E-03	-.41431E-02	.87713E-04	-.27700E-01	-.13417E-03	.63076E-01
v	-.12484E-01	.92008E-04	.21020E-02	-.16492E-02	-.12355E 00	.81514E-02
w	.11215E-02	.12060E-01	-.70963E-03	.52272E-01	.52805E-03	-.70081E 00
SAS on						
δ_B	0.44515E-02	0.45118E 00	0.41178E-01	0.52667E-01	0.33591E-01	0.51360E 00
δ_A	.48834E 00	.92812E-05	.85063E-02	.67658E-04	.10957E 01	-.83095E-03
δ_R	-.13275E 00	.17572E-03	.19329E 00	.21441E-04	-.10192E-01	.15247E-03
δ_C	-.12818E-01	.18237E 00	.13475E-01	.51540E 00	.64092E-01	-.10985E 02
p	-.18499E 01	.38673E-01	-.30602E-01	.23319E-01	-.38448E 01	-.38880E-01
q	.23448E-02	-.17036E 01	-.63966E-01	.27436E 01	.11146E 00	-.48112E 00
r	-.69859E-01	-.29837E 00	-.66854E-01	-.69797E-01	-.20289E 00	-.22188E 00
u	-.44009E-03	-.15333E-03	.45154E-03	-.27231E-01	.16060E-03	.67680E-01
v	-.17427E-01	.10027E-03	.91899E-02	-.16471E-02	-.12418E 00	.79958E-02
w	.11216E-02	.12191E-01	-.70072E-03	.52297E-01	.52671E-03	-.70069E 00

TABLE 41.- STABILITY AND CONTROL DERIVATIVES, $V_{eq} = 130$ KNOTS.

	L	M	N	X	Y	Z
SAS off						
δ_B	0.21123E-02	0.44601E 00	0.43973E-01	0.65784E-01	0.27197E-01	0.46277E 00
δ_A	.49179E 00	.68062E-05	.82524E-02	.23823E-04	.11066E 01	-.35830E-03
δ_R	-.13550E 00	.79200E-04	.19517E 00	.17629E-04	-.15153E-01	.53364E-04
δ_C	-.14705E-01	.19110E 00	.15004E-01	.35527E 00	.59271E-01	-.11143E 02
p	-.93025E 00	.41965E-01	-.29312E-01	.24776E-01	-.17771E 01	-.35792E-01
q	.14853E-01	-.16772E 01	-.68904E-01	.27638E 01	.16740E 00	-.30235E 00
r	-.70654E-01	-.30869E 00	-.56485E-01	-.78874E-01	-.18537E 00	-.25638E 00
u	-.47011E-03	-.22112E-02	-.13100E-03	-.37849E-01	.25163E-03	.13208E-01
v	-.13160E-01	.27804E-03	.22743E-02	-.17813E-02	-.13514E 00	.81796E-02
w	.13102E-02	.12423E-01	-.68993E-03	.42638E-01	.28617E-02	-.70578E 00
SAS on						
δ_B	0.21255E-02	0.44608E 00	0.43970E-01	0.65772E-01	0.27233E-01	0.46282E 00
δ_A	.49179E 00	.12994E-04	.82566E-02	.38594E-04	.11066E 01	-.52602E-03
δ_R	-.13549E 00	.87862E-04	.19517E 00	.17629E-04	-.15109E-01	.22870E-04
δ_C	-.14739E-01	.19101E 00	.15009E-01	.35526E 00	.59168E-01	-.11143E 02
p	-.18254E 01	.42097E-01	-.33686E-01	.24709E-01	-.37760E 01	-.35182E-01
q	.14795E-01	-.16770E 01	-.68886E-01	.27638E 01	.16725E 00	-.30254E 00
r	-.70668E-01	-.30869E 00	-.56483E-01	-.78869E-01	-.18540E 00	-.25634E 00
u	-.45135E-03	.17370E-02	.25679E-03	-.37269E-01	.49216E-03	.17447E-01
v	-.18035E-01	.28193E-03	.92009E-02	-.17801E-02	-.13590E 00	.83442E-02
w	.13086E-02	.12469E-01	-.68580E-03	.42640E-01	.28572E-02	-.70574E 00

TABLE 42.- STATIC TRIM DATA, SLUNG LOAD ATTACHED

 $V_{eq} = 0.1 \text{ knot, SAS on}$ $\theta_{SL} = 0^\circ$

CH-47B TRIM DATA RUN NO. 5														
18:28 FEB 22, '83														
VTOT = .1 FT	U = .1 KT	V = .0 FT	W = .0 FT	T = .0 FT	TEMP = 386.0 DG	DPCG = .0	1.0 IN	BODG = .0	.0 IN	PHP = .0				
G.W. = 25500.0 LBS	RPM = 24.1	H = 97.0 FT	T = 0.0 DEG	P = 0.0 DEG	PHI = 0.0 DEG	PSI = 0.0 DEG	PHI = 0.0 DEG	PSI = 0.0 DEG	PHI = 0.0 DEG	PSI = 0.0 DEG	PHI = 0.0 DEG	PSI = 0.0 DEG	PHI = 0.0 DEG	PSI = 0.0 DEG
THETA = .66237E 01	PHI = -.39458E 00	PSI = .00000E 00	P = .00000E 00	Q = .00000E 00	R = .00000E 00	DELTA PLT = .388961E -01	DELP PLT = .20269E 00	DELP TLT = .13846E 01	DELP TLT = .13846E 00	DELP TLT = .13846E 01	DELP TLT = .13846E 00	DELP TLT = .13846E 01	DELP TLT = .13846E 00	DELP TLT = .13846E 01
DELB PLT = .99618E 02	DELB PLT = .19618E 02	DELB PLT = .13846E -01	DELB PLT = .15750E 01	DELB PLT = .13846E 01	DELB PLT = .13846E 01	DELB TLT = .28805E 00	DELB TLT = .11500E 01	DELB TLT = .13846E 01	DELB TLT = .13846E 00	DELB TLT = .13846E 01	DELB TLT = .13846E 00	DELB TLT = .13846E 01	DELB TLT = .13846E 00	DELB TLT = .13846E 01
THETA FP = .19618E 02	AICFP = .28805E 00	BICFP = .11500E 01	THETAFP = .10496E 02	PHIFP = .15750E 01	PHIFP = .15750E 01	PHIFP = .15750E 01	PHIFP = .15750E 01	PHIFP = .15750E 01	PHIFP = .15750E 01	PHIFP = .15750E 01	PHIFP = .15750E 01	PHIFP = .15750E 01	PHIFP = .15750E 01	PHIFP = .15750E 01
SIGMA FP = .66379E -01	SIGMA PR = .66379E -01	GHTM FS = .46931E -03	LHDG FP = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03	LHDG PR = .57000E -03
THRUST F = .17054E 05	NORMFL F = .44803E 03	SIDE F = .36029E 00	TOPDUE F = .43802E 05	L HDP F = .41686E 03	M HDP F = .26757E 03	N HDP F = .17108E 03	O HDP F = .15319E 03	P HDP F = .12100E 03	Q HDP F = .10747E 03	R HDP F = .10011E 01	S HDP F = .13499E 07	T HDP F = .13499E 07	U HDP F = .13499E 07	V HDP F = .13499E 07
THRUST R = .16515E 05	NORMFR = .43084E 03	SIDE R = .13987E 03	TOPDUE R = .43771E 05	L HDU R = .41686E 03	M HDU R = .26757E 03	N HDU R = .17108E 03	O HDU R = .15319E 03	P HDU R = .12100E 03	Q HDU R = .10747E 03	R HDU R = .10011E 01	S HDU R = .13499E 07	T HDU R = .13499E 07	U HDU R = .13499E 07	V HDU R = .13499E 07
CT FR = .48740E -02	CH FR = .12804E -03	CY FR = .24588E -04	CO FR = .41623E -03	HO FR = .46179E -01	AI FR = .15319E 01	ET FR = .15319E 01	EV FR = .15319E 00	GO FR = .14339E 05						
CT PR = .47198E -02	CH PR = .12313E -03	CY PR = .39975E -04	CO PR = .46745E -03	HO PR = .44717E -01	AI PR = .14339E -01	ET PR = .14339E -01	EV PR = .14339E -01	GO PR = .14339E -01						
X FUSE = -.25129E 00	X SLING = .20366E -02	LHDH SL = .39458E 01	L F.POT = .10275E 04	L F.POT = .15319E 04	L F.POT = .15319E 04	L F.POT = .15319E 04	L F.POT = .15319E 04	L F.POT = .15319E 04	L F.POT = .15319E 04	L F.POT = .15319E 04	L F.POT = .15319E 04	L F.POT = .15319E 04	L F.POT = .15319E 04	L F.POT = .15319E 04
Y FUSE = .20728E 00	Y SLING = .89942E -05	MU SL = .00000E 00	Y F.POT = .16389E 01	Y F.POT = .13355E 02	Y F.POT = .13355E 02	Y F.POT = .13355E 02	Y F.POT = .13355E 02	Y F.POT = .13355E 02	Y F.POT = .13355E 02	Y F.POT = .13355E 02	Y F.POT = .13355E 02	Y F.POT = .13355E 02	Y F.POT = .13355E 02	Y F.POT = .13355E 02
Z FUSE = .57495E 03	Z SLING = .00000E 00	MU SL = .66237E 01	Z F.POT = .16814E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05	Z F.POT = .16445E 05
L FUSE = .21933E 00	L SLING = .00000E 00	MU SL = .10000E 01	L F.POT = .15739E 04	L F.POT = .15367E 04	L F.POT = .15367E 04	L F.POT = .15367E 04	L F.POT = .15367E 04	L F.POT = .15367E 04	L F.POT = .15367E 04	L F.POT = .15367E 04	L F.POT = .15367E 04	L F.POT = .15367E 04	L F.POT = .15367E 04	L F.POT = .15367E 04
M FUSE = .83688E 03	M SLING = .00000E 00	MU SL = .37110E 06	M F.POT = .37110E 06	M F.POT = .32500E 06	M F.POT = .32500E 06	M F.POT = .32500E 06	M F.POT = .32500E 06	M F.POT = .32500E 06	M F.POT = .32500E 06	M F.POT = .32500E 06	M F.POT = .32500E 06	M F.POT = .32500E 06	M F.POT = .32500E 06	M F.POT = .32500E 06
N FUSE = -.51126E 00	N SLING = .42326E -05	MU SL = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05	N F.POT = .45193E 05
BETA FS = -.45820E -01	BETA SL = .44307E -01	SL WGT = .75000E 04	BETH FP = .45553E -01	BETH FP = .45561E -01	BETH FP = .45561E -01	BETH FP = .45561E -01	BETH FP = .45561E -01	BETH FP = .45561E -01	BETH FP = .45561E -01	BETH FP = .45561E -01	BETH FP = .45561E -01	BETH FP = .45561E -01	BETH FP = .45561E -01	BETH FP = .45561E -01
ALPH FS = -.89685E 02	ALPH SL = .65203E 01	J SL = .77711E 04												

WINTER 44249E -02 THETA SL .00000E 00 L SL .20000E 02

WIFS , 20000E 02

WIPR .00000E 00 YPR BODY .48639E 02 TPR BODY .14022E 03

RIGAR .14022E 03 BIGAR .14022E 03

JOINTS, LANDING GEAR, TAIL

ITC PSHSR 1
RSASD 1 NSTHLL 1
ISTEADY 1 NTPDCP 0
ISLTH1 1

TABLE 43.- STATIC TRIM DATA, SLUNG LOAD ATTACHED

$$V_{eq} = 75 \text{ knots, SAS on}$$

$$\theta_{SL} = 0^\circ$$

CH-47B TRIM DATA PUN NO. 9												
19:40 FEB 24, '83												
VTOT = 75.0 KT	U	-75.1 FT	V	-0 KT	W	1.4 FT	ROLL	PITCH	YAW	IN	FHP	JO
G.W. = 25500.0 LBS PPM	*	24.1 H	= 99.4 FT	TEMP = 286.0 DEG	INC = 0	ROLL = 0.0000E+00	PITCH = 0.0000E+00	YAW = 0.0000E+00	IN = 0.0000E+00	JO = 0.0000E+00	FHP = 0.0000E+00	JO = 0.0000E+00
THETHA	PHI	PSI	P	Q	R	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
.10461E-01	-.23680E-00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
DELB PLT	DELB PLT	DELB PLT	DELB PLT	DELB TOT	DELB TOT	ROLL TOT	PITCH TOT	YAW TOT	IN TOT	FHP TOT	JO TOT	JO TOT
-.20137E-01	.17054E-00	.11654E-00	.49505E-01	-.10400E-01	.17054E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
THETHA FR	AICER	BICER	THETHA FR	ROLL FR	PITCH FR	ROLL TOT	PITCH TOT	YAW TOT	IN TOT	FHP TOT	JO TOT	JO TOT
.16295E-02	.69200E-00	-.37506E-00	.17054E-00	.10540E-00	.14746E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
SIGMA FR	SIGMA FR	GAMMA FS	THETHA FR	ROLL FR	PITCH FR	ROLL TOT	PITCH TOT	YAW TOT	IN TOT	FHP TOT	JO TOT	JO TOT
.66979E-01	.66979E-01	.13581E-01	-.37506E-00	-.37506E-01	.14746E-00	-.14746E-00	-.14746E-00	-.14746E-00	-.14746E-00	-.14746E-00	-.14746E-00	-.14746E-00
THRUST F	NORMAL F	SIDE F	TOPDOE F	L BHP FR	H BHP FR	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
.16770E-05	.1082E-04	.27542E-03	.23401E-05	.28467E-04	.14506E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
THRUST R	NORMAL R	SIDE R	TOPDOE R	L BHP FR	H BHP FR	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
.16834E-05	.23701E-03	.13918E-03	.31566E-05	.15151E-04	.16781E-03	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
CT FR	CH FR	CY FR	CO FR	HD FR	HD FR	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
.47932E-02	.28815E-03	.70717E-04	.12229E-03	.41151E-01	.13070E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
CT RR	CH RR	CY RR	CO RR	HD RR	HD RR	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
.48112E-02	.67738E-04	.30078E-04	.30078E-03	.14716E-01	.11654E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
X FUSE	X SLING	LNDMH SL	X FPOT	X PRST	X HI	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
-.89948E-03	-.10623E-04	.27680E-00	.16277E-04	.19375E-03	.12105E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
Y FUSE	Y SLING	NU SL	Y FPOT	Y PRST	Y HI	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
.31663E-01	.59513E-00	.00000E+00	.27544E-03	-.13015E-03	.11712E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
Z FUSE	Z SLING	NU SL	Z FPOT	Z PRST	Z HI	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
.53621E-03	.00000E+00	-.91139E-01	-.16720E-05	-.16690E-05	-.82130E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
L FUSE	L SLING	K BHP SL	L FPOT	L PRST	L HI	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
-.37867E-02	.00000E+00	.10100E-01	.77991E-03	-.29025E-03	-.92737E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
M FUSE	M SLING	NU SL	M FPOT	M PRST	M HI	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
-.32282E-04	.00000E+00	-.91139E-01	.32339E-06	-.32107E-06	.15201E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
N FUSE	N SLING	NU SL	N FPOT	N PRST	N HI	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
-.72878E-02	-.11903E-01	-.29119E-05	-.29046E-05	-.29035E-05	-.14738E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
BETA FS	BETA SL	SL WIGHT	BETH FR	BETA FR	BETH FR	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
-.43241E-02	-.43242E-02	.75000E-04	-.43653E-02	-.43291E-02	-.14738E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
ALPH FS	ALPH SL	J SL	ALPH FR	ALPH FR	ALPH FR	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
-.33565E-01	.10461E-01	.77711E-04	-.14738E-01	-.14738E-01	-.14738E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
VINTF	THETA SL	L SL	WIPR	WFR	WFR	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
.94679E-01	.00000E+00	.20000E-02	.10000E-00	.10000E-00	.10000E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
WIFS	SMA SL	R SL	ACRR	ACRR	ACRR	ROLL FR	PITCH FR	YAW FR	IN FR	FHP FR	JO FR	JO FR
-.97476E-01	.20000E-02	.00000E+01	.39430E-01	.26250E-01	.26250E-01	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00	.11654E-00
CONTROL FLAGS SET UP												
ISLING 1	IECSOM 8											
IDCPT 1	PSASP 1											
PSASO 1	PSASP 1											
ISTEADY 1	NSTALL 1											
NTROCR 1	NGREFF 0											
ISLTRM 1												

TABLE 44.- STATIC TRIM DATA, SLUNG LOAD ATTACHED

$V_{eq} = 0.1$ knot, SAS on

$\theta_{SL} = -5^\circ$

CH-47B TRIM DATA RUN NO. 1											
19:09 FEB 22, 1983											
WTOT *	.1 FT	U	* 24.1	.1 FT	M	* 97.0 FT	DELT	M	* .0 FT	AFT	DIST
G.W. = 25500.0 LBS RPM =	.00000E 00		.00000E 00	.00000E 00		.00000E 00	.00000E 00		.00000E 00		.00000E 00
THETA	RHI	PSI	P	H	DEL	DELT	DELT	DEL	DEL	DELT	DELT
.66237E 01	-.39001E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 01						
DELB PLT	DELS PLT	DELP PLT	DELB PLT	DELS PLT	DELB TGT						
.98888E-01	.20224E 00	-.30171E 01	.57589E 01	-.20336E 01	.10477E 00						
THETO FP	HICFP	EICFP	THETO FP	HICFP	1.01	1.01	1.01	1.01	1.01	1.01	1.01
.13613E 01	.13613E 00	-.15000E 01	.13613E 00								
SIGMA FP	SIGMA FP	SIGMA FS	SIGMA FP	SIGMA FS	SIGMA FP						
.66897E-01	.66897E-01	.49393E-01	.66897E-01	.49393E-01	.66897E-01						
THRUST F	NOFTHL F	SIDE F	TOPFL F	SIDE F	NOFTHL F	NOFTHL F	NOFTHL F	NOFTHL F	NOFTHL F	NOFTHL F	NOFTHL F
.17056E-05	.14410E-05	.18164E-05	.14716E-05	.14716E-05	.14410E-05						
THRUST F	NOFTHL F	SIDE F	GEODE F	NOFTHL F	GEODE F	GEODE F	GEODE F	GEODE F	GEODE F	GEODE F	GEODE F
.16516E-05	-.14398E-05	-.14398E-05	.14177E-05	-.14177E-05	-.14398E-05						
CT FP	CH FP	CY FP	CO FP	CR FP	CT FPOT						
.48744E-03	.10980E-03	.10468E-03	.14101E-03	.16132E-03	.10980E-03						
CT FP	CH FP	CY FP	CO FP	CR FP	CT FPOT						
.47202E-02	-.12314E-02	-.34749E-02	.14079E-02	.14472E-02	-.14472E-01						
Z FUSE	Z SLING	LHDLR SL	Z FLPOT								
-.12515E-00	-.19021E-02	.39561E-00	.20255E-04	.15600E-04	.14872E-04						
Y FUSE	Y SLING	NU SL	Y FLPOT								
.120739E-00	.11111E-04	.001000E 00	.06045E-02	.12039E-02							
Z FUSE	Z SLING	NU SL	Z FLPOT								
.157500E-03	.000000E 00	-.66237E-01	-.16316E-05	-.11644E-05							
L FUSE	L SLING	NU SL	L FLPOT								
.21935E-00	.000000E 00	.100000E 01	-.52985E-04	.53764E-04	-.53764E-04						
II FUSE	II SLING	NU SL	II FLPOT								
.03695E-03	.000000E 00	.000000E 00	.33113E-06	-.32300E-06							
II FUSE	II SLING	NU SL	II FLPOT								
-.51131E-00	-.36507E-04	.45200E-05	-.45187E-05	.45187E-05							
BETA FS	BETA SL	SL WIGHT	BETA FP								
-.45870E-01	-.63446E-01	.75000E-04	-.45603E-01	-.45611E-01							
ALPH FS	ALPH SL	J SL									
-.89685E-02	.14610E-01	.77711E-04									
VINTF	THETA SL	L SL									
.41251E-02	-.49996E-01	.20000E-02									
WIFS	SMA SL	R SL									
.30554E-02	.20000E-02	.80000E-01									
CONTROL FLAGS SET UP											
ISLING 1	I EDSCON 0										
IDCPT 1	PSASP 1										
PSASD 1	PSASP 1										
ISTEADY 1	NSTHLL 1										
NTROCP 1	NGPEFF 0										
ISLTRII 1											
WIPF											
.00000E 00	.00045E-02										
YFP BODY											
-.13953E-03											
AICRR											
-.48381E-08											
BICRR											
.14996E-01											

TABLE 45.- STATIC TRIM DATA, SLUNG LOAD ATTACHED

$V_{eq} = 75$ knots, SAS on

$\theta_{SL} = -5^\circ$

CH-47B TRIM DATA RUN NO. 1											
19:07 FEB 22, 1983											
WTOT = 75.0 FT U	= 75.1 XT	U = 24.1 H	V = 89.5 FT RSP	U = 10.0 FT RSP							
G.W. = 25500.0 LBS PPI =			P = .00000E 00								
THETH	PHI	PSI	R	O	F	T	M	B	C	D	E
.96231E 00	-.23708E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00	.00000E 00
DELB PLT	DELB PLT	DELP PLT	DELC PLT	DELC PLT	DELC PLT	DELC PLT	DELC PLT	DELC PLT	DELC PLT	DELC PLT	DELC PLT
-.20112E 01	.17302E 00	.11521E 00	.14945E 01	-.17001E 01	-.17501E 01						
THETO FP	HICFP	BLCFP	THED FP								
.16310E 02	.69506E 00	-.37505E 00	.11701E 00	.10500E 00							
SIGMA FP	SIGMA FP	SIGMA FP	SIGMA FP	SIGMA FP	SIGMA FP	SIGMA FP	SIGMA FP	SIGMA FP	SIGMA FP	SIGMA FP	SIGMA FP
.66973E-01	.66973E-01	.13574E-01	.13574E-01	.13574E-01	.13574E-01	.13574E-01	.13574E-01	.13574E-01	.13574E-01	.13574E-01	.13574E-01
THRUST F	NORMHL F	SIDE F	TOPOL F	TOPOL F	TOPOL F	TOPOL F	TOPOL F	TOPOL F	TOPOL F	TOPOL F	TOPOL F
.16784E-05	.16109E-04	.12758E-04	.12351E-05								
THROST P	NORMRL P	SIDE P	TOPOL P	TOPOL P	TOPOL P	TOPOL P	TOPOL P	TOPOL P	TOPOL P	TOPOL P	TOPOL P
.16829E-05	.12302E-05	.14849E-05	.15173E-05								
CT FP	CH FP	CY FP	CD FP	CR FP	CI FP	CO FP	CP FP	CT FP	CH FP	CH FP	CH FP
.47396E-02	.29088E-03	.76701E-04	.12739E-02	.14157E-01	.12739E-01						
CT FP	CH FP	CY FP	CD FP	CR FP	CI FP	CO FP	CP FP	CT FP	CH FP	CH FP	CH FP
.48099E-02	.68104E-04	.37582E-04	.15021E-03	.14157E-01							
X FUSE	Z SLING	LADMR SL	LT PLT								
-.88976E-03	-.11098E-04	.23786E-00	.14274E-04	.19510E-03							
Y FUSE	Y SLING	NU SL	Y PLT								
.29263E-01	.59513E-00	.00000E 00	.12754E-03	-.13431E-03							
Z FUSE	C SLING	NU SL	C PLT								
.54473E-03	.00000E 00	-.93736E-01	-.16735E-05	-.16903E-05							
L FUSE	L SLING	F BAF SL	L PLT								
-.37878E-02	.00000E 00	.10103E-01	.17516E-03	-.16735E-02							
M FUSE	M SLING		M PLT								
-.33383E-04	.00000E 00		.18342E-05	-.13303E-05							
N FUSE	N SLING		N PLT								
-.68114E-02	-.59513E-00		.29250E-05	-.29181E-05							
BETA FS	BETH SL	SL MIGHT	BETA FP	BETH FP							
-.39957E-02	-.39958E-02	.75000E-04	-.40344E-02	-.16903E-02							
ALPH FS	ALPH SL	J SL									
-.34430E-01	-.40373E-01	.77711E-04									
WINTF	THETA SL	L SL									
.94761E 01	-.49996E 01	.20000E 02									
WIFS	SMA SL	R SL									
-.97545E 01	.20000E 02	.80000E 01									
CONTROL FLAGS SET UP											
ISLING 1	IEOSCON 0										
IDCPT 1	PSASP 1										
PSASD 1	PSASR 1										
ISTEADY 1	NSTALL 1										
HTPOCP 1	NGREFF 0										
ISLTPM 1											
WIPPP											
.00000E 00											
WPP BODY											
.27048E 02											
WPP BODY											
.13851E 03											
RICRR											
.34181E-01											
BICRR											
.26250E 01											

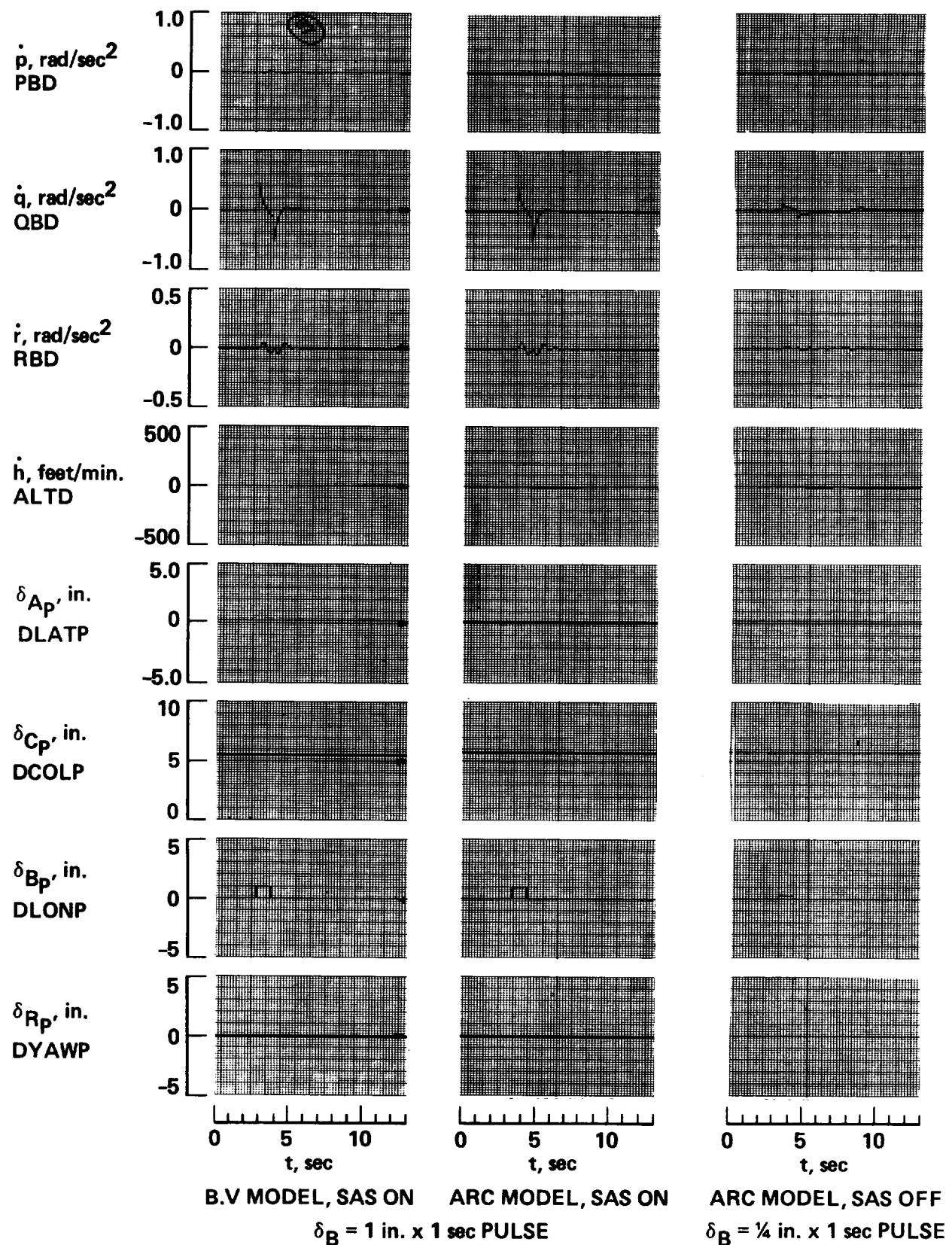


Figure 1.- BV versus ARC simulation response data; hover.

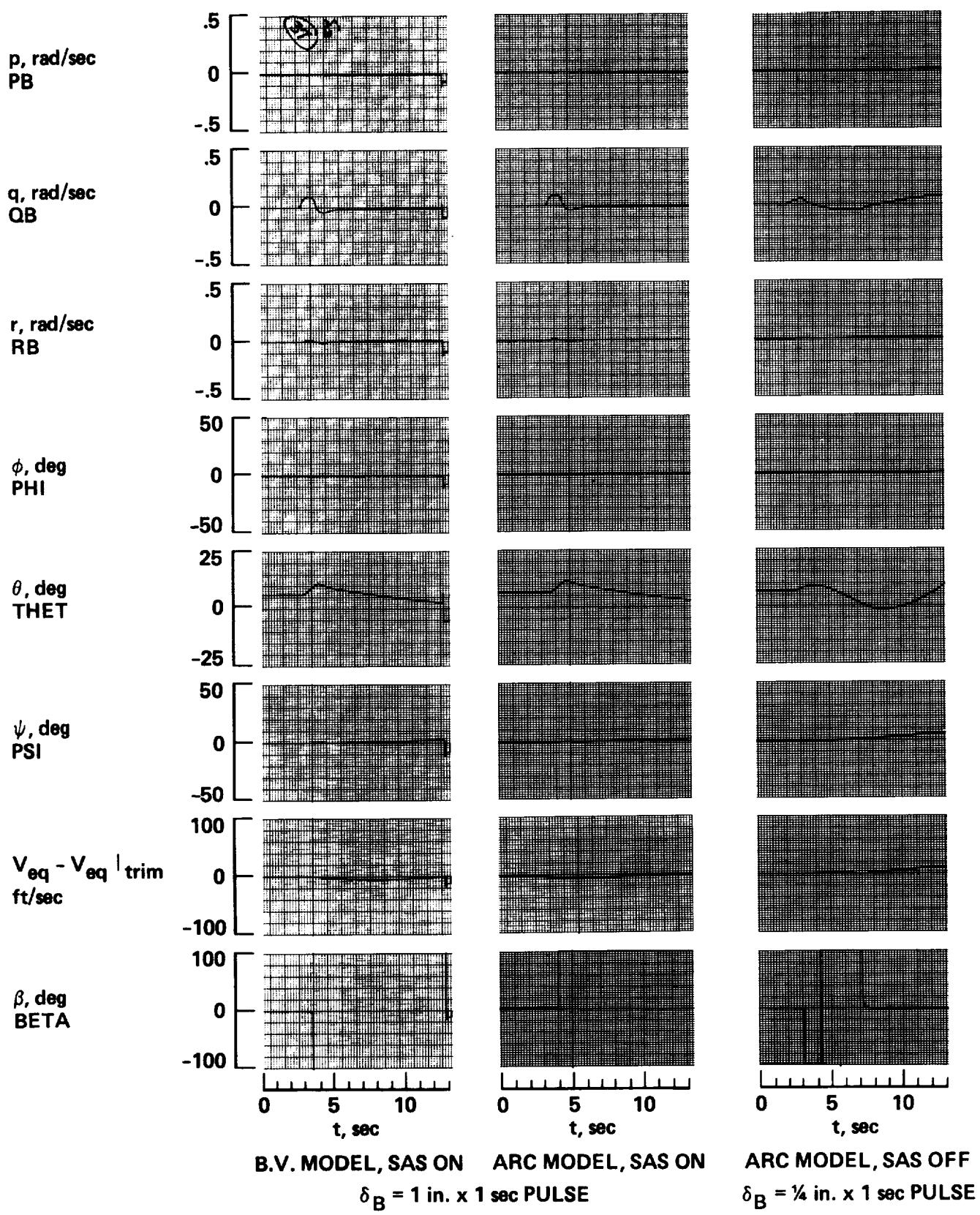


Figure 2.- BV versus ARC simulation response data; hover.

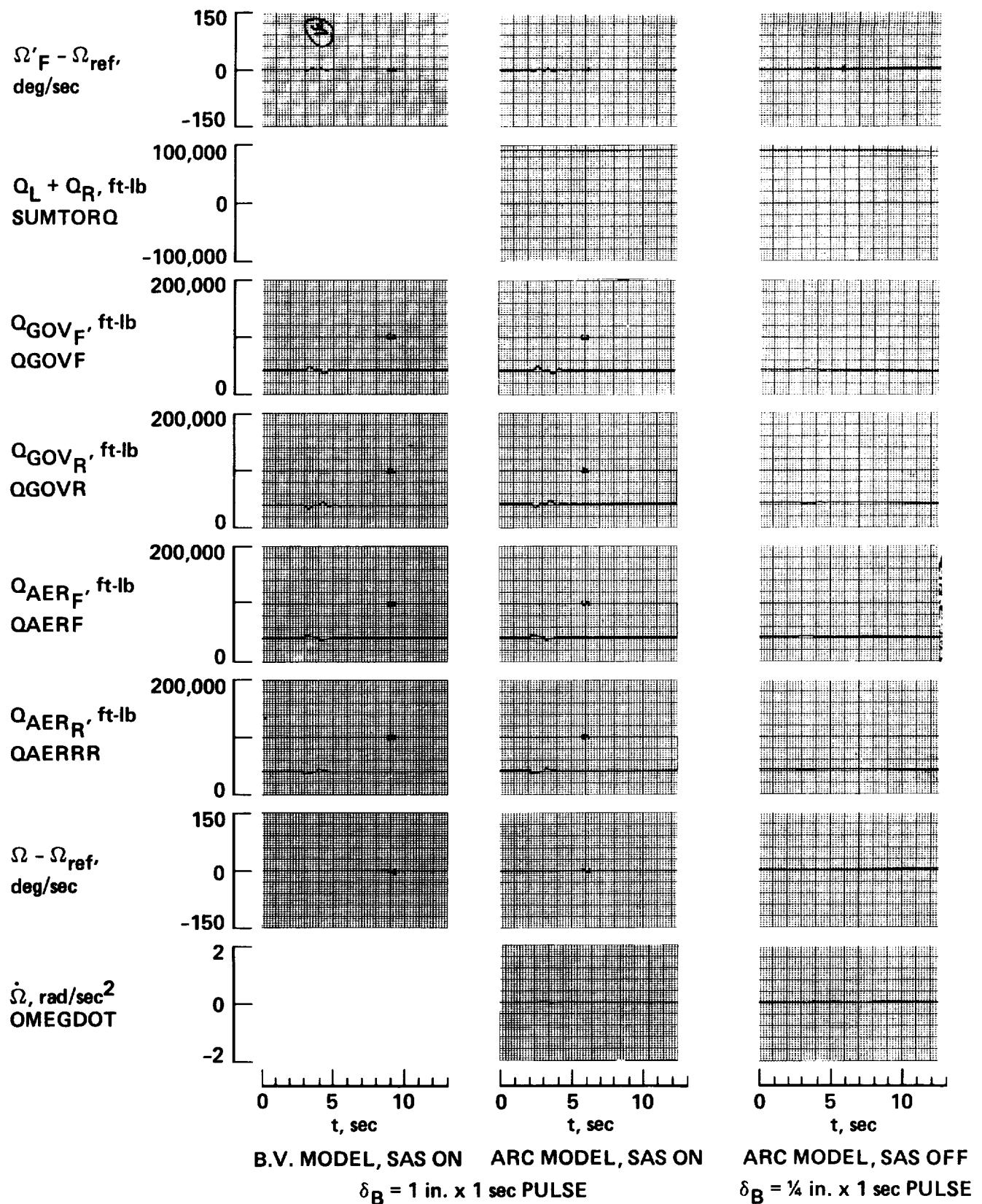


Figure 3.- BV versus ARC simulation response data; hover.

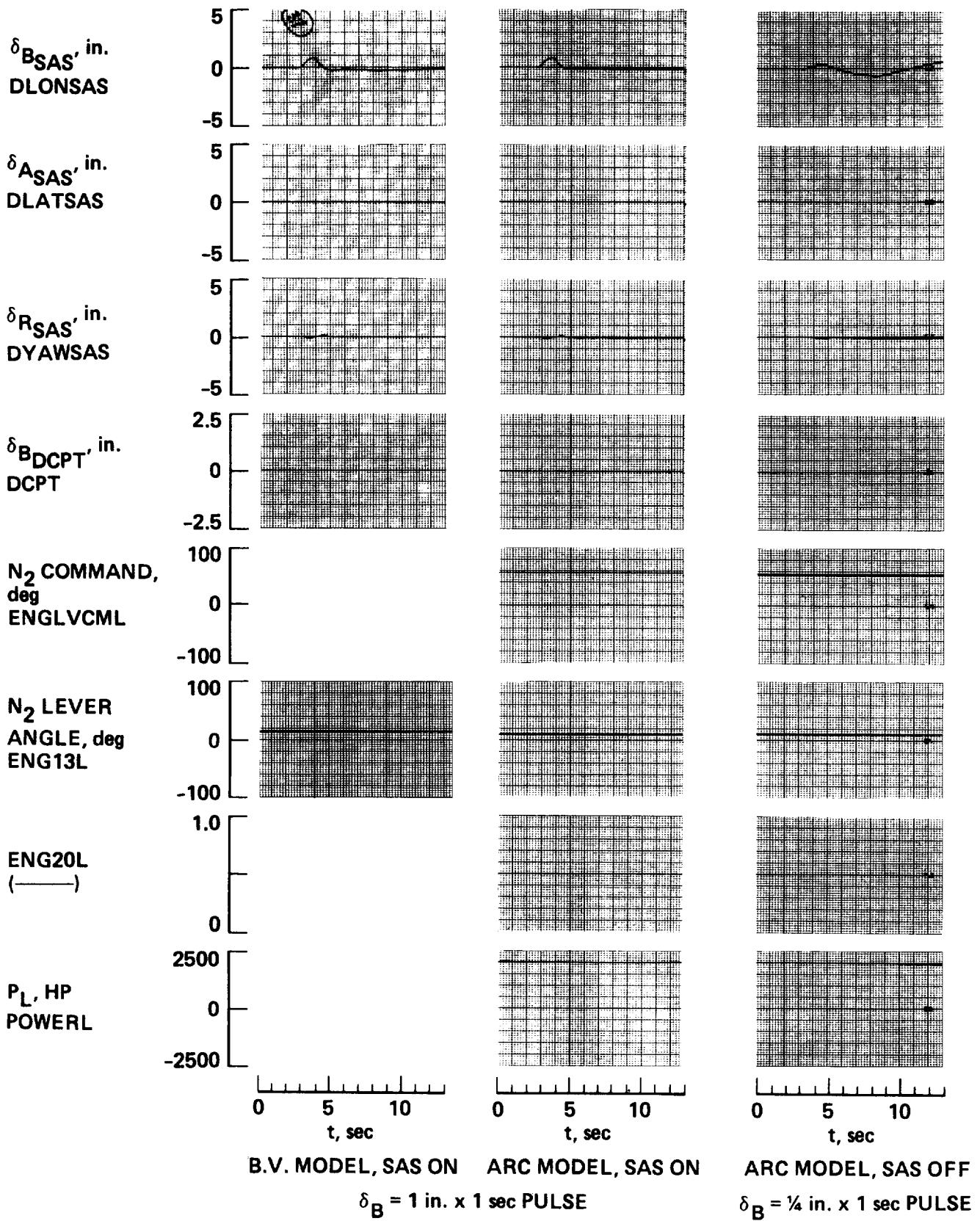


Figure 4.- BV versus ARC simulation response data; hover.

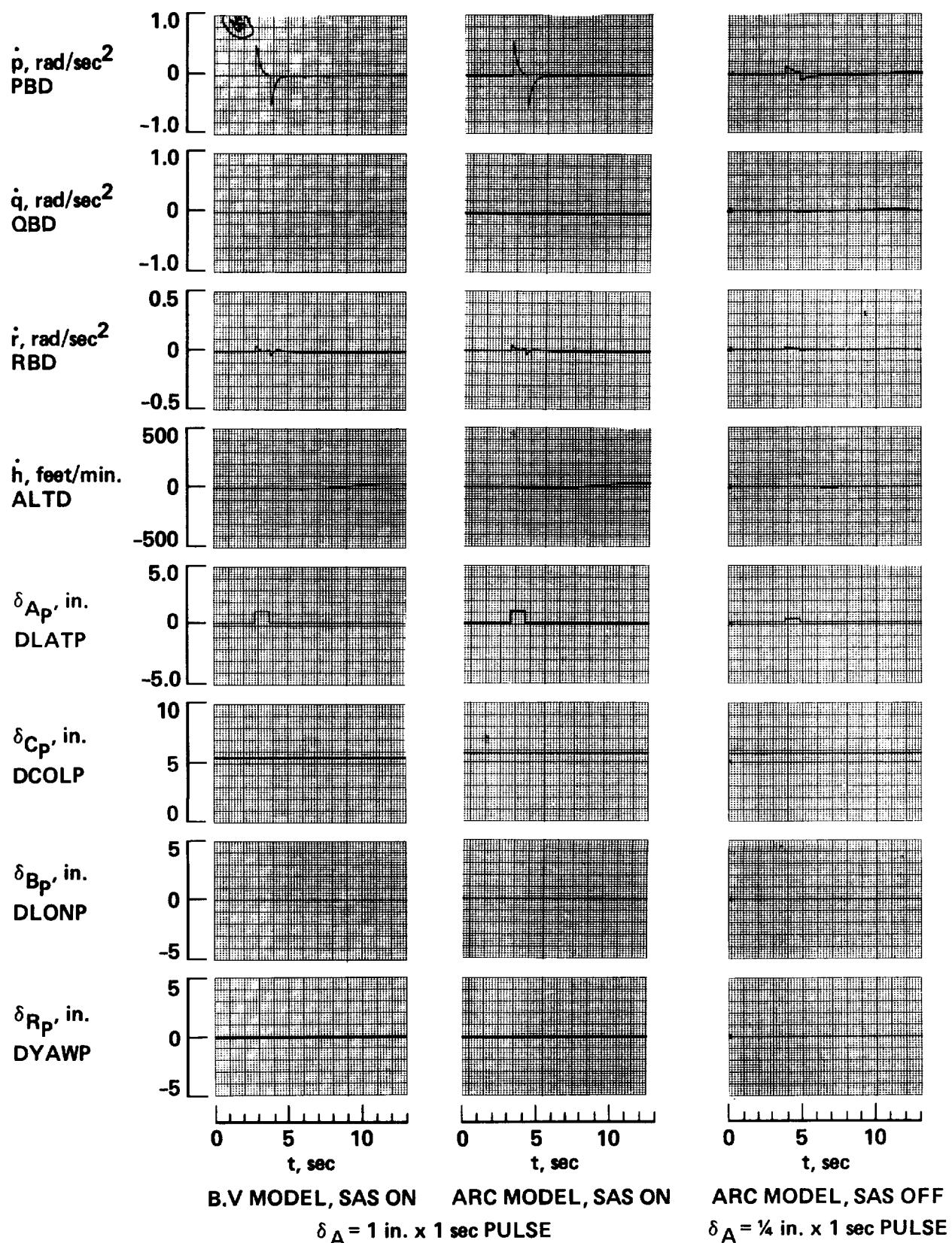


Figure 5.- BV versus ARC simulation response data; hover.

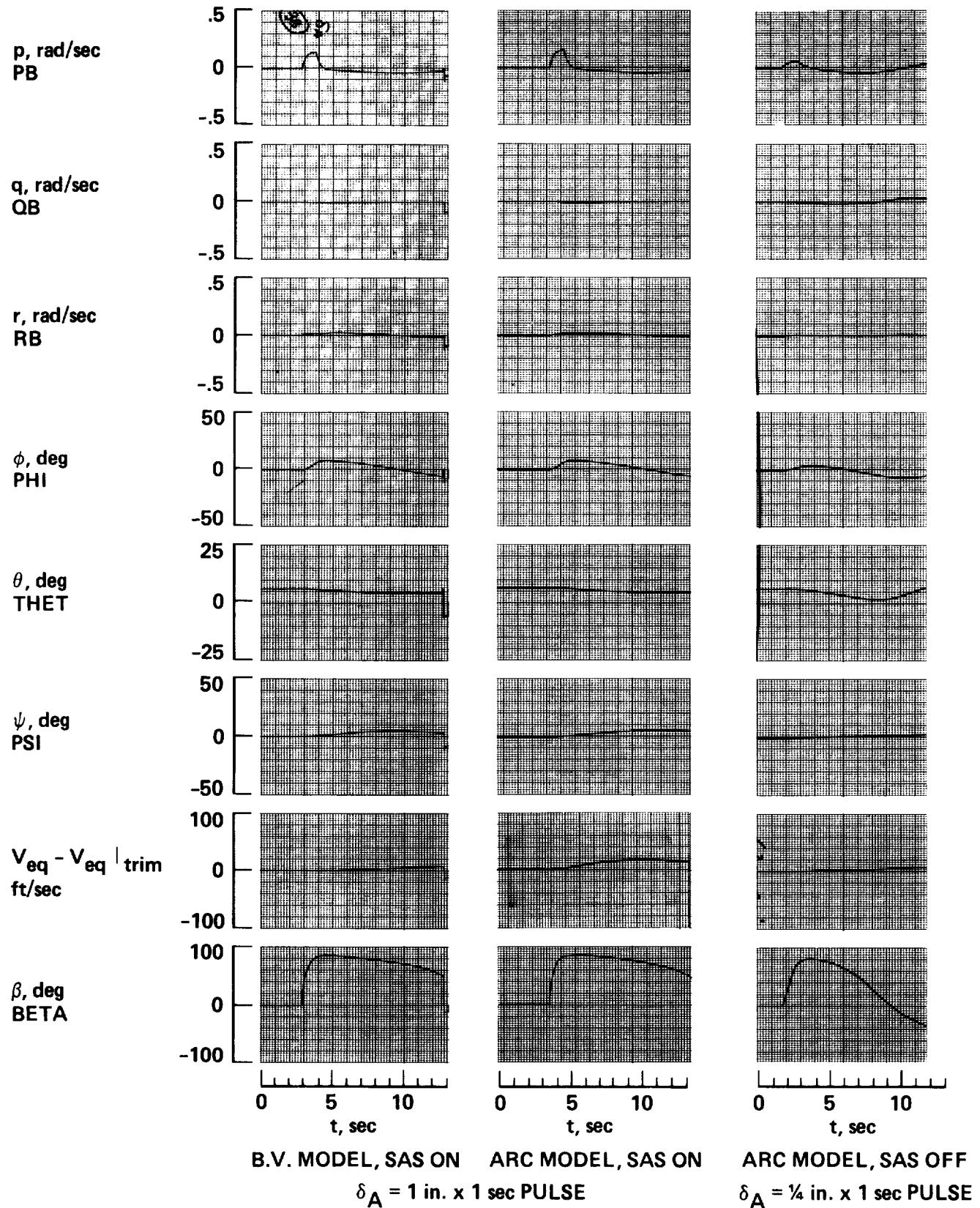


Figure 6.- BV versus ARC simulation response data; hover.

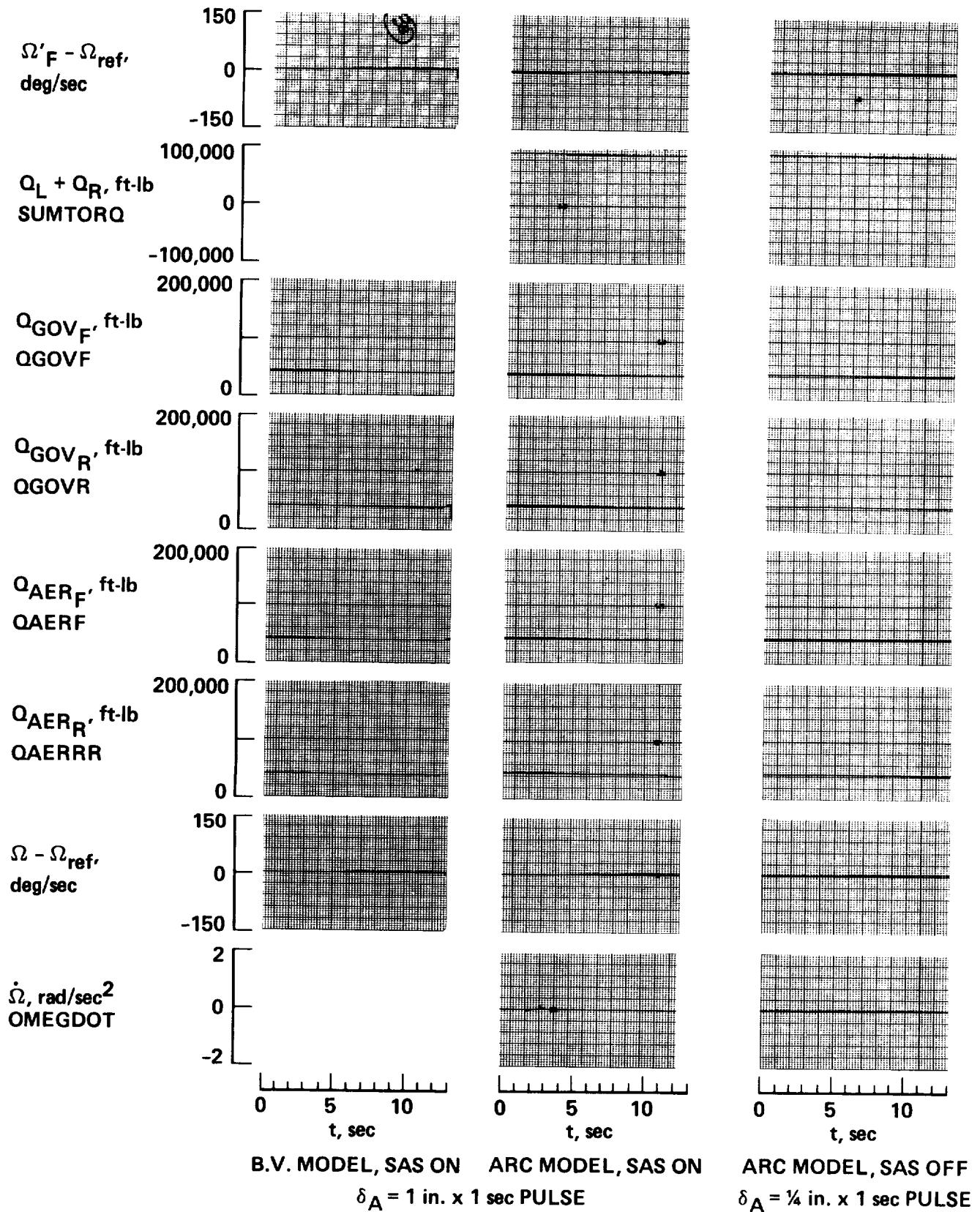


Figure 7.- BV versus ARC simulation response data; hover.

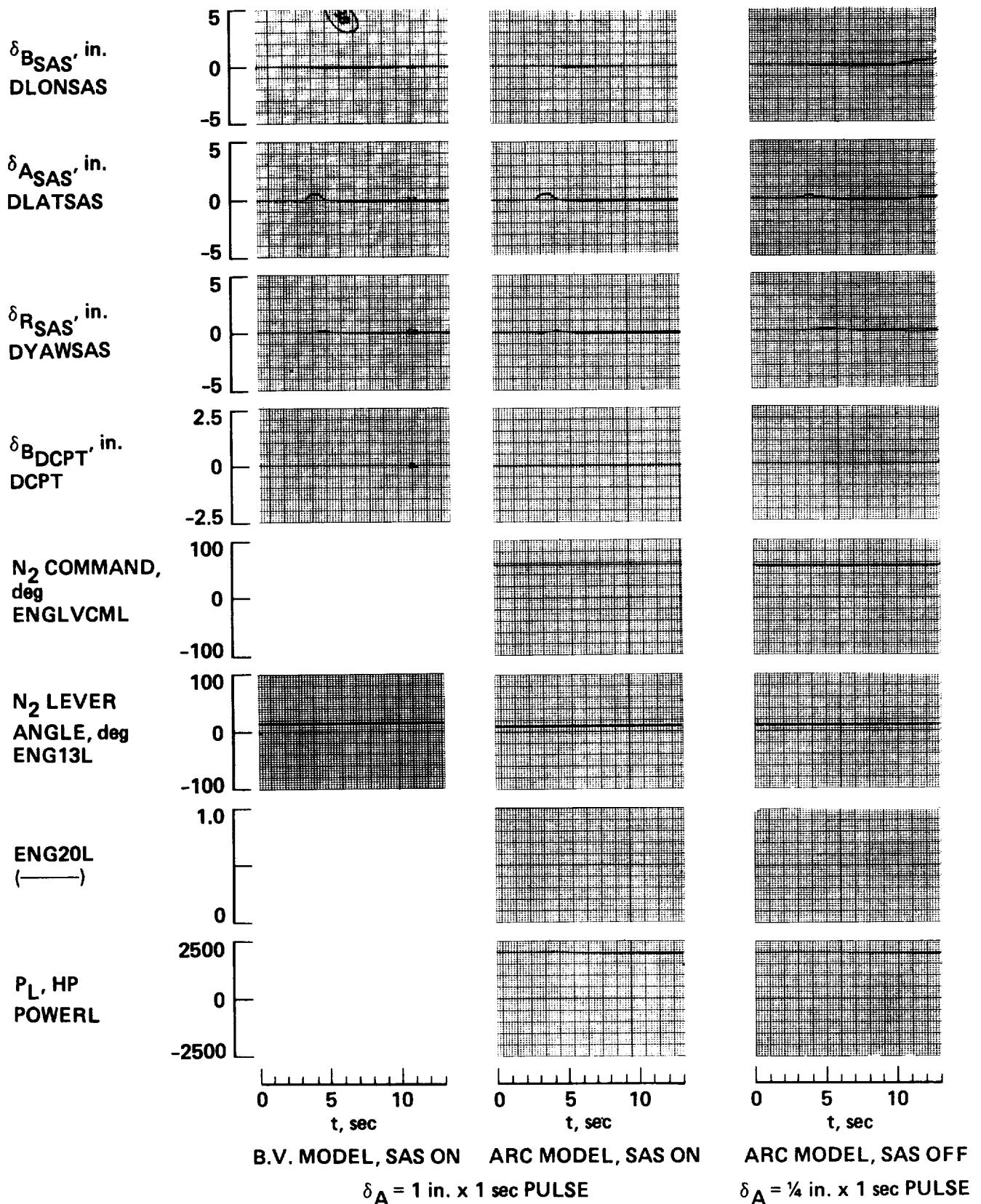


Figure 8.- BV versus ARC simulation response data; hover.

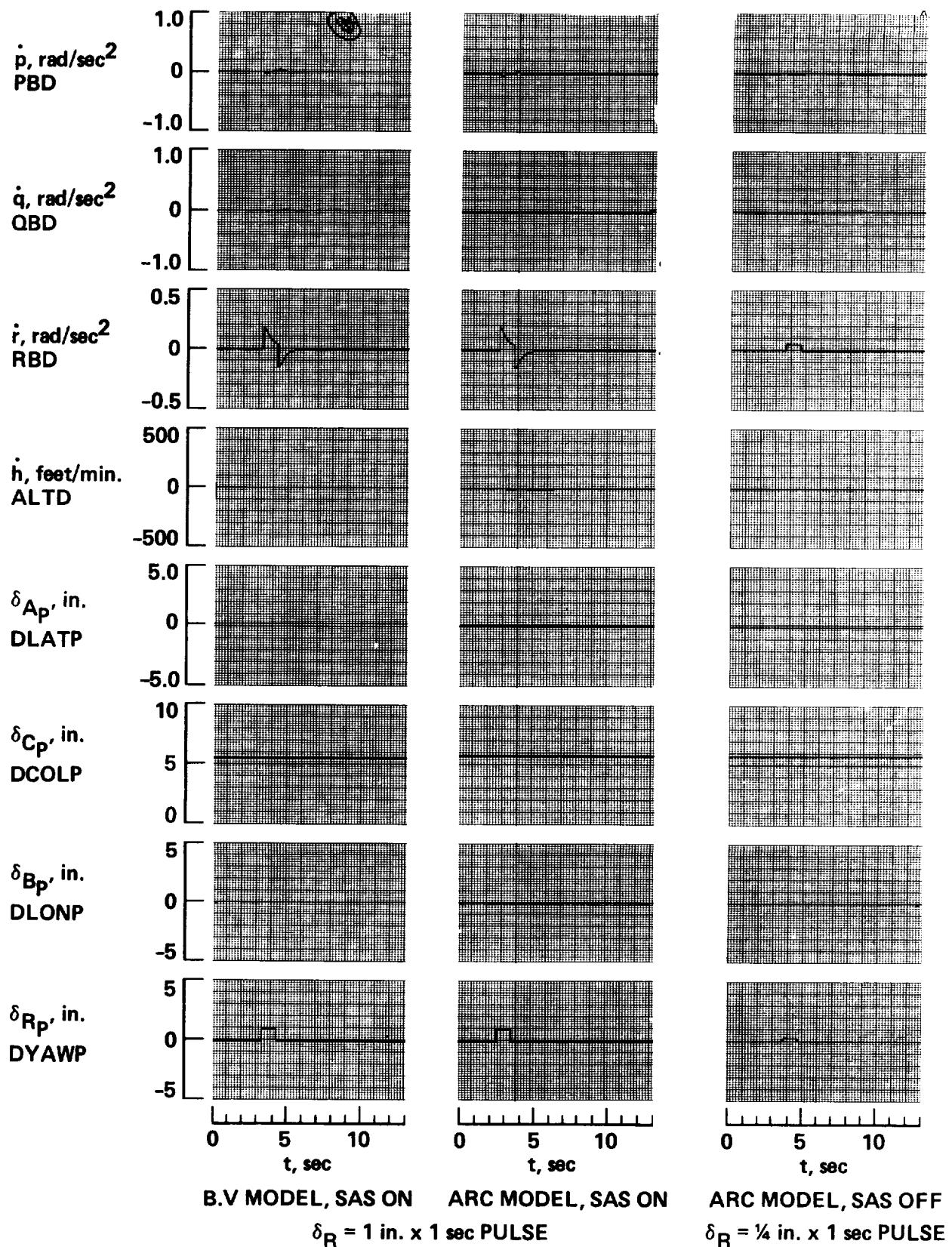


Figure 9.- BV versus ARC simulation response data; hover.

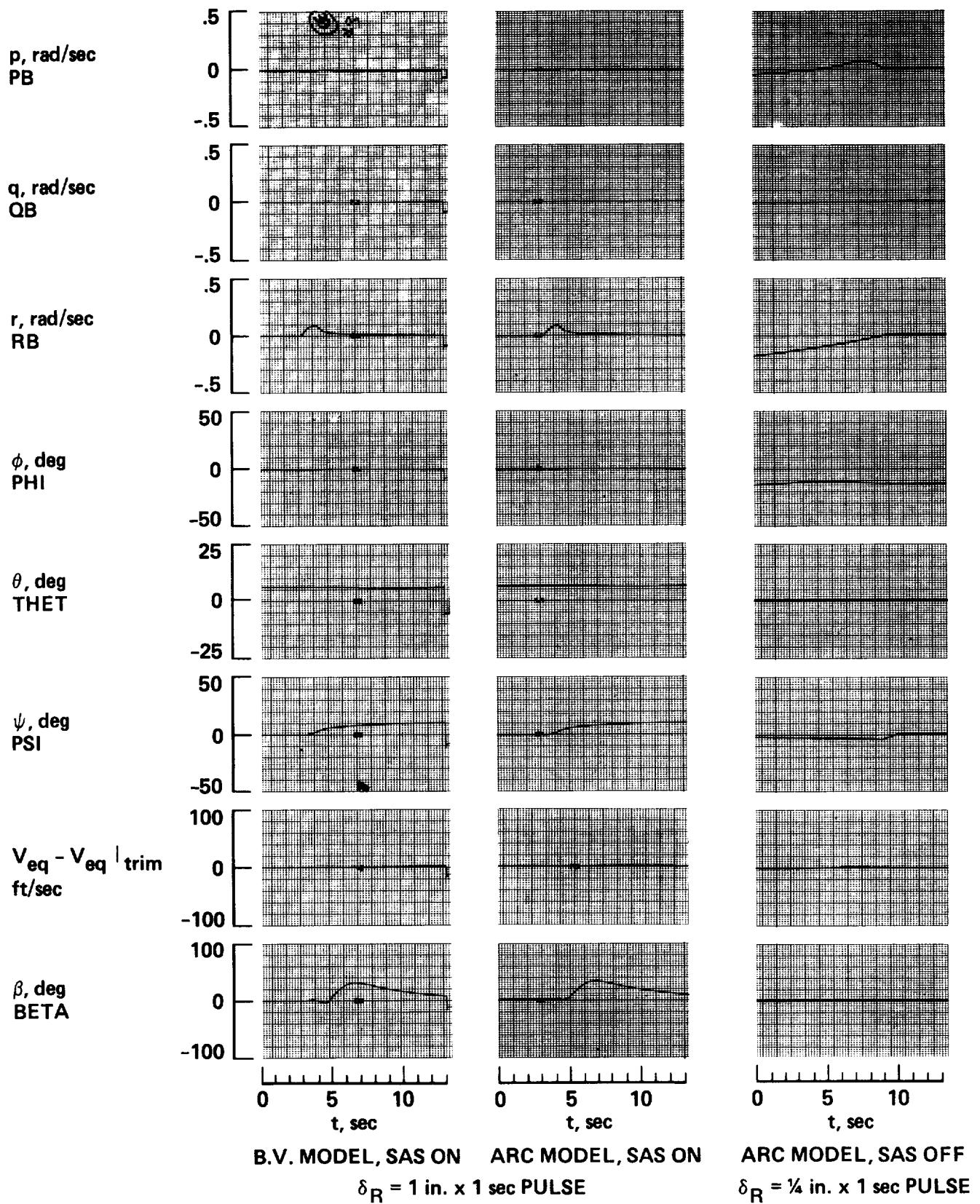


Figure 10.- BV versus ARC simulation response data; hover.

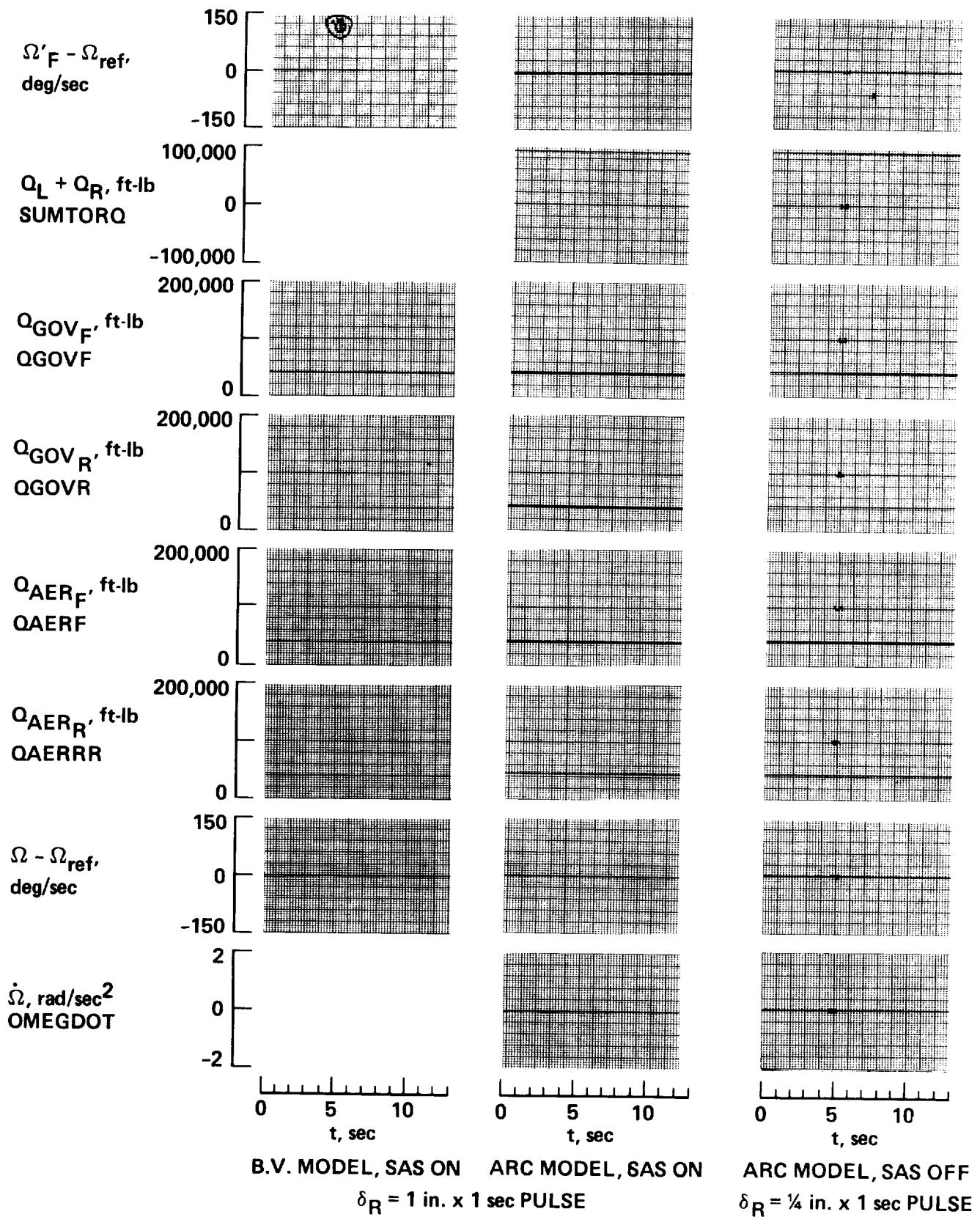


Figure 11.- BV versus ARC simulation response data; hover.

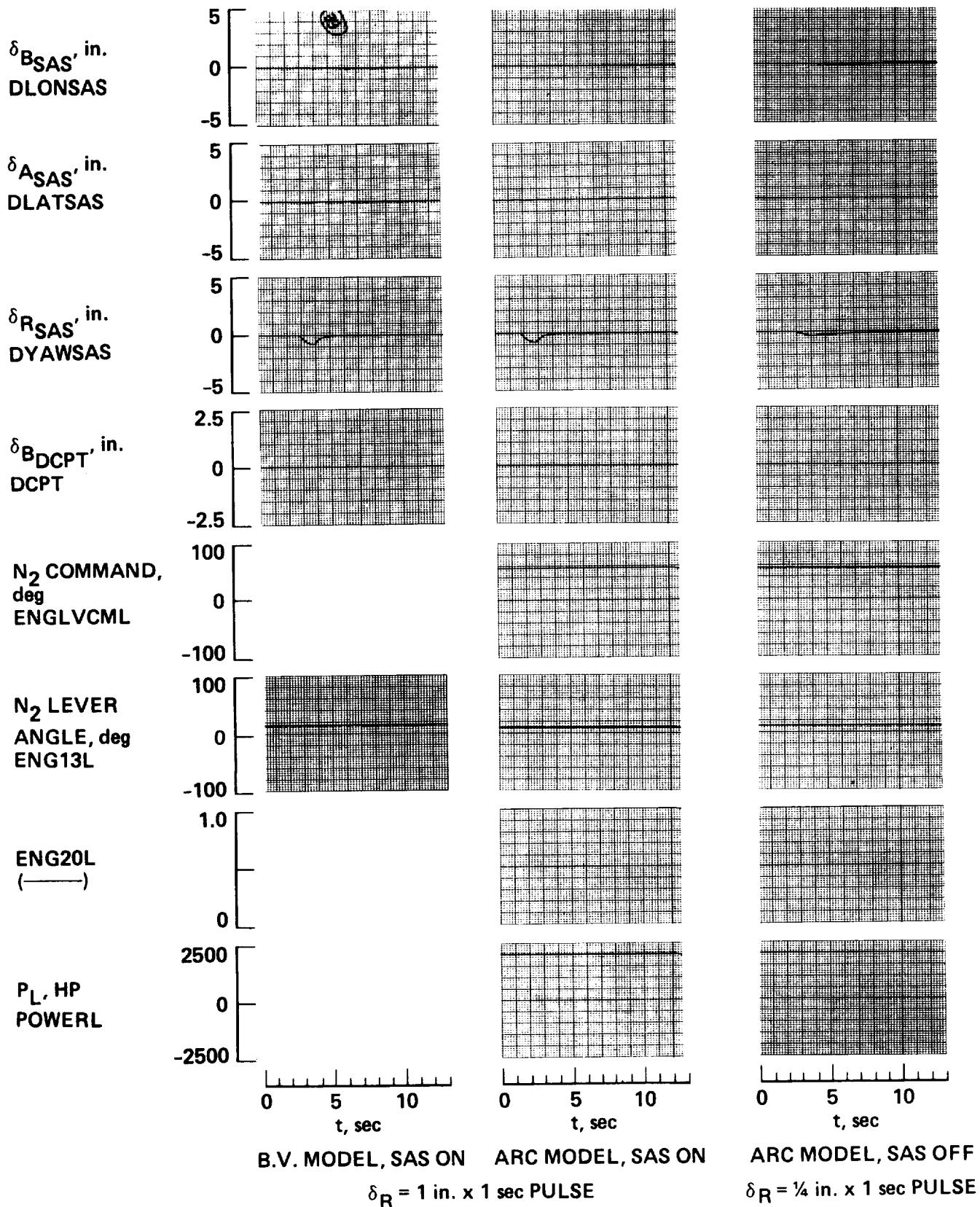


Figure 12.- BV versus ARC simulation response data; hover.

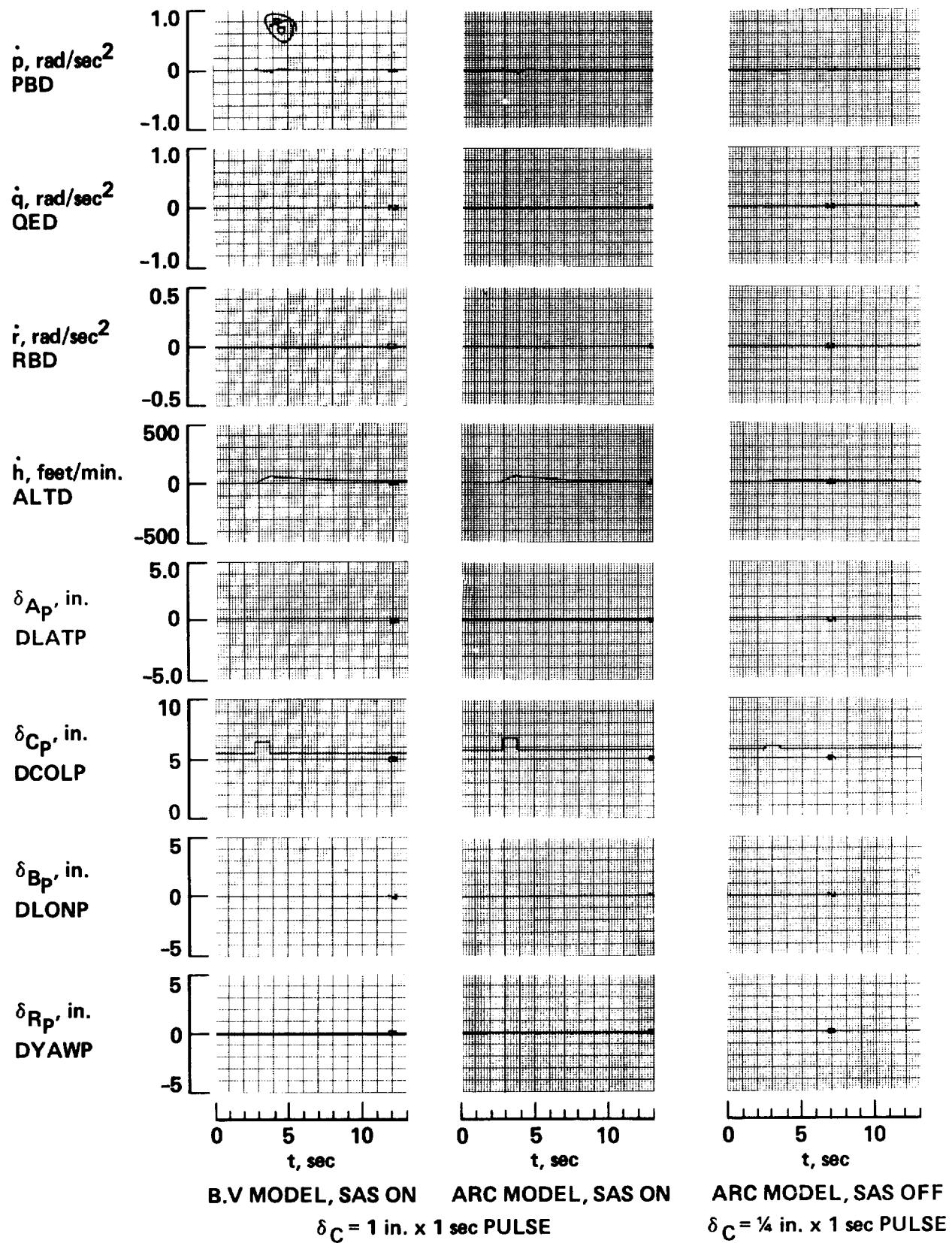


Figure 13.- BV versus ARC simulation response data; hover.

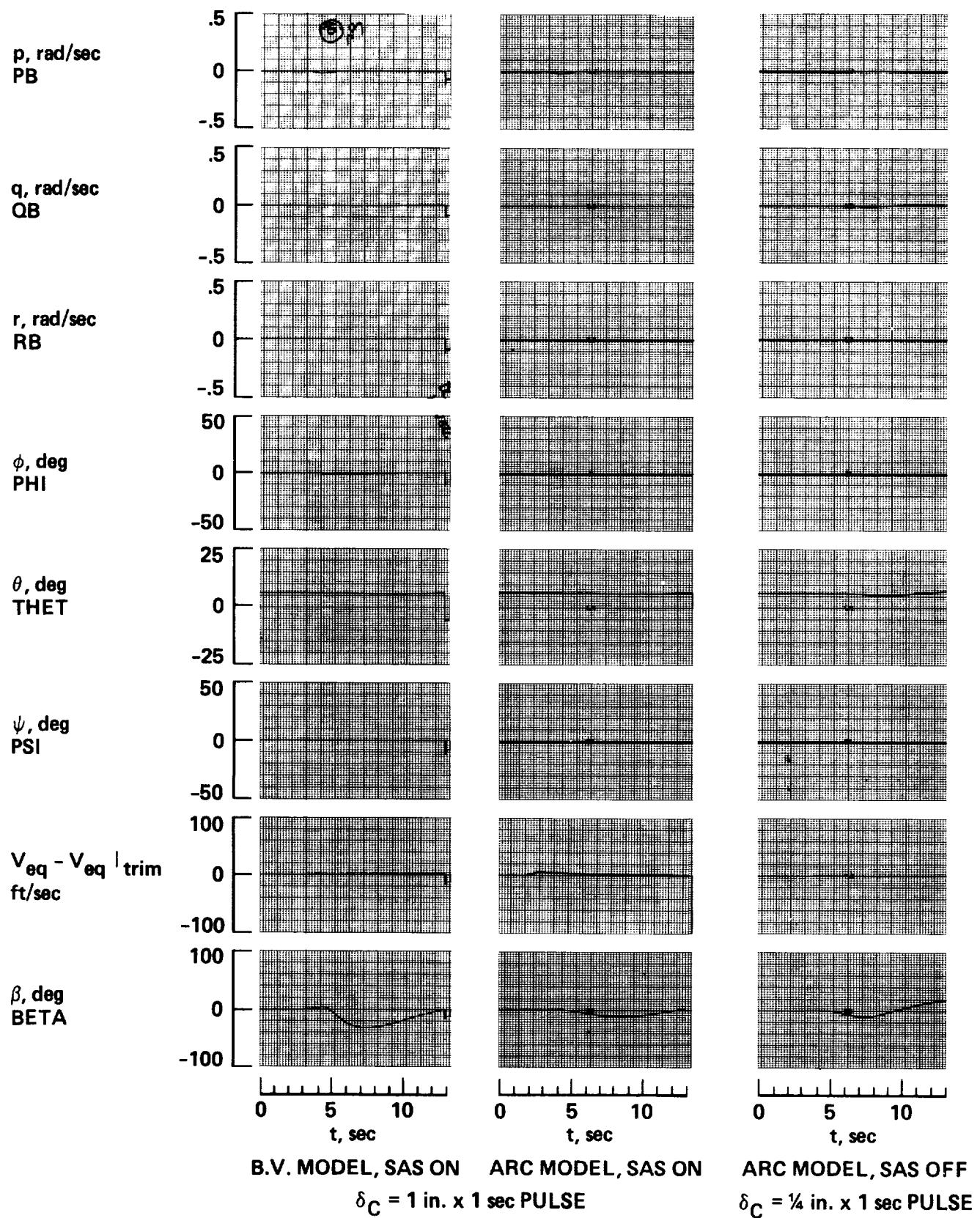


Figure 14.- BV versus ARC simulation response data; hover.

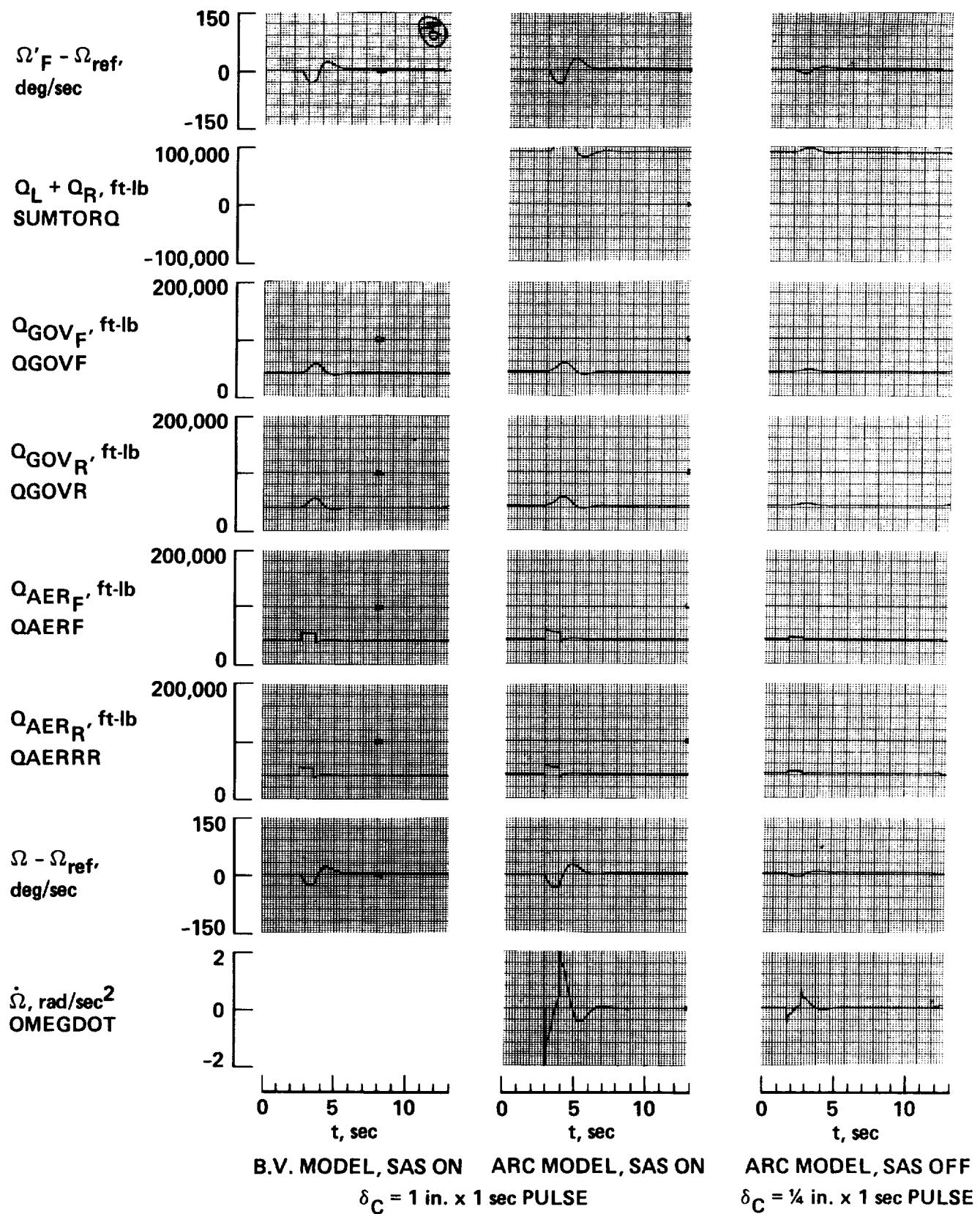


Figure 15.- BV versus ARC simulation response data; hover.

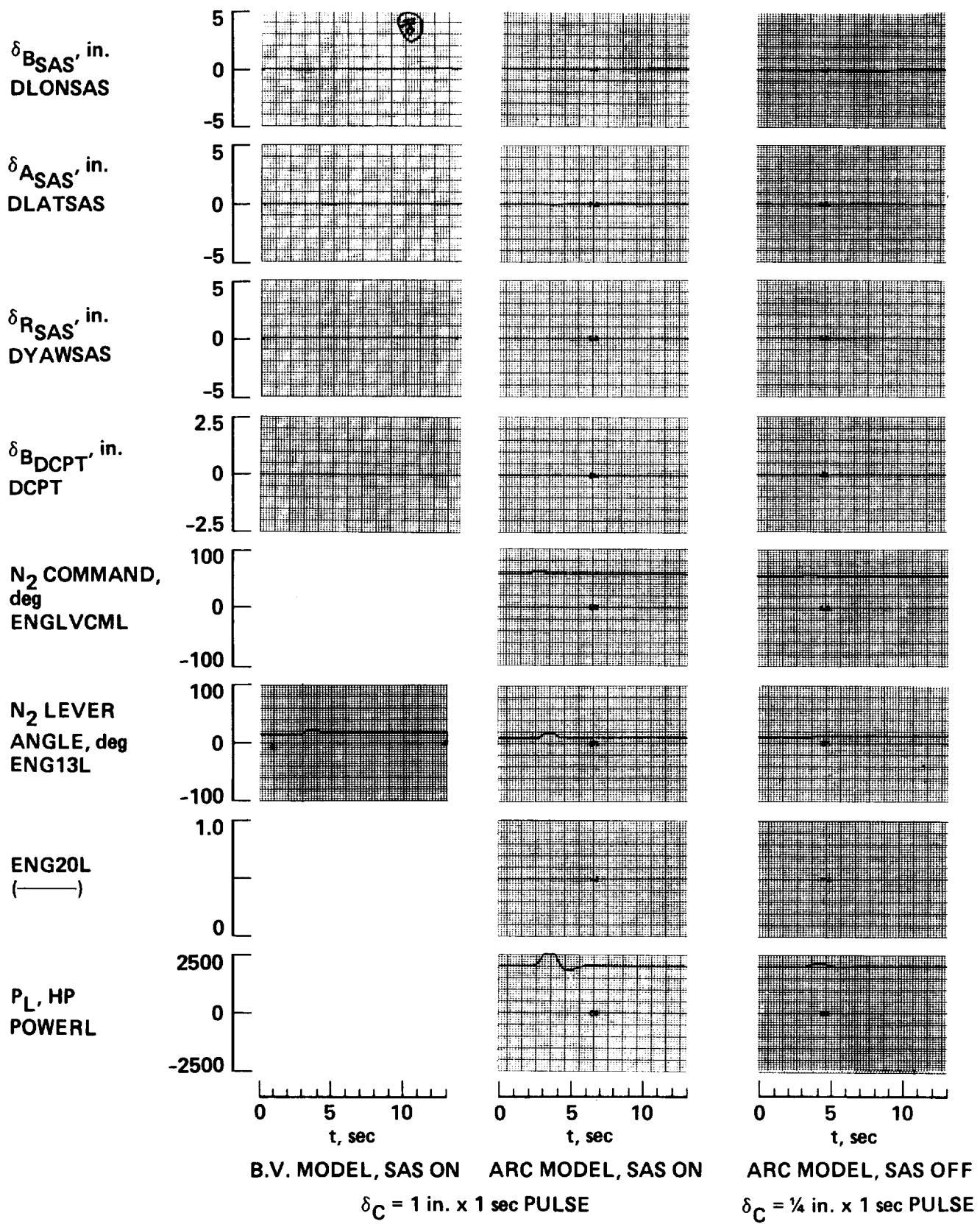


Figure 16.- BV versus ARC simulation response data; hover.

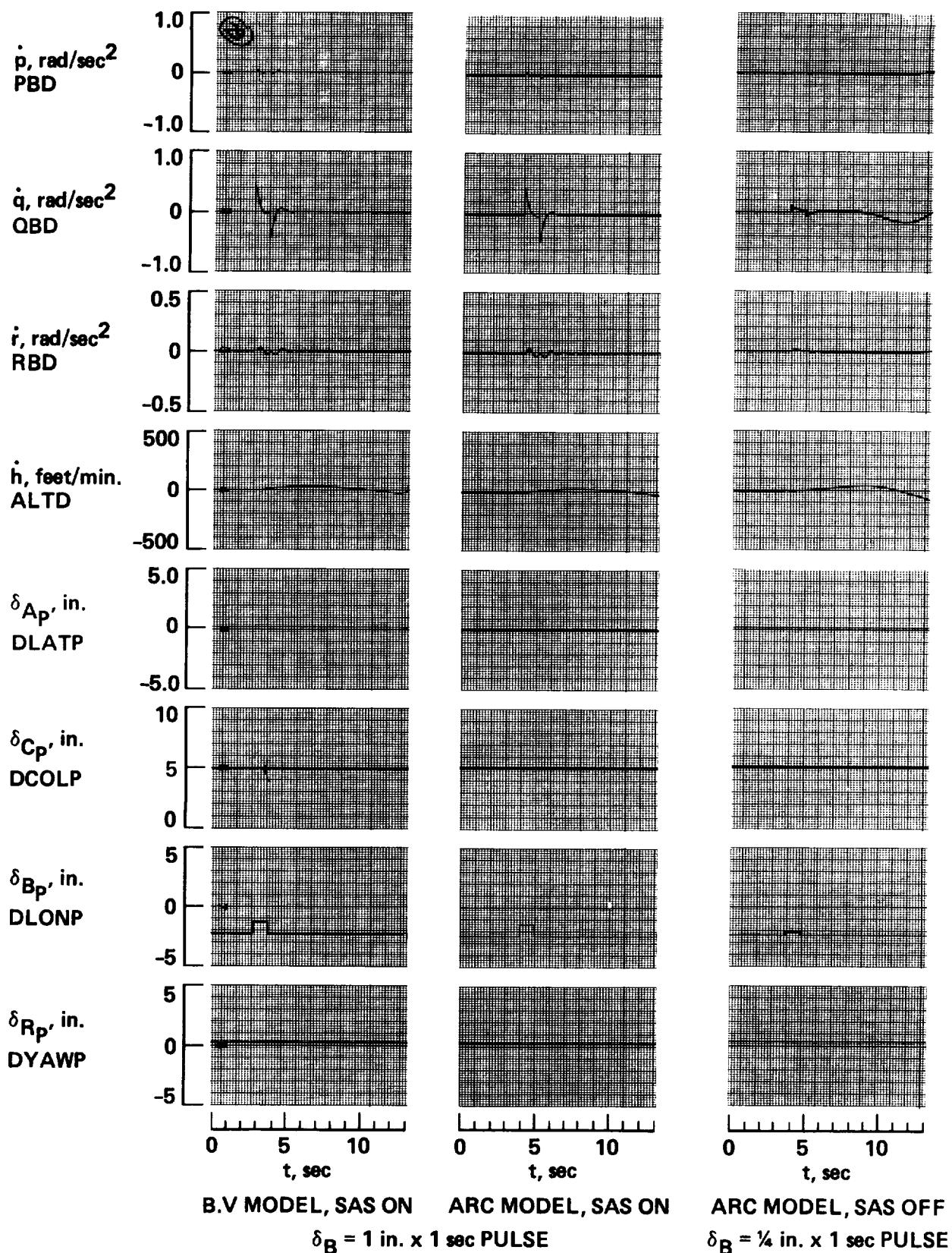


Figure 17.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

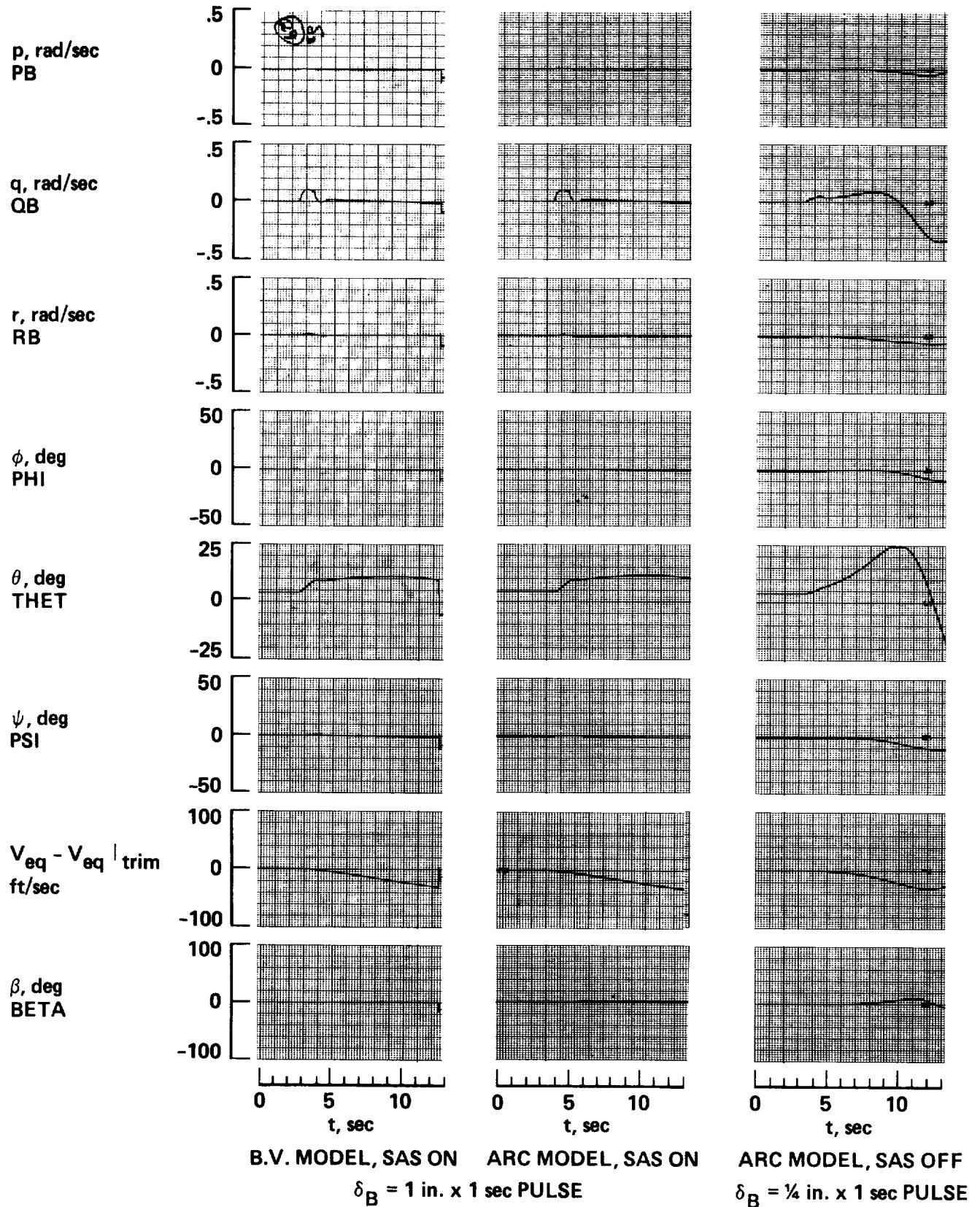


Figure 18.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

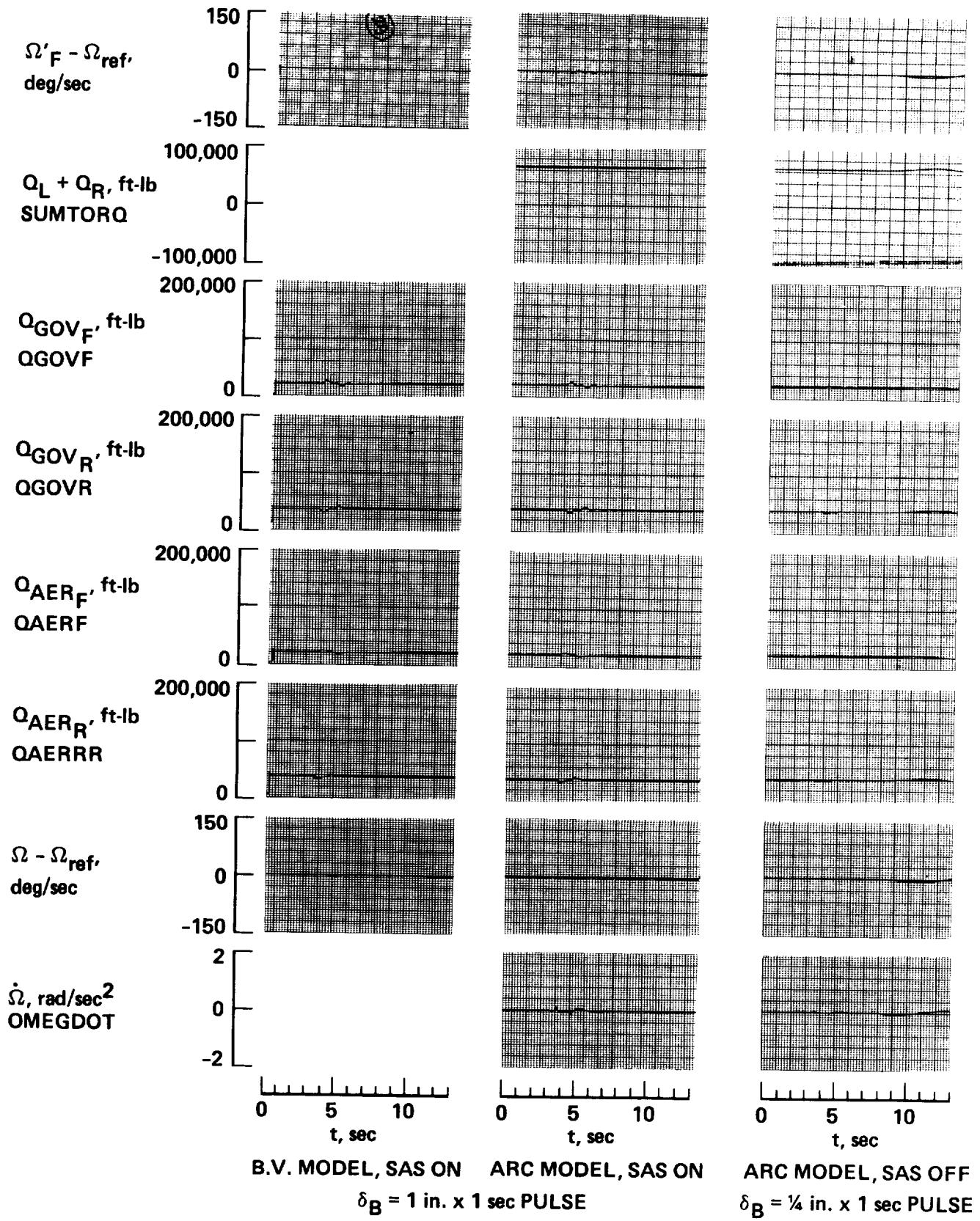


Figure 19.- BV versus ARC simulation response data; $V_{\text{eq}} = 40$ knots.

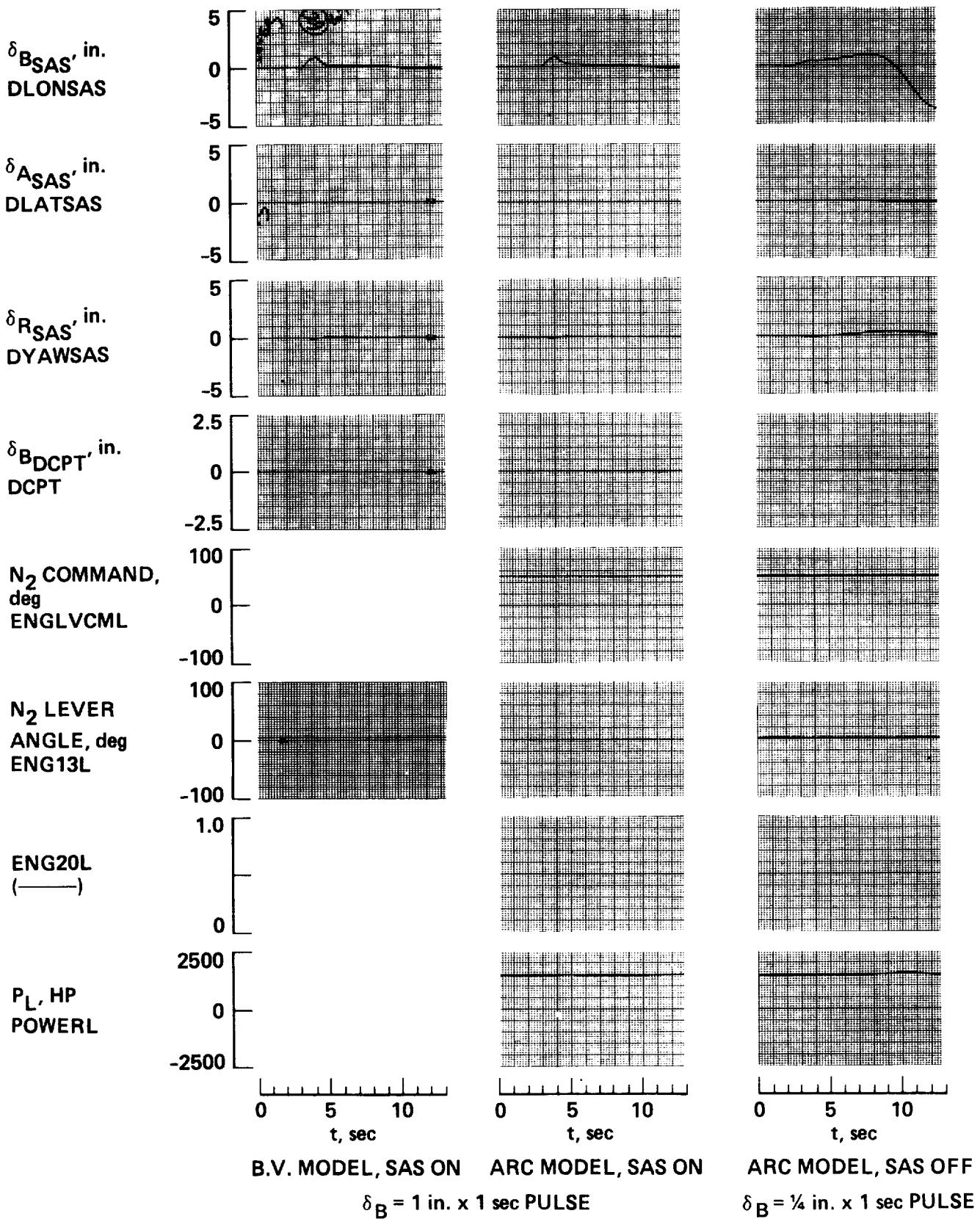


Figure 20.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

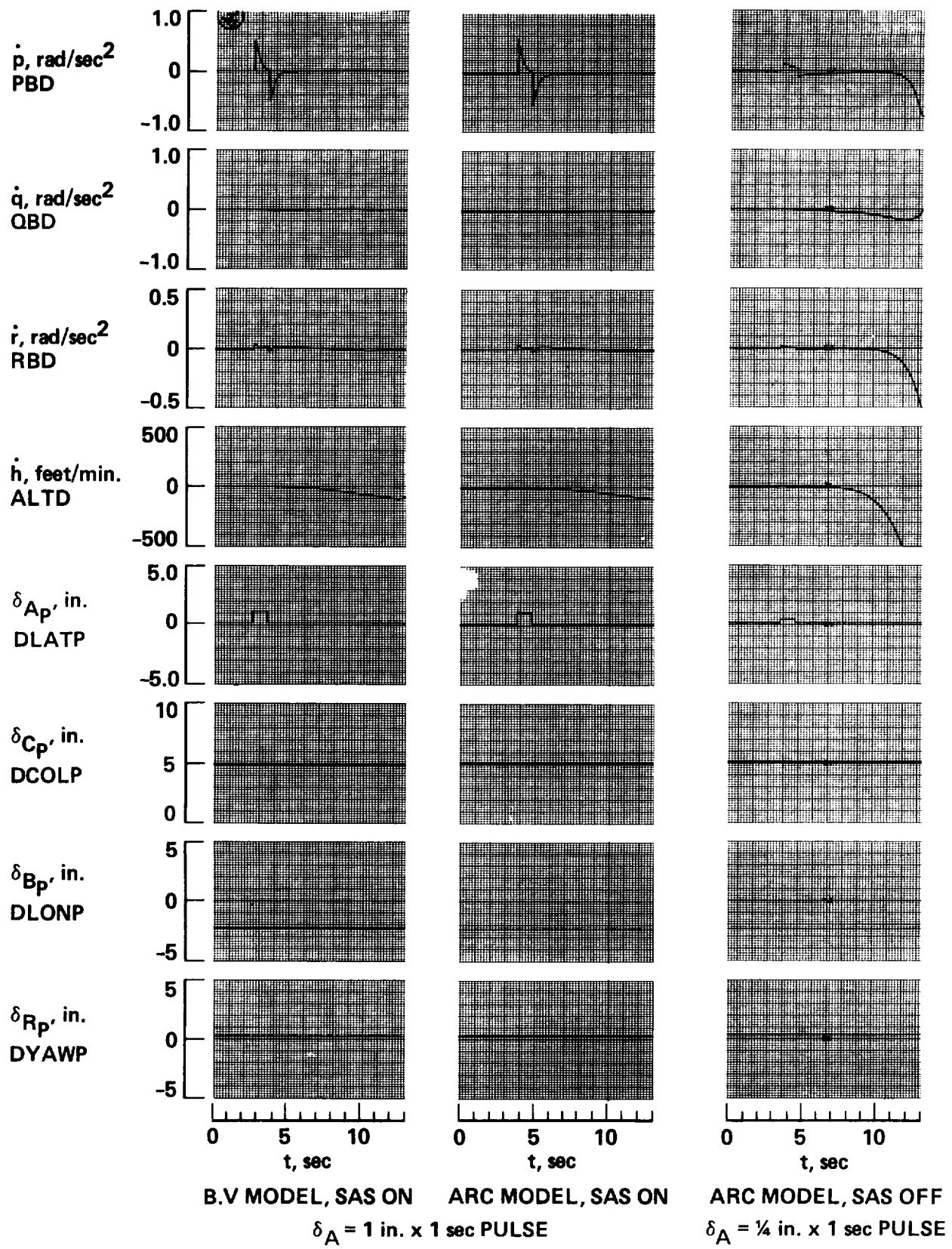


Figure 21.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

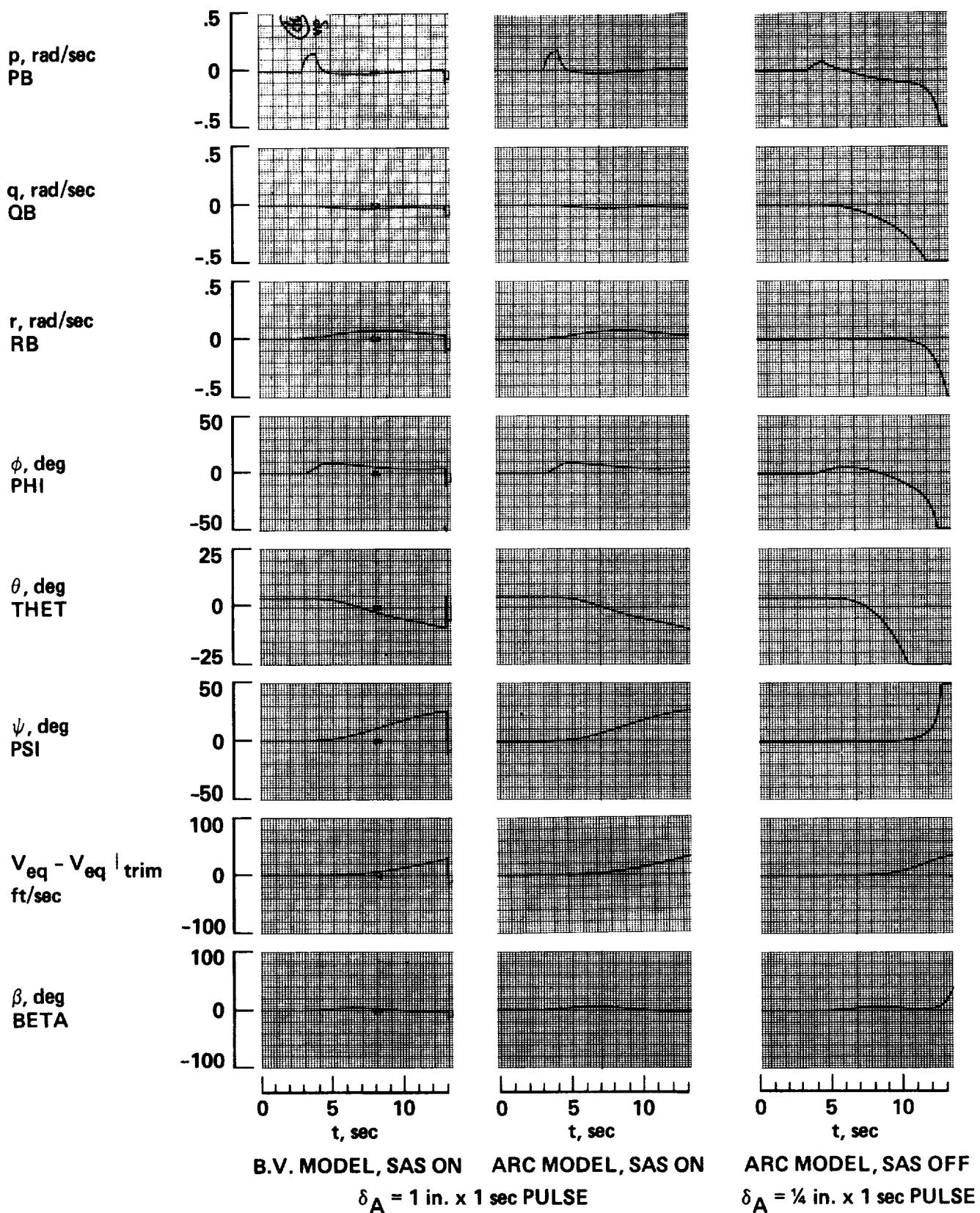


Figure 22.- BV versus ARC simulation response data; $V_{\text{eq}} = 40$ knots.

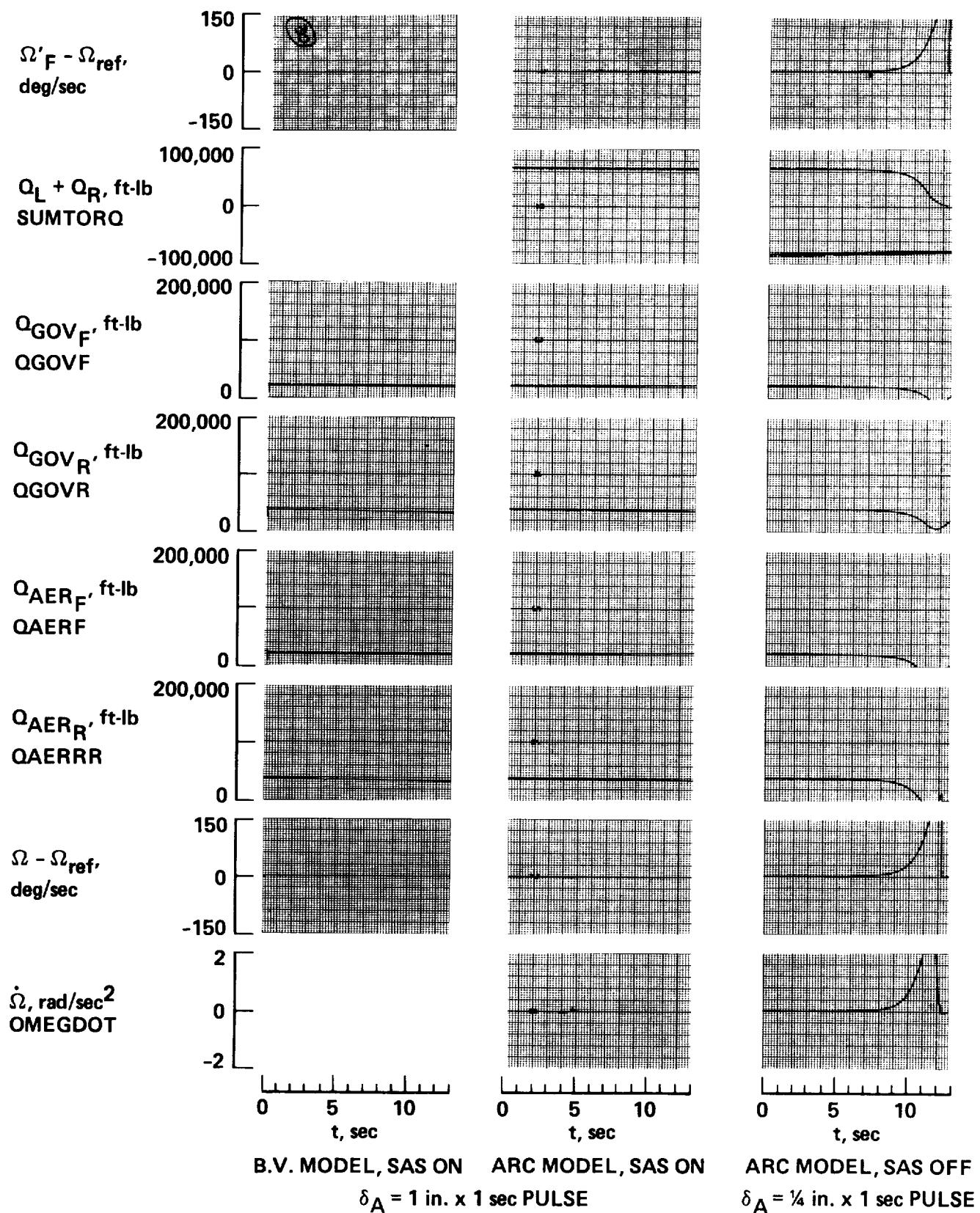


Figure 23.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

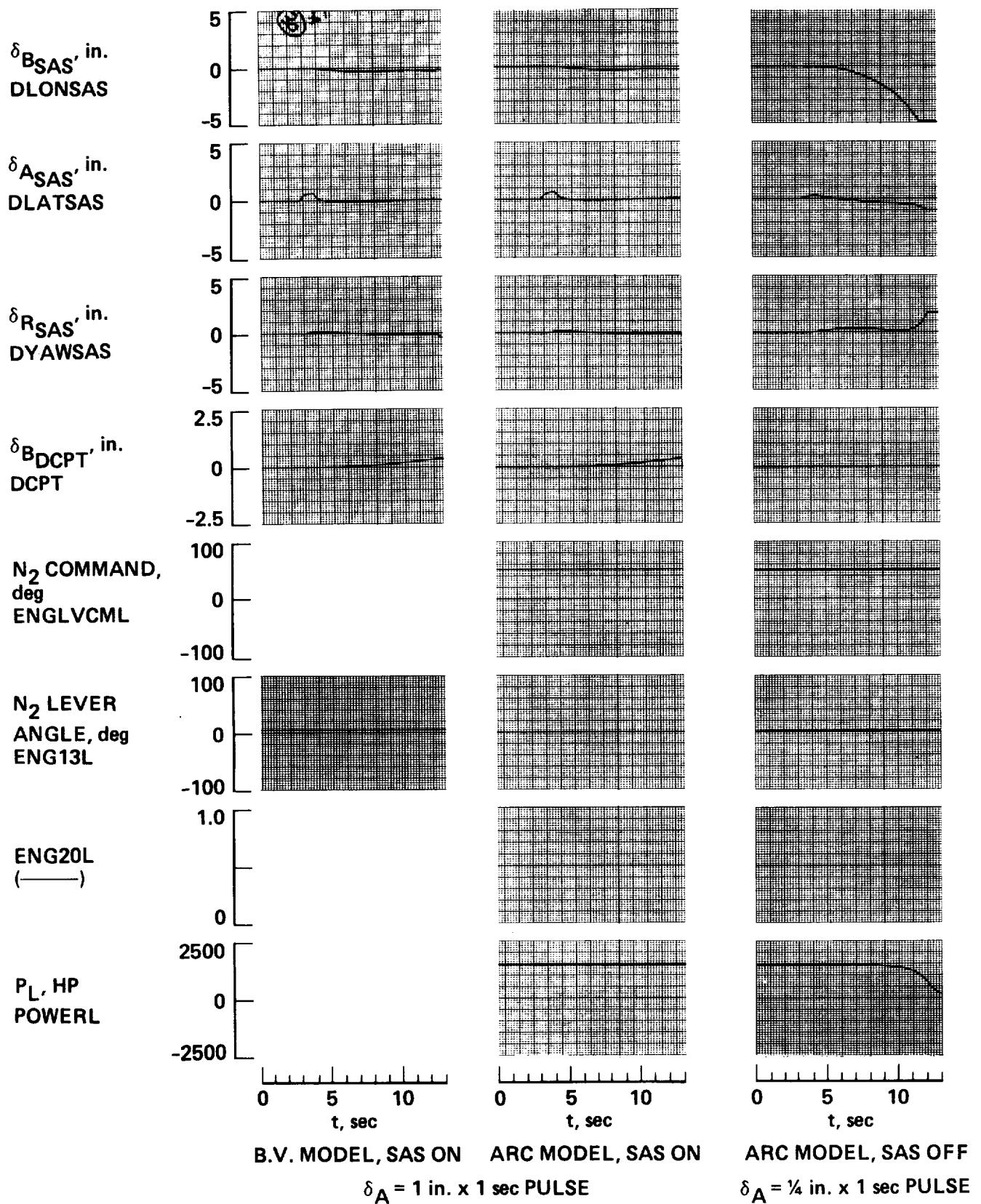


Figure 24.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

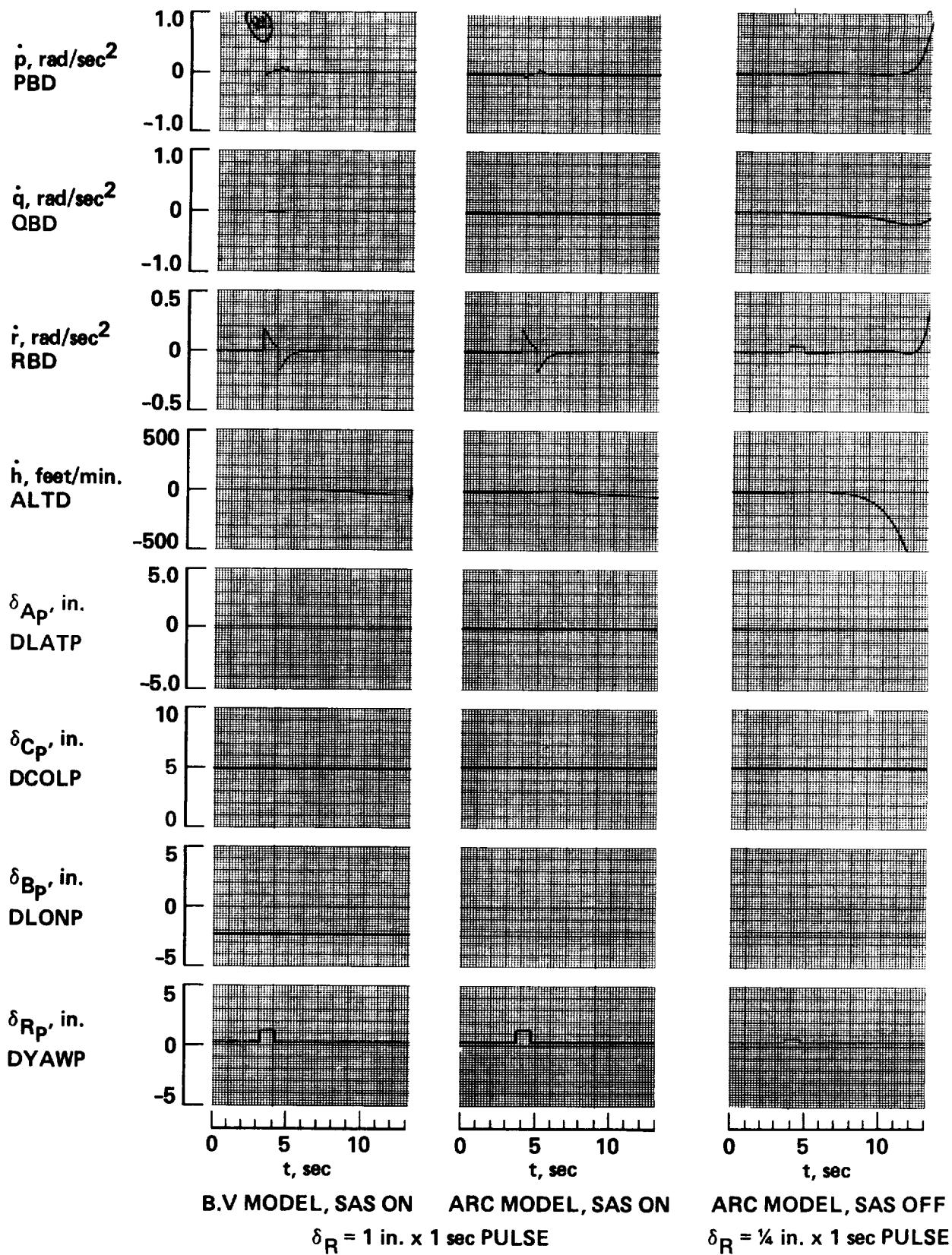


Figure 25.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

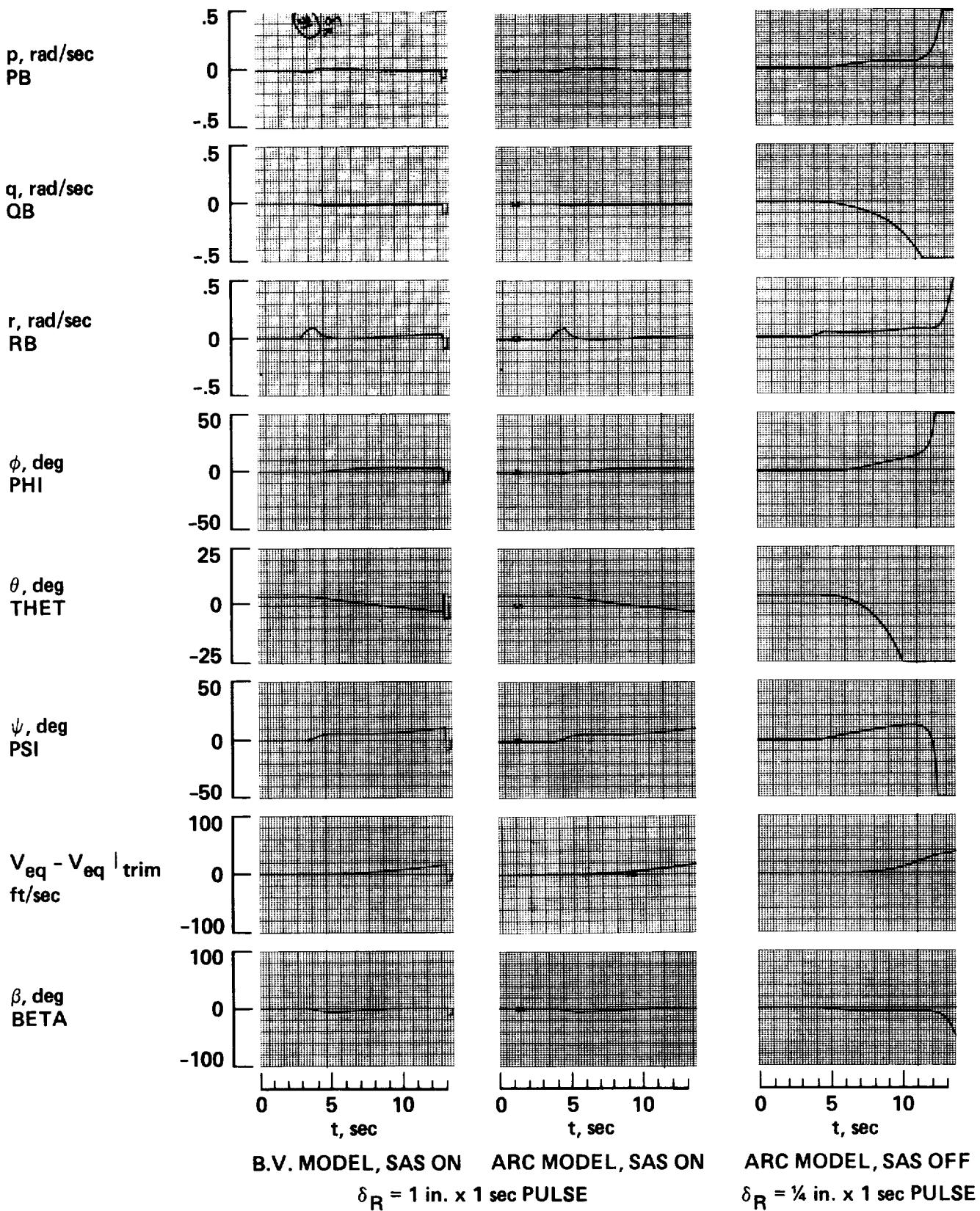


Figure 26.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

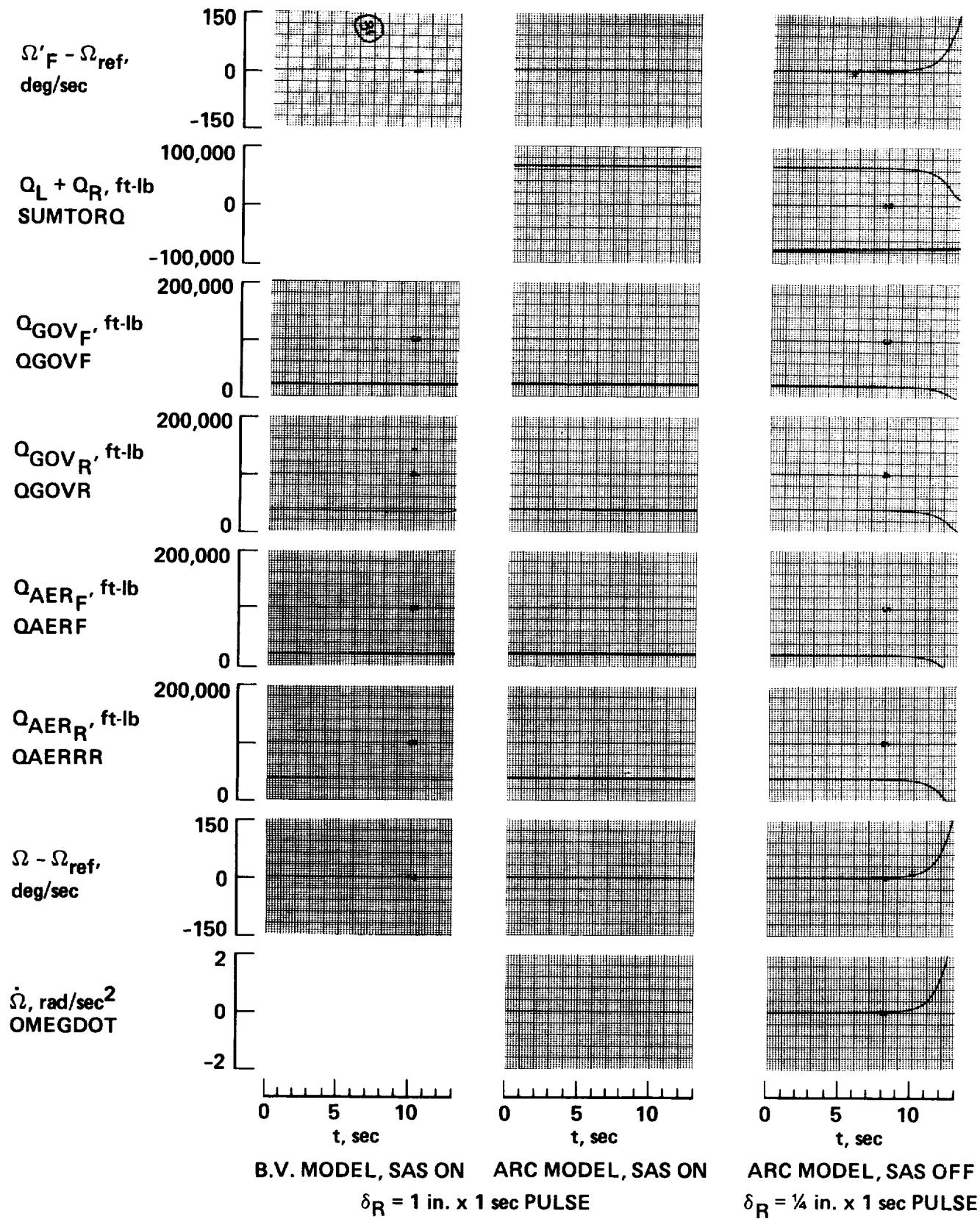


Figure 27.- BV versus ARC simulation response data; $V_{\text{eq}} = 40$ knots.

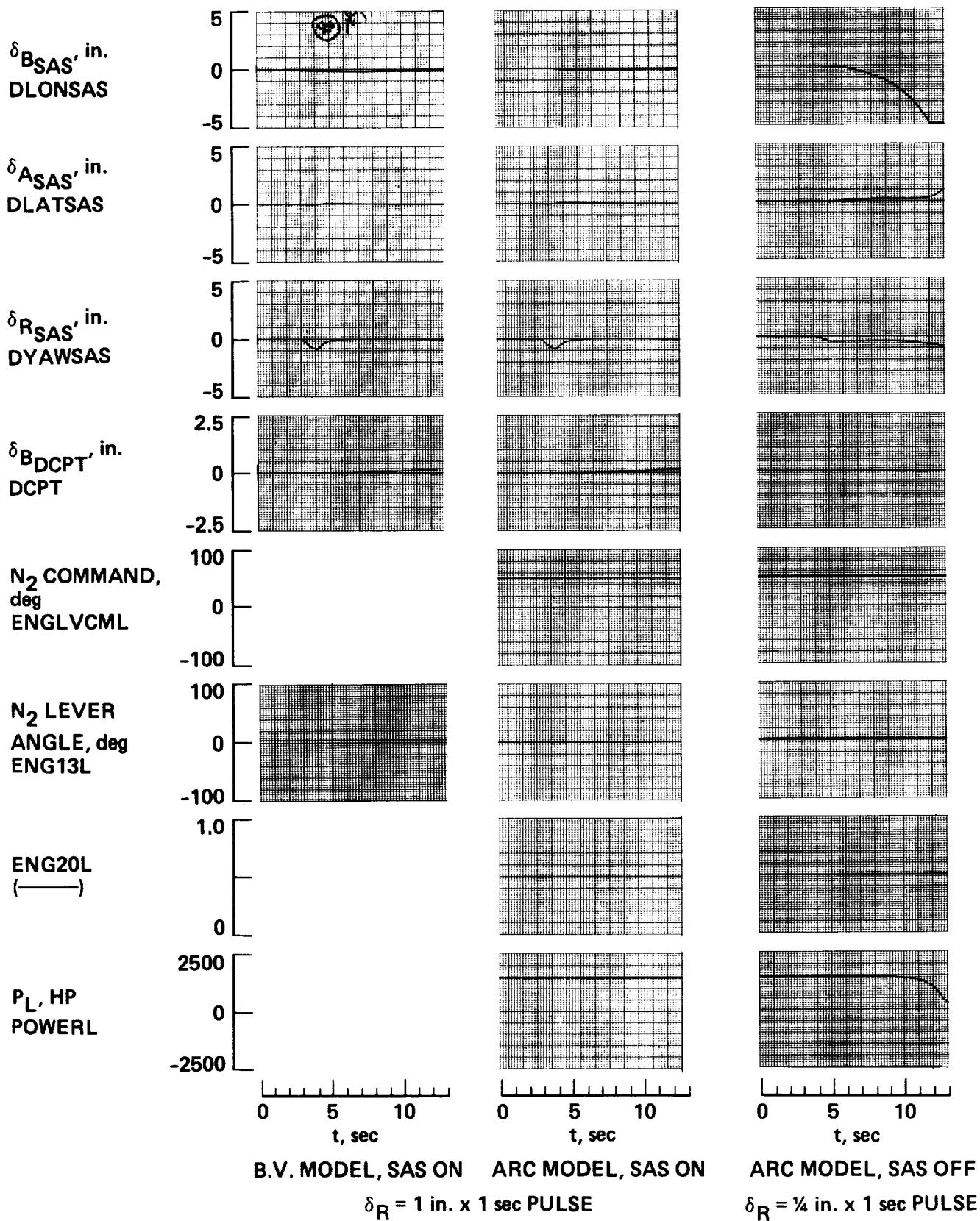


Figure 28.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

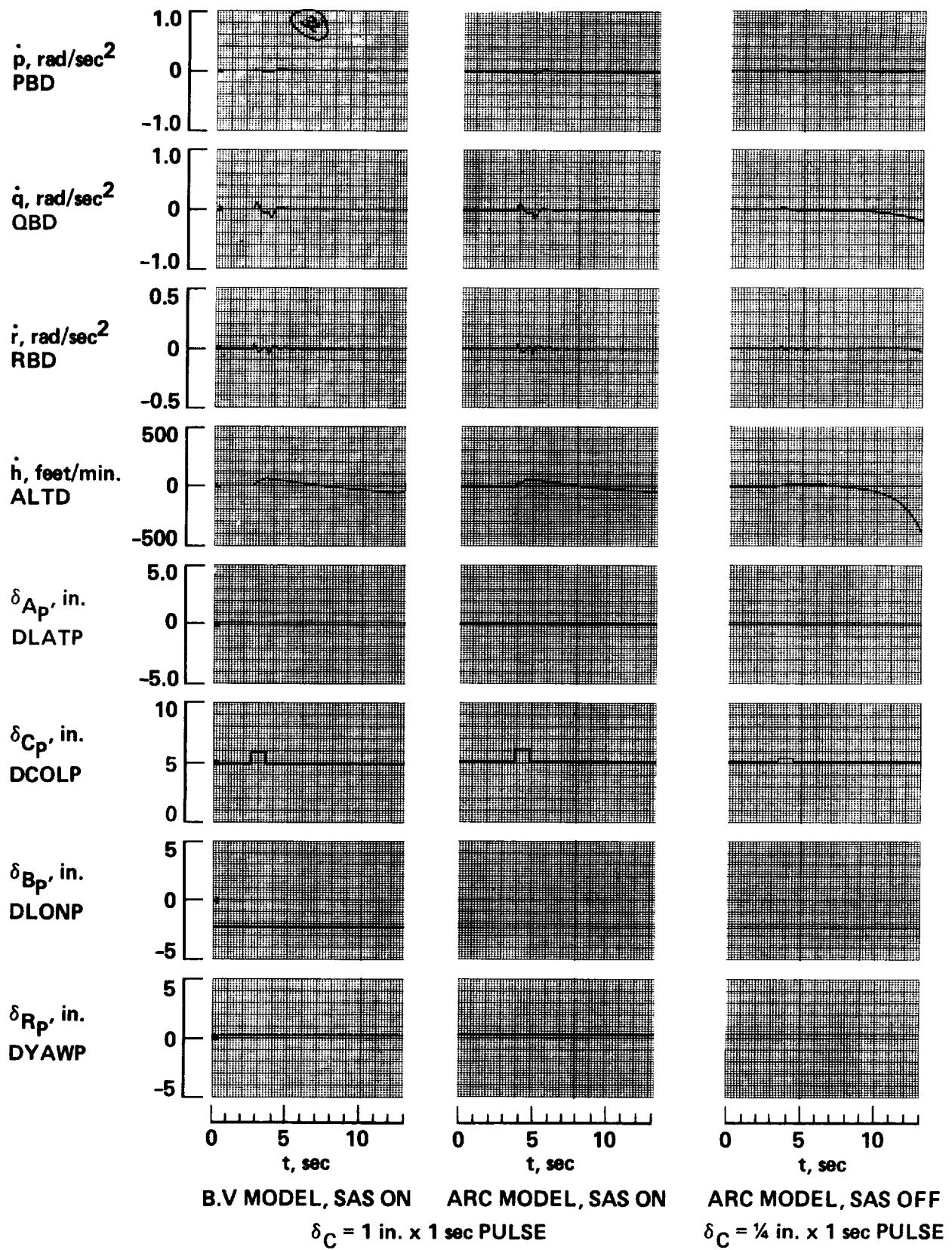


Figure 29.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

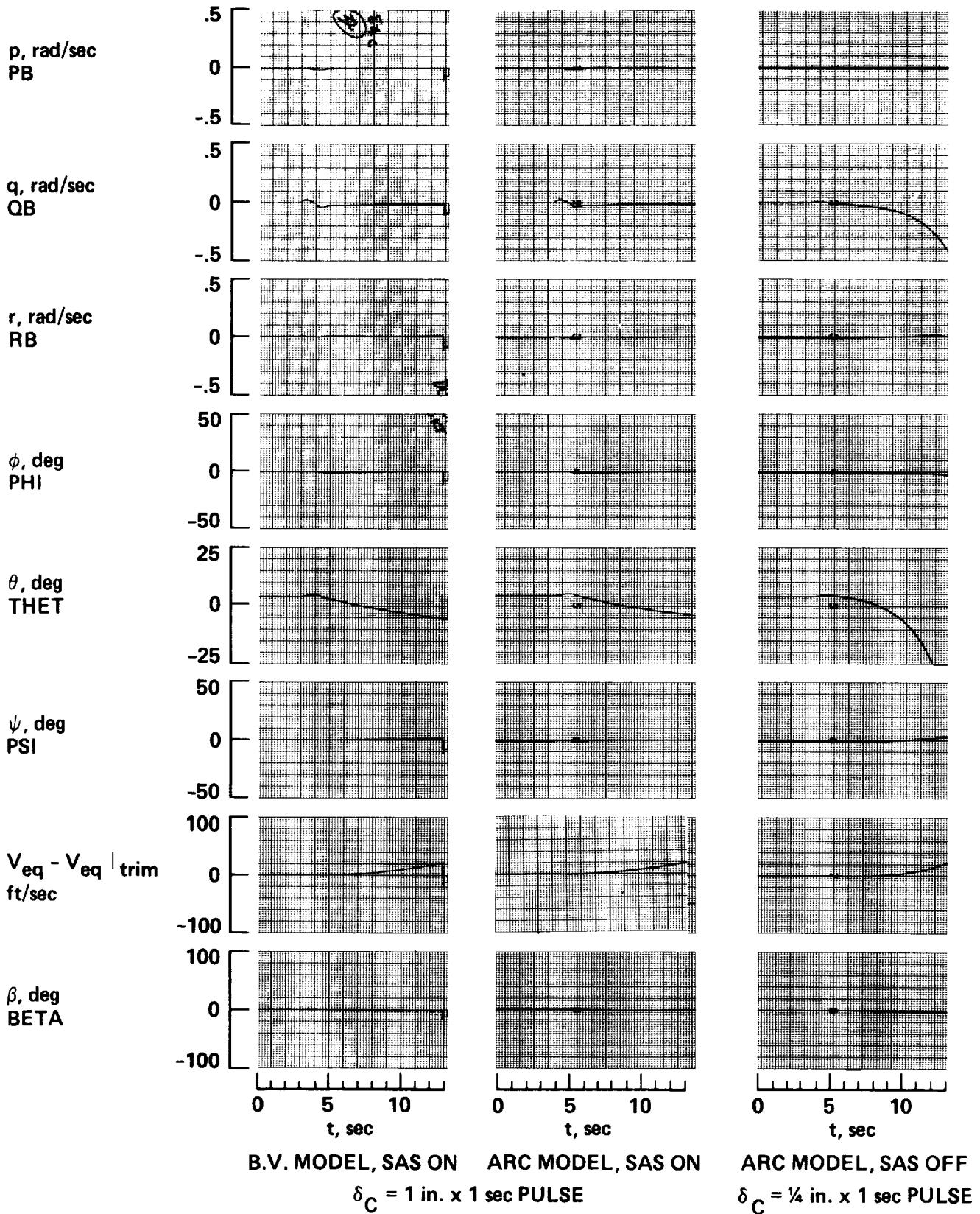


Figure 30.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

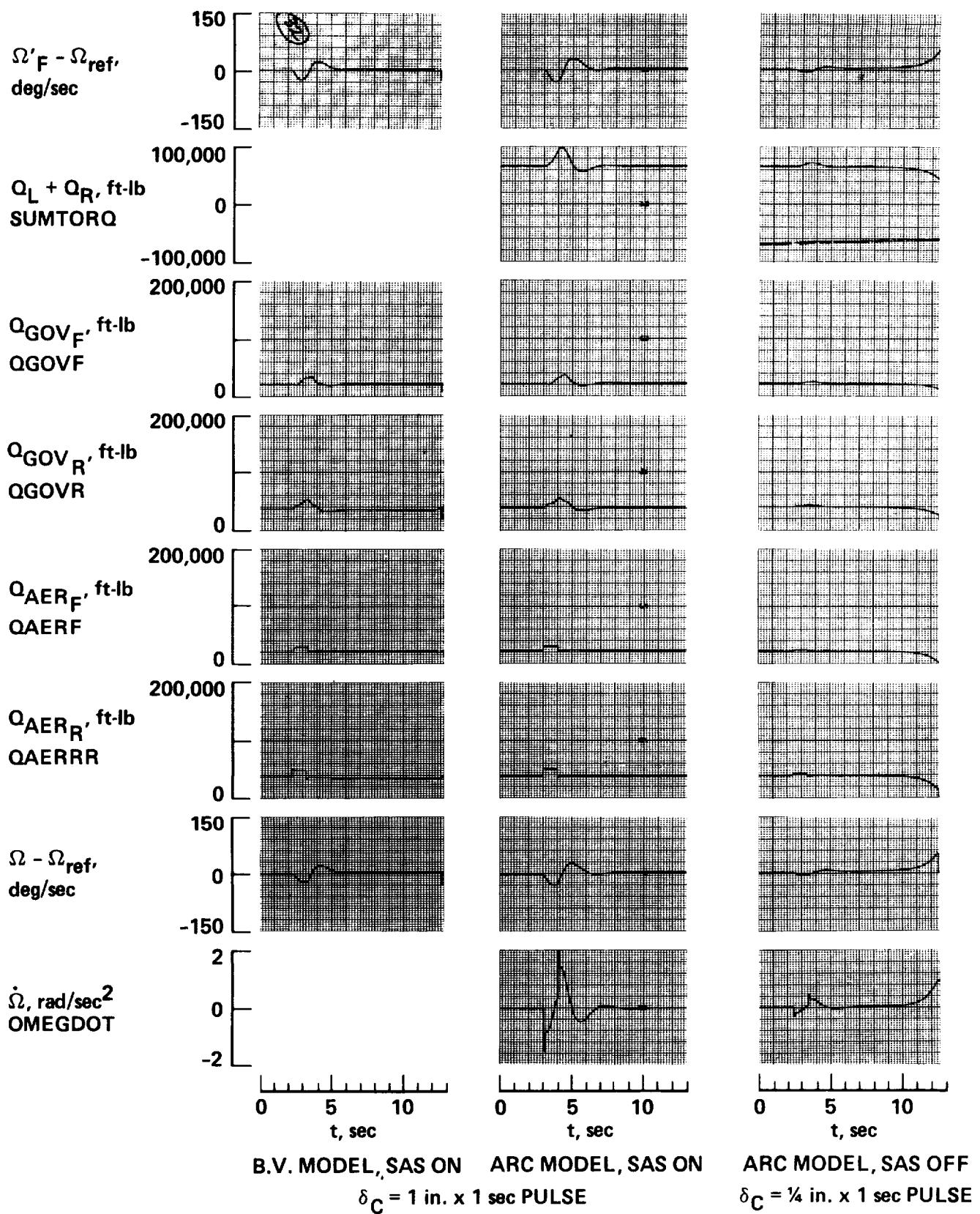


Figure 31.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

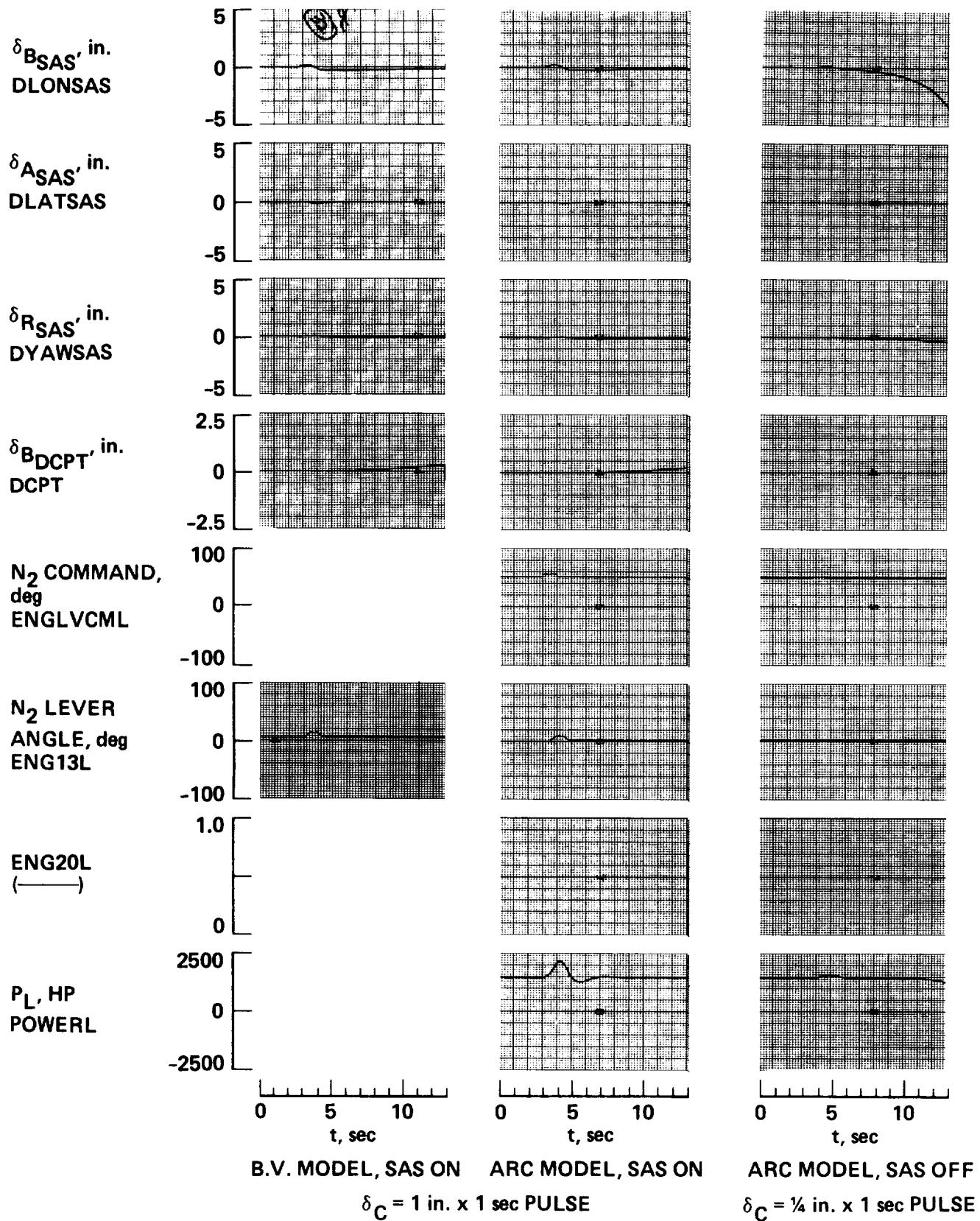


Figure 32.- BV versus ARC simulation response data; $V_{eq} = 40$ knots.

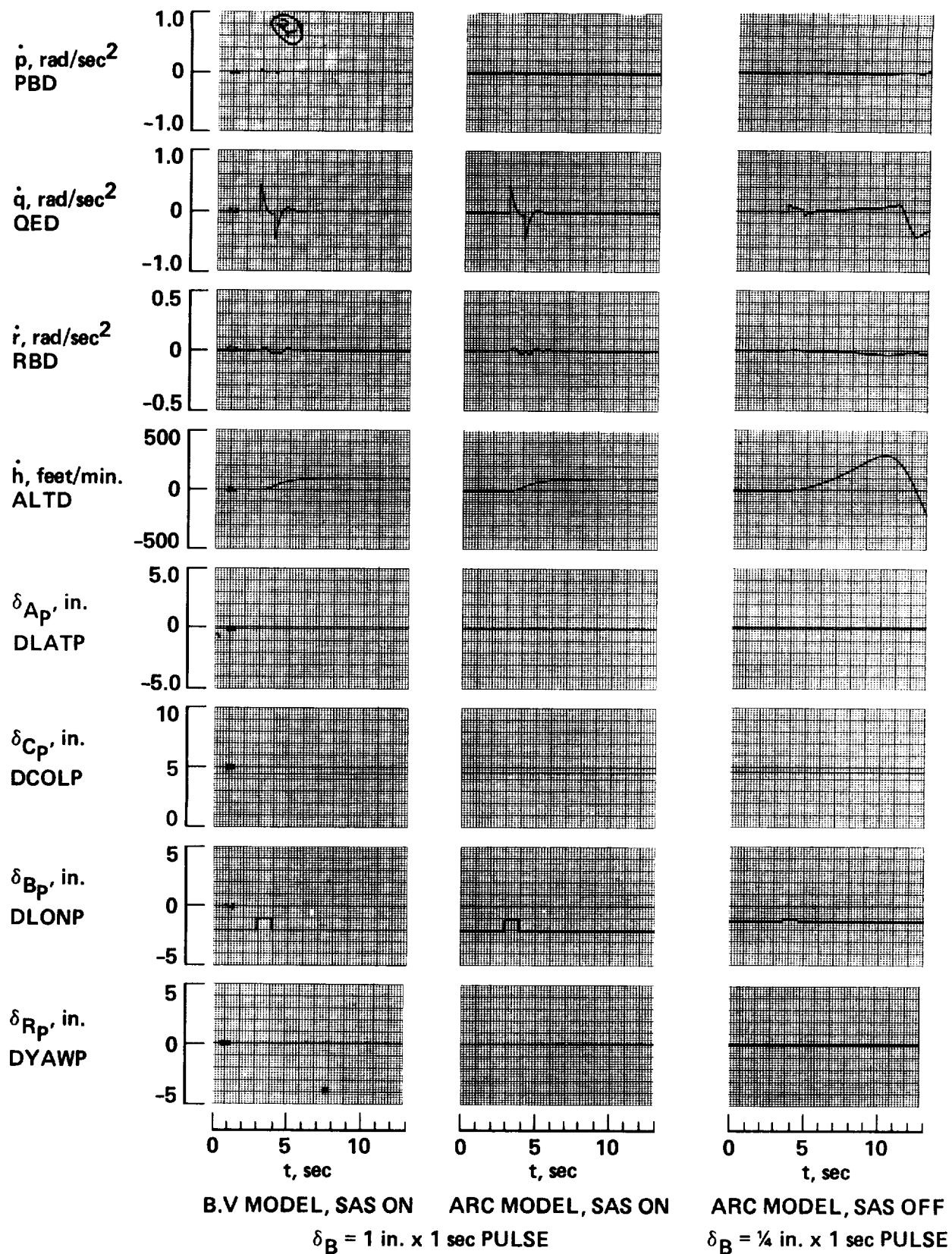


Figure 33.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

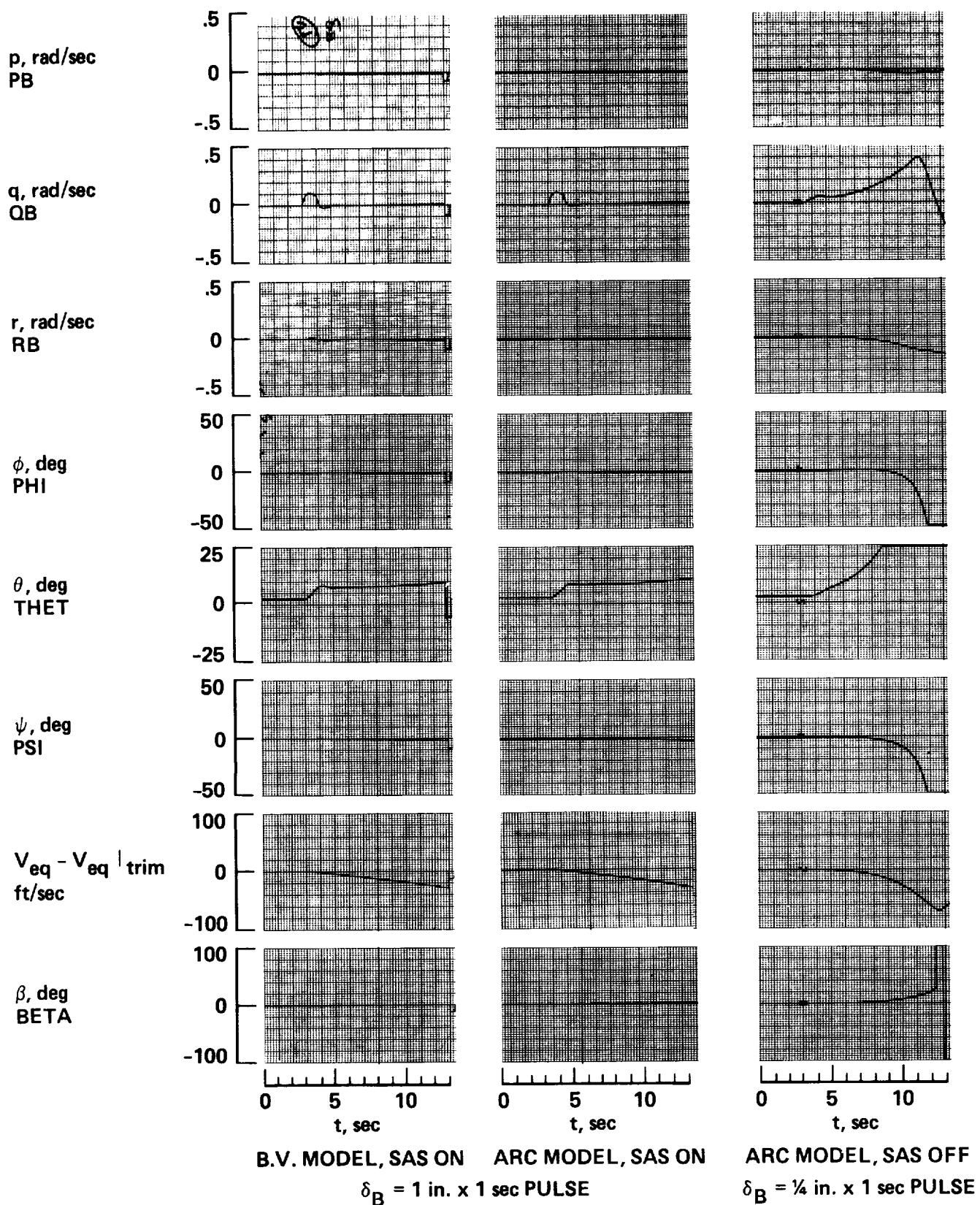


Figure 34.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

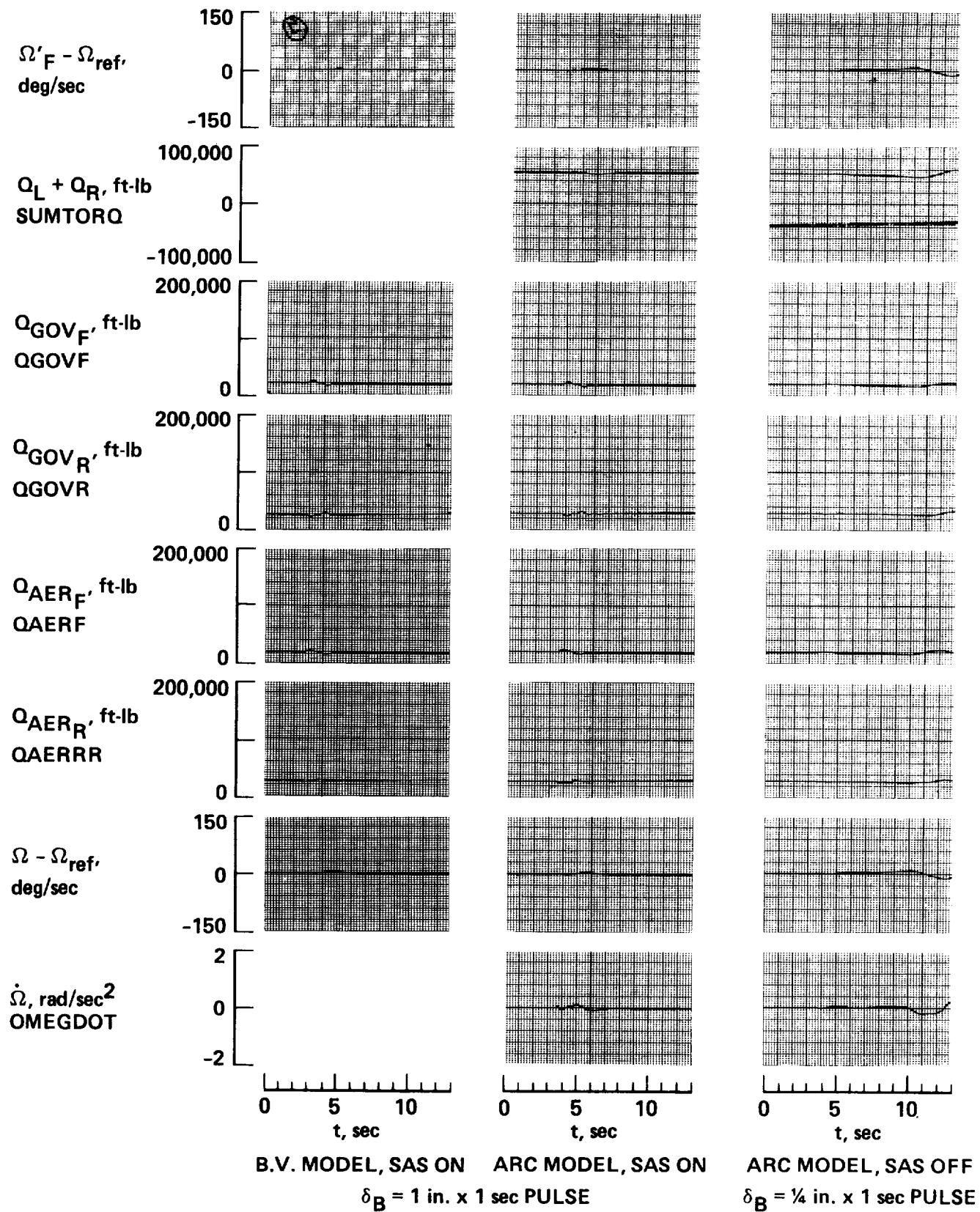


Figure 35.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

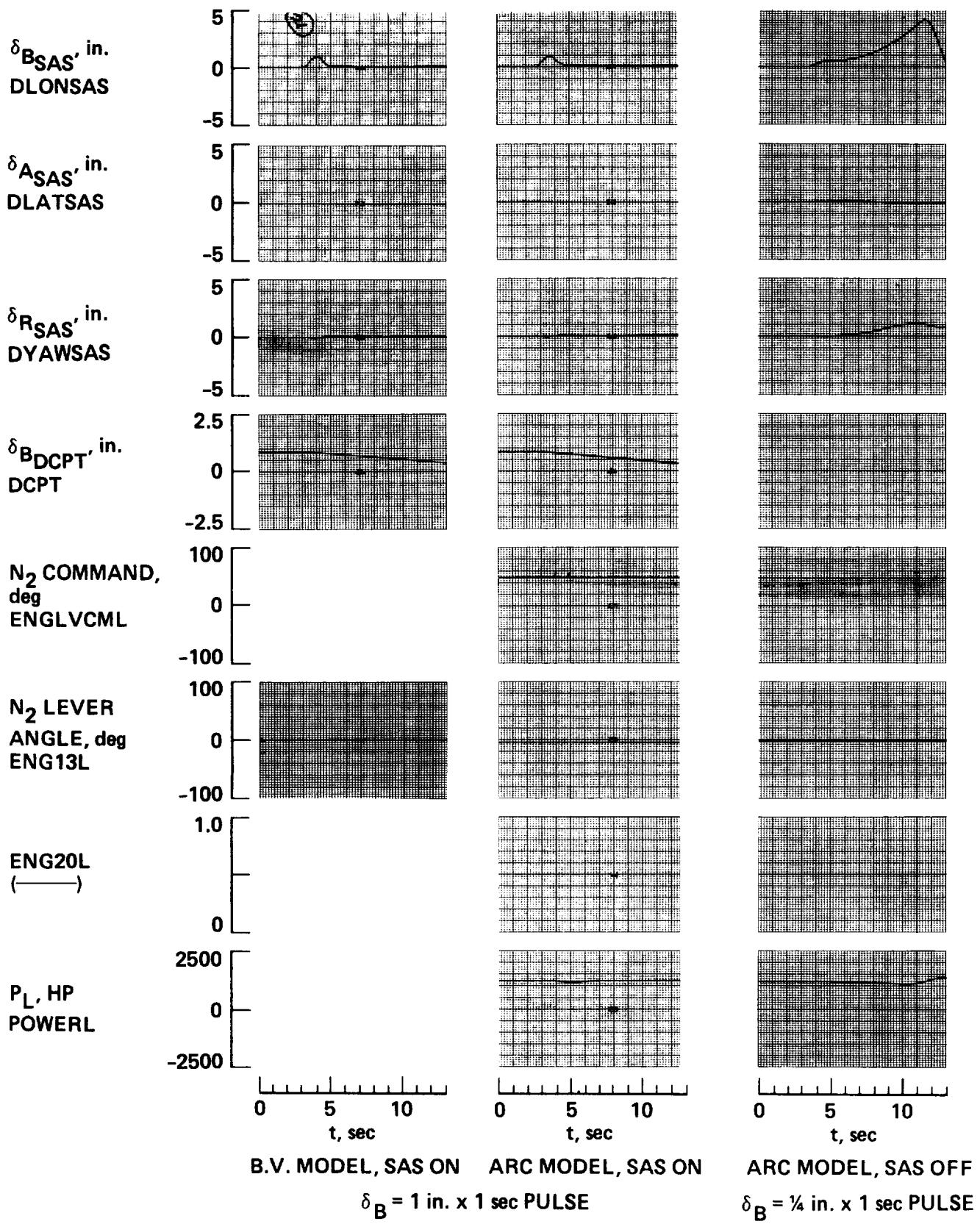


Figure 36.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

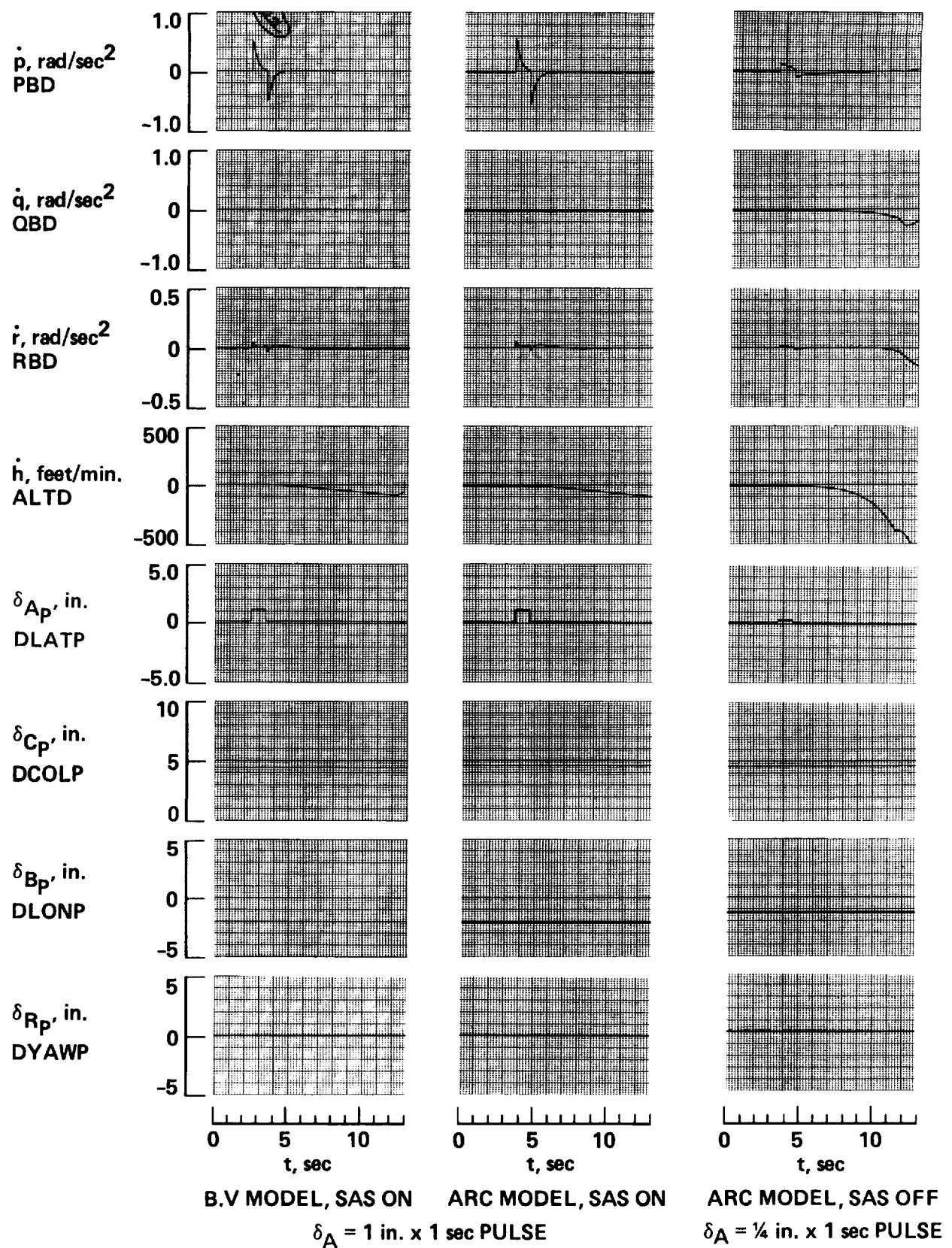


Figure 37.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

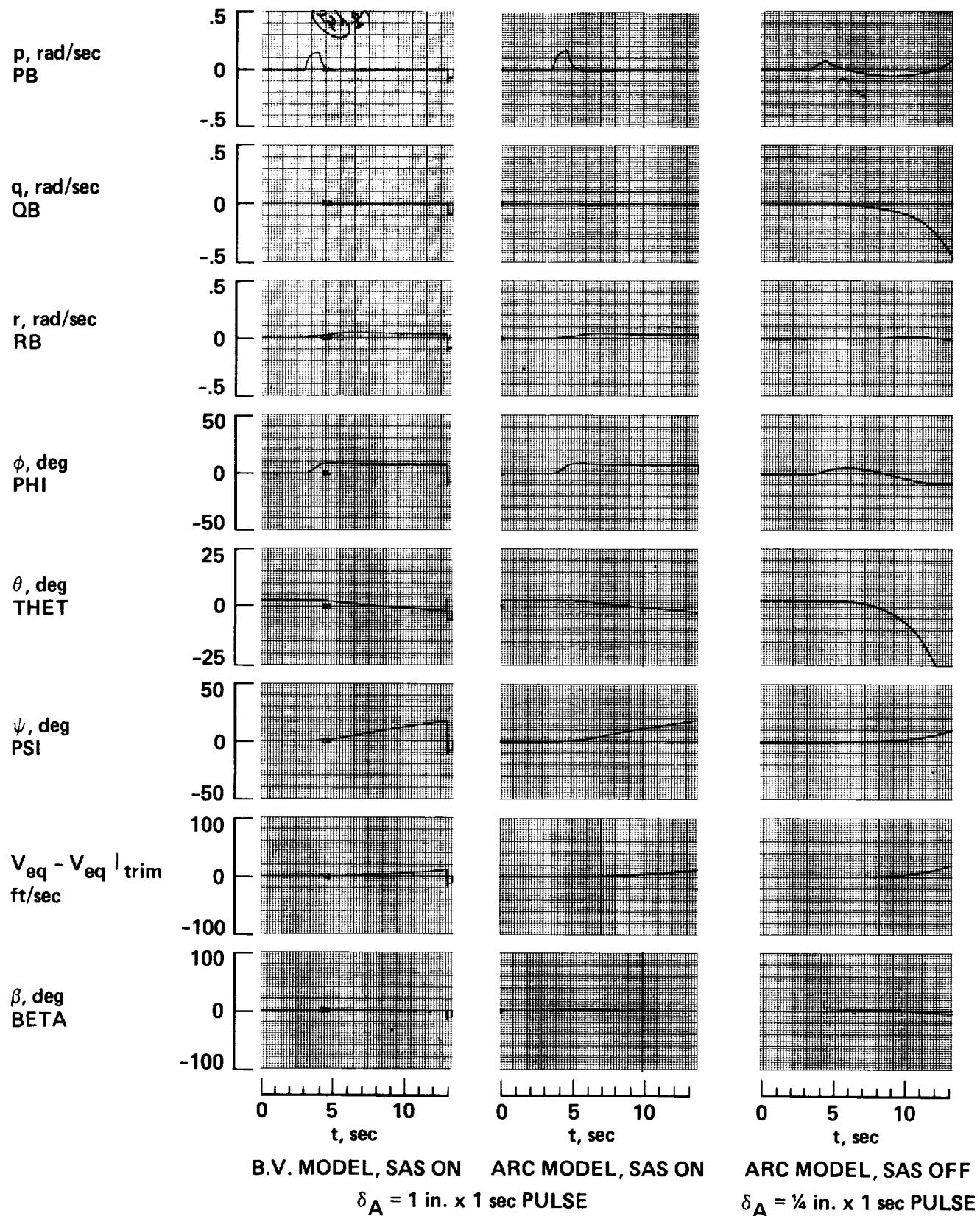


Figure 38.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

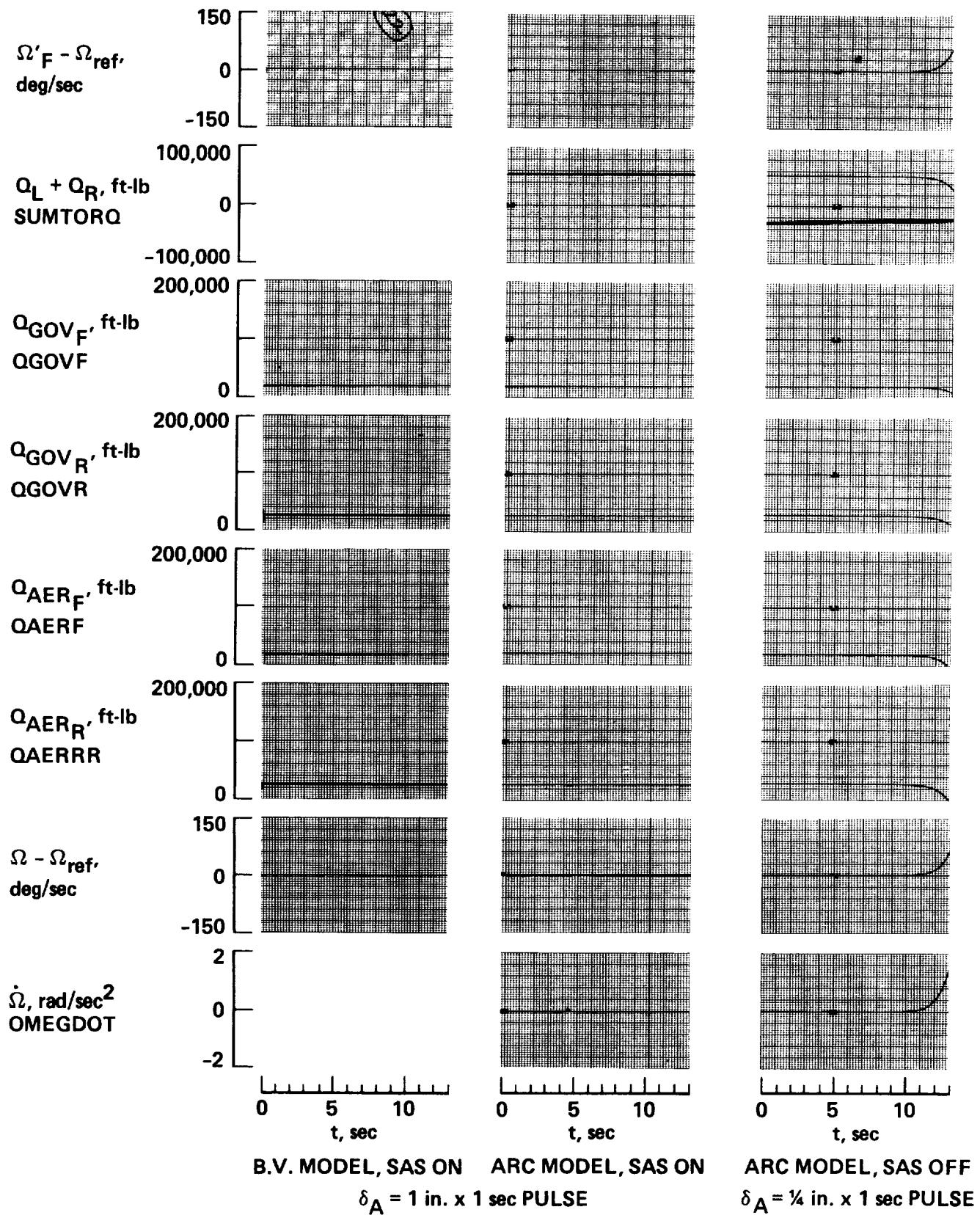


Figure 39.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

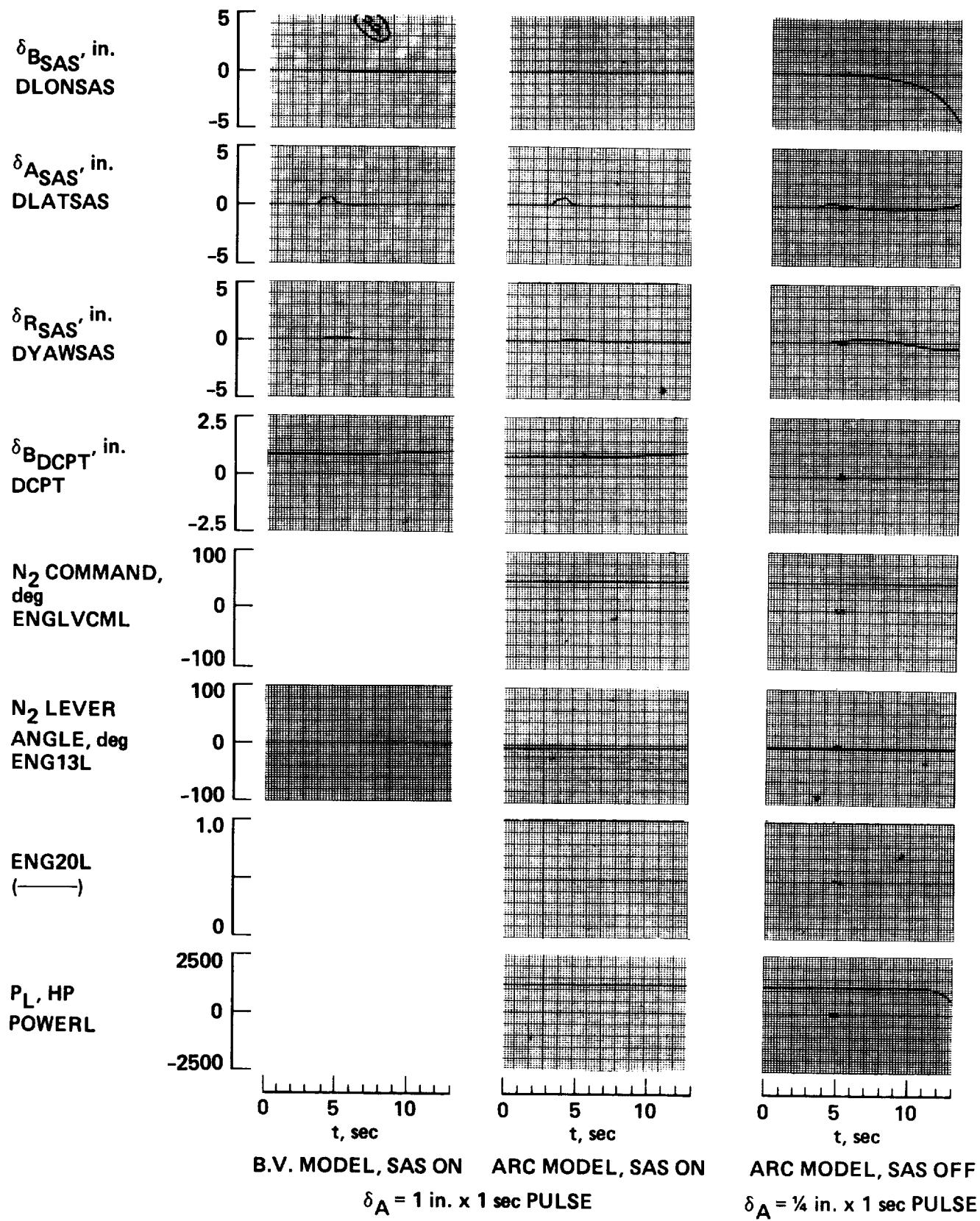


Figure 40.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

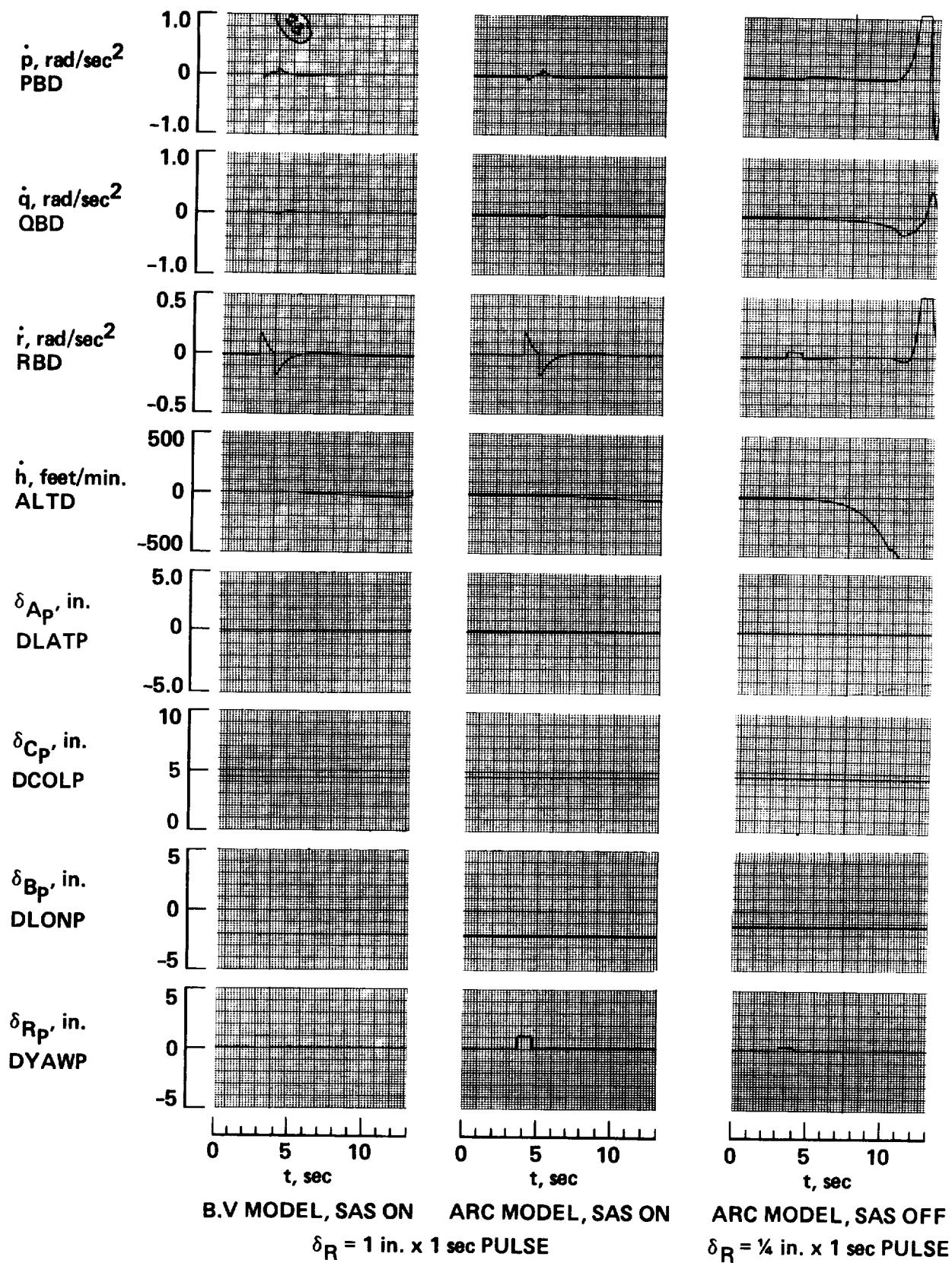


Figure 41.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

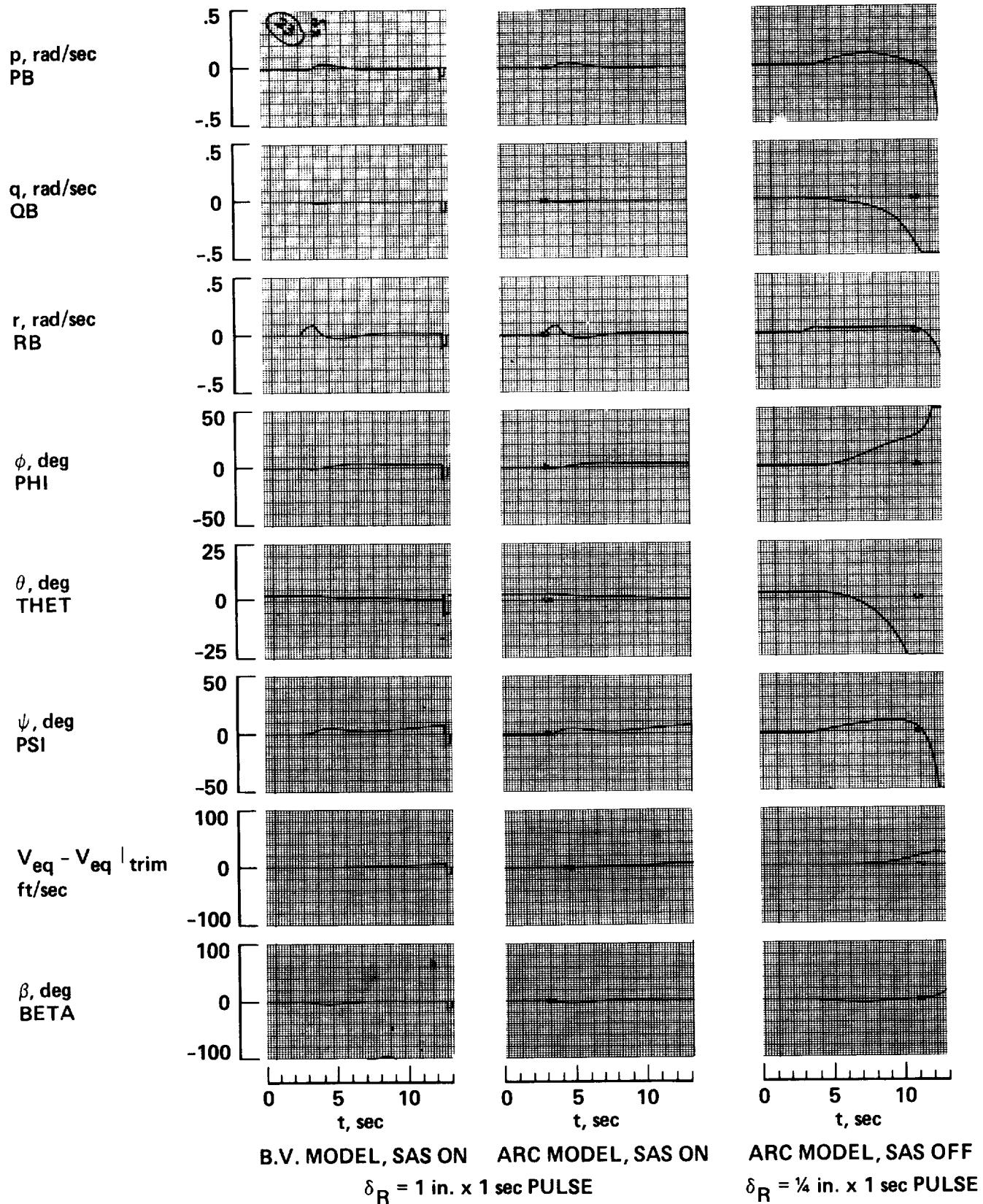


Figure 42.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

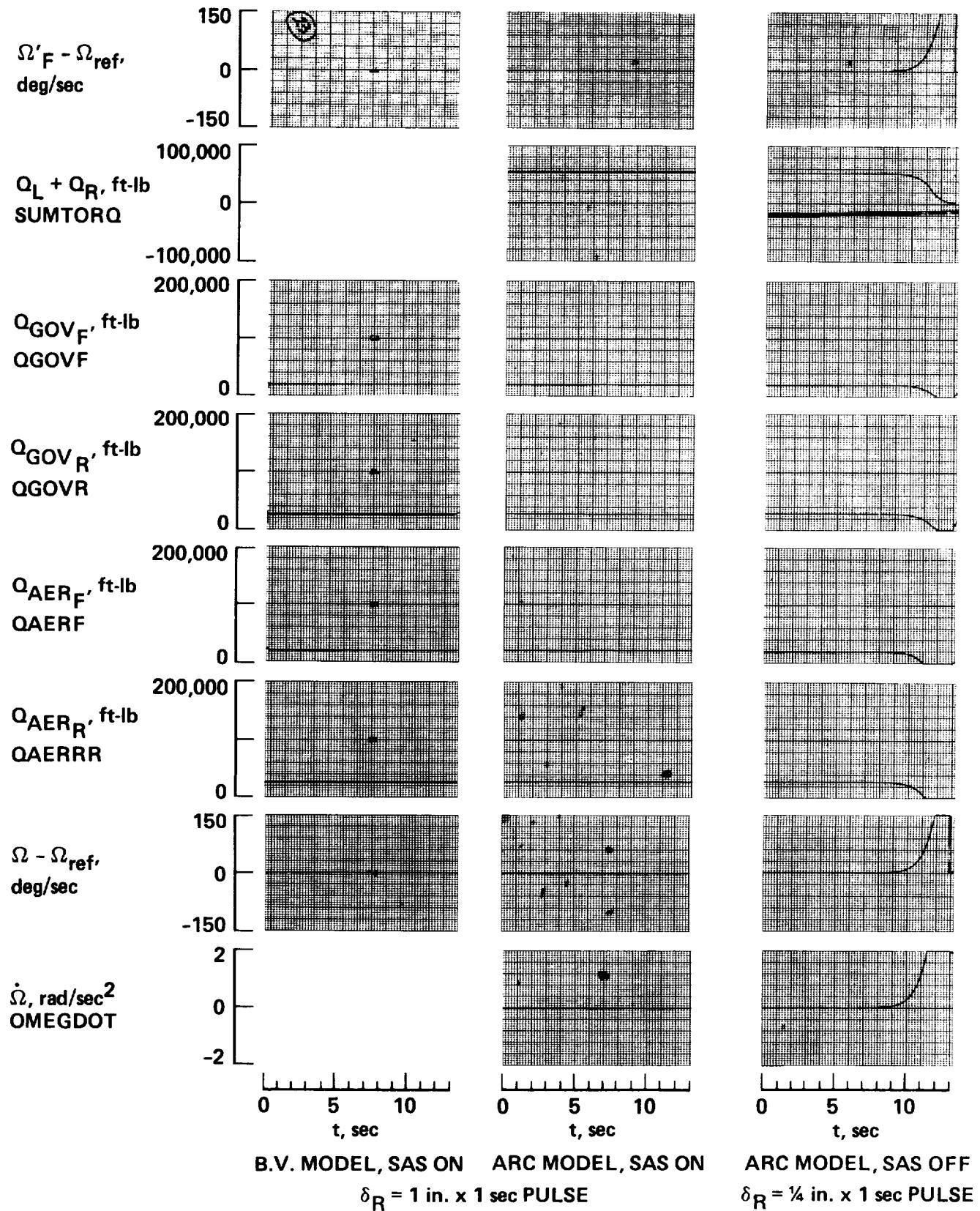


Figure 43.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

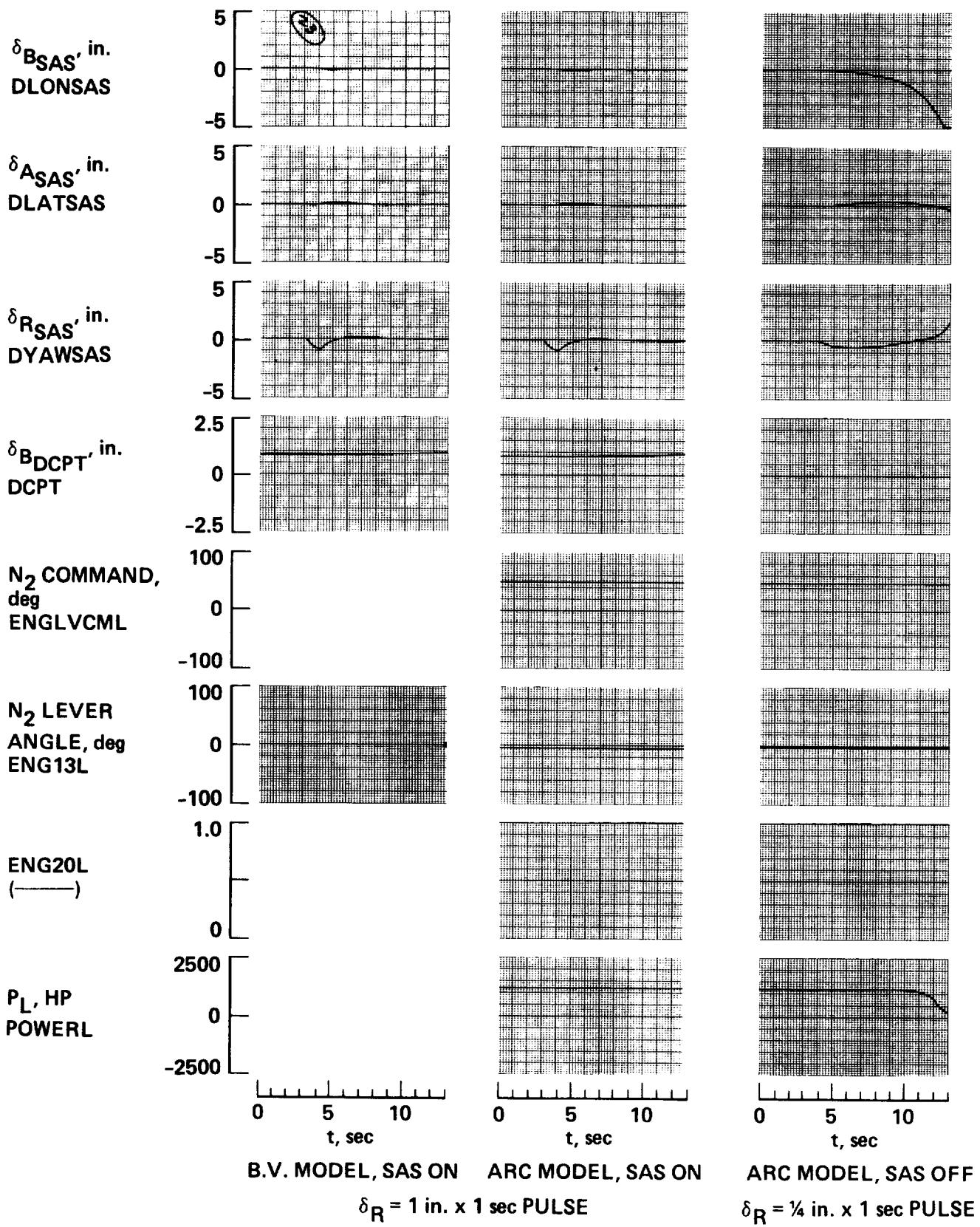


Figure 44.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

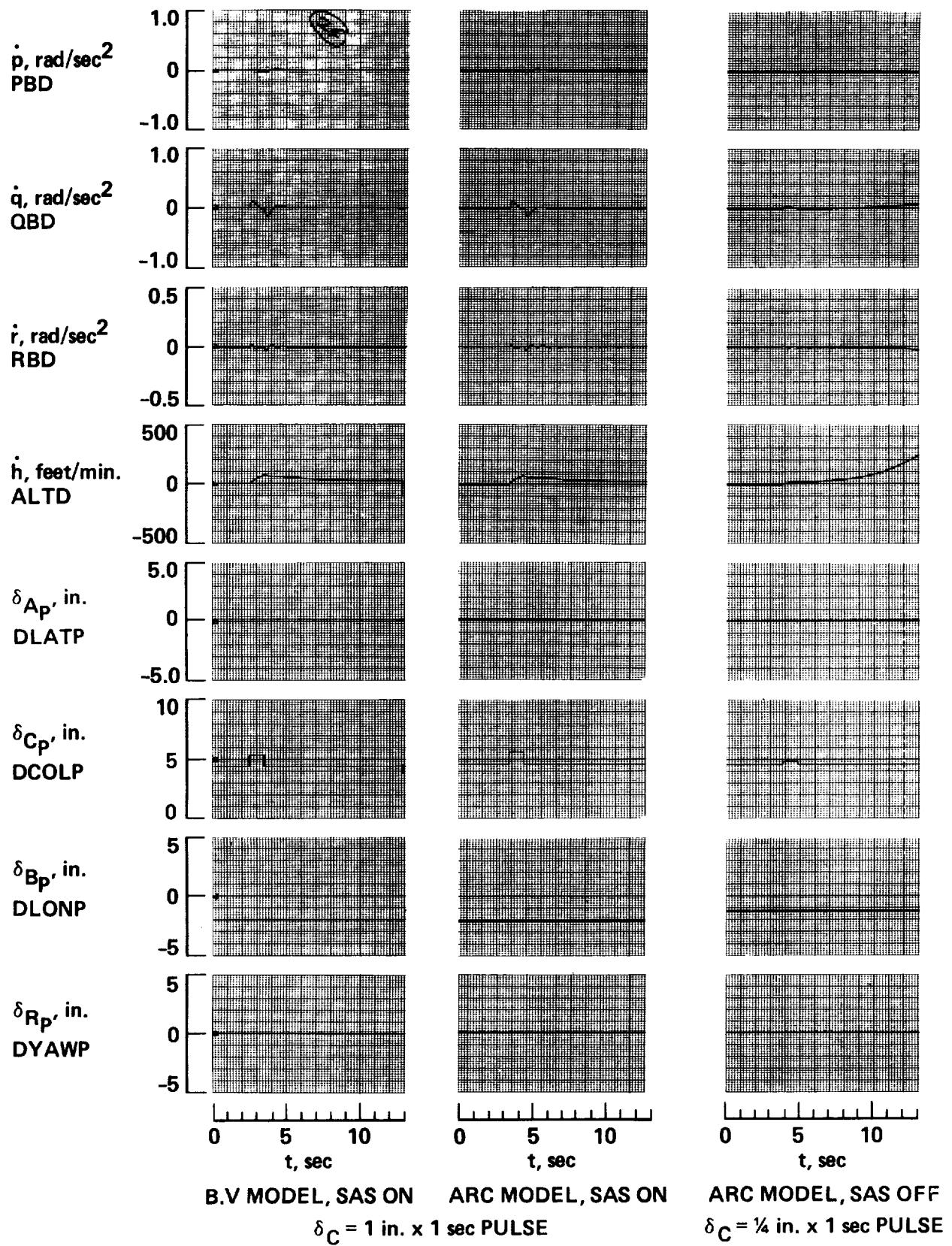


Figure 45.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

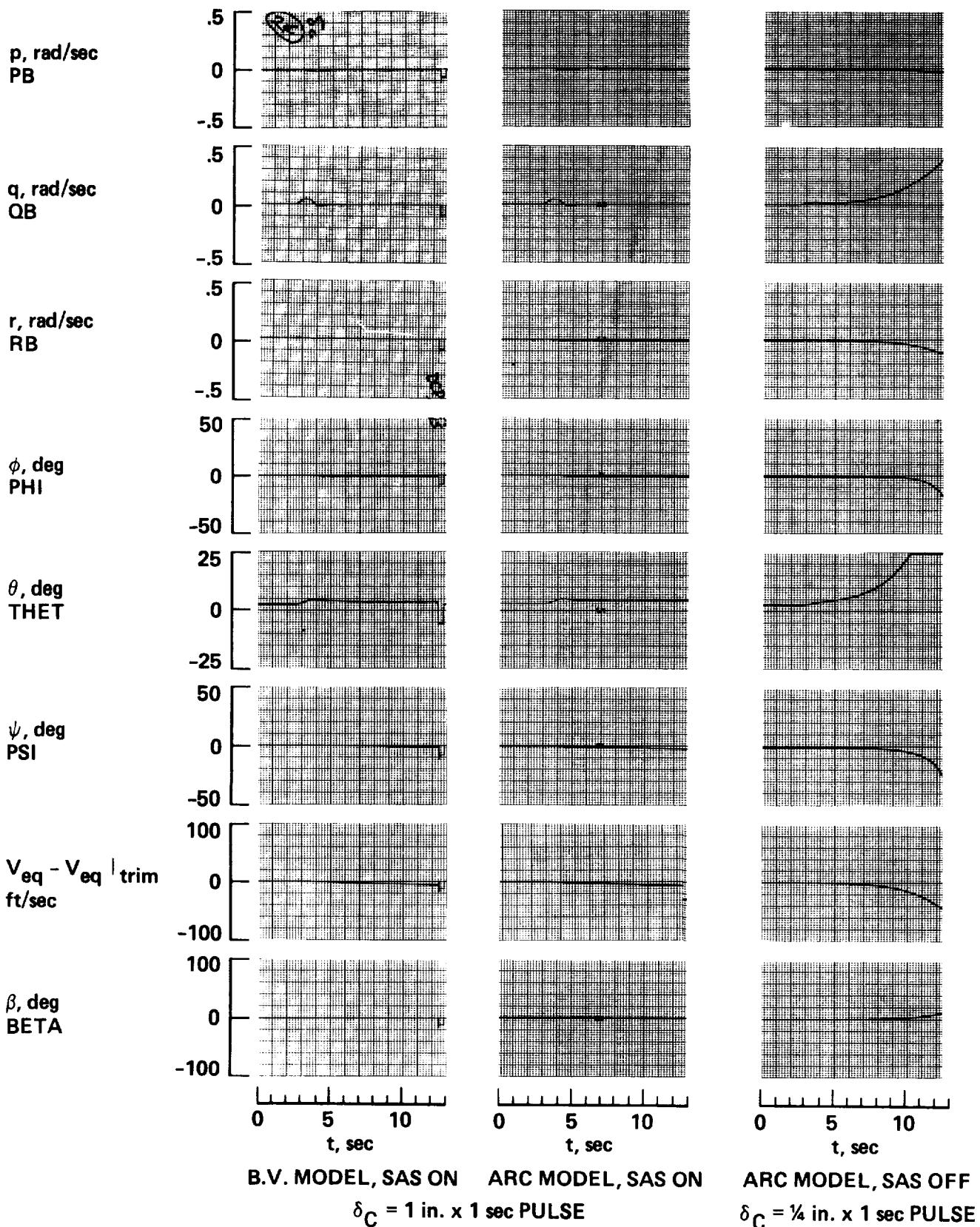


Figure 46.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

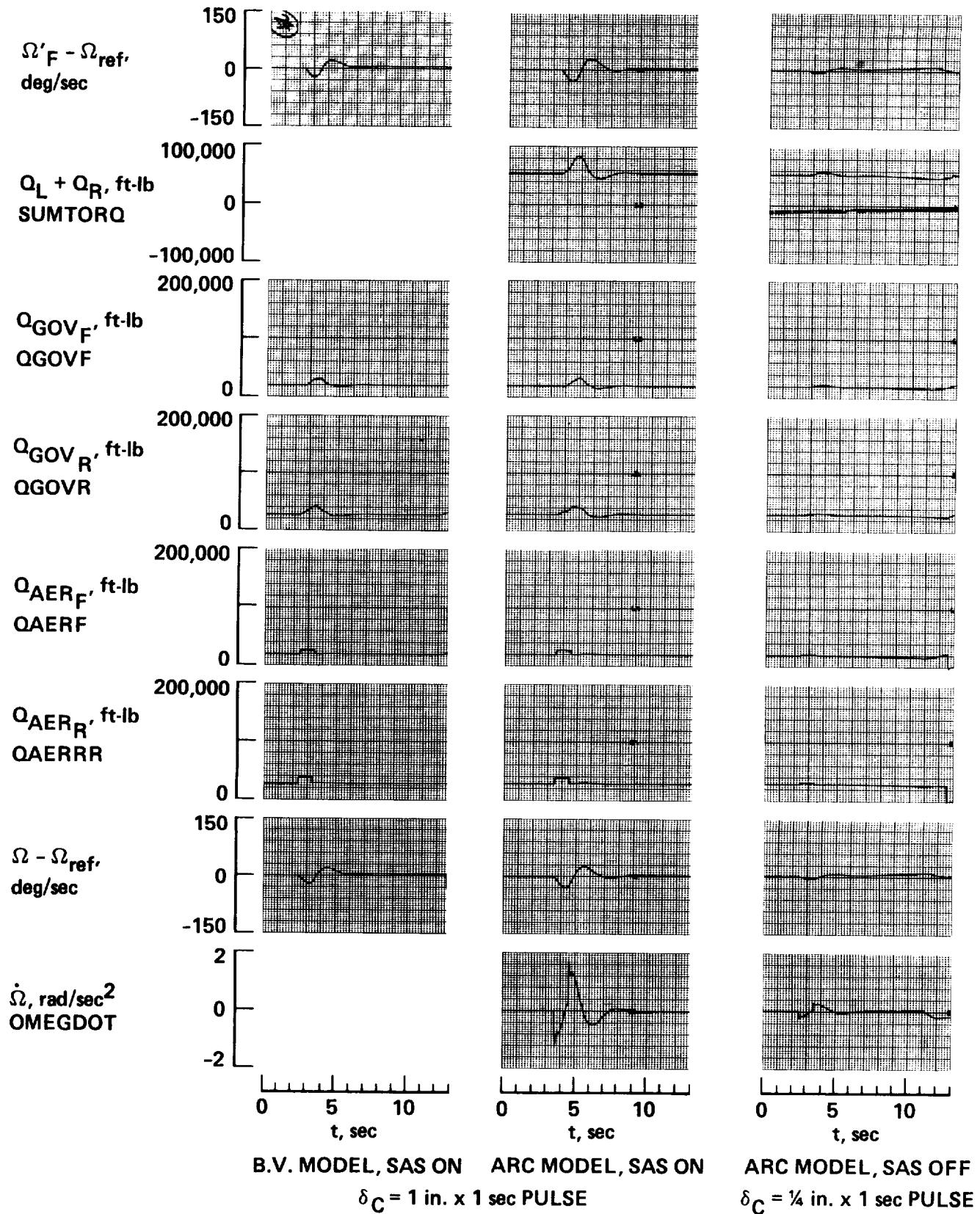


Figure 47.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

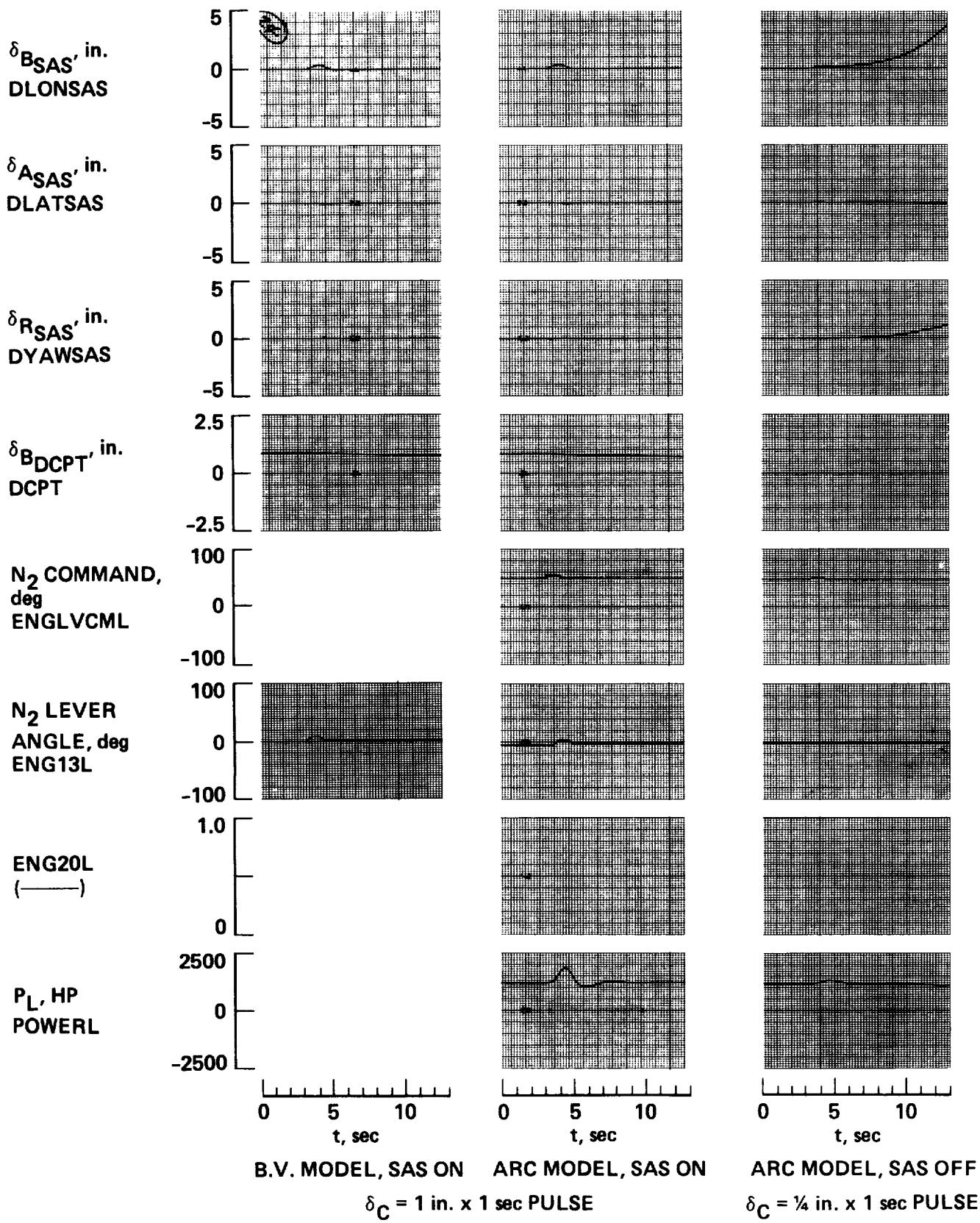


Figure 48.- BV versus ARC simulation response data; $V_{eq} = 75$ knots.

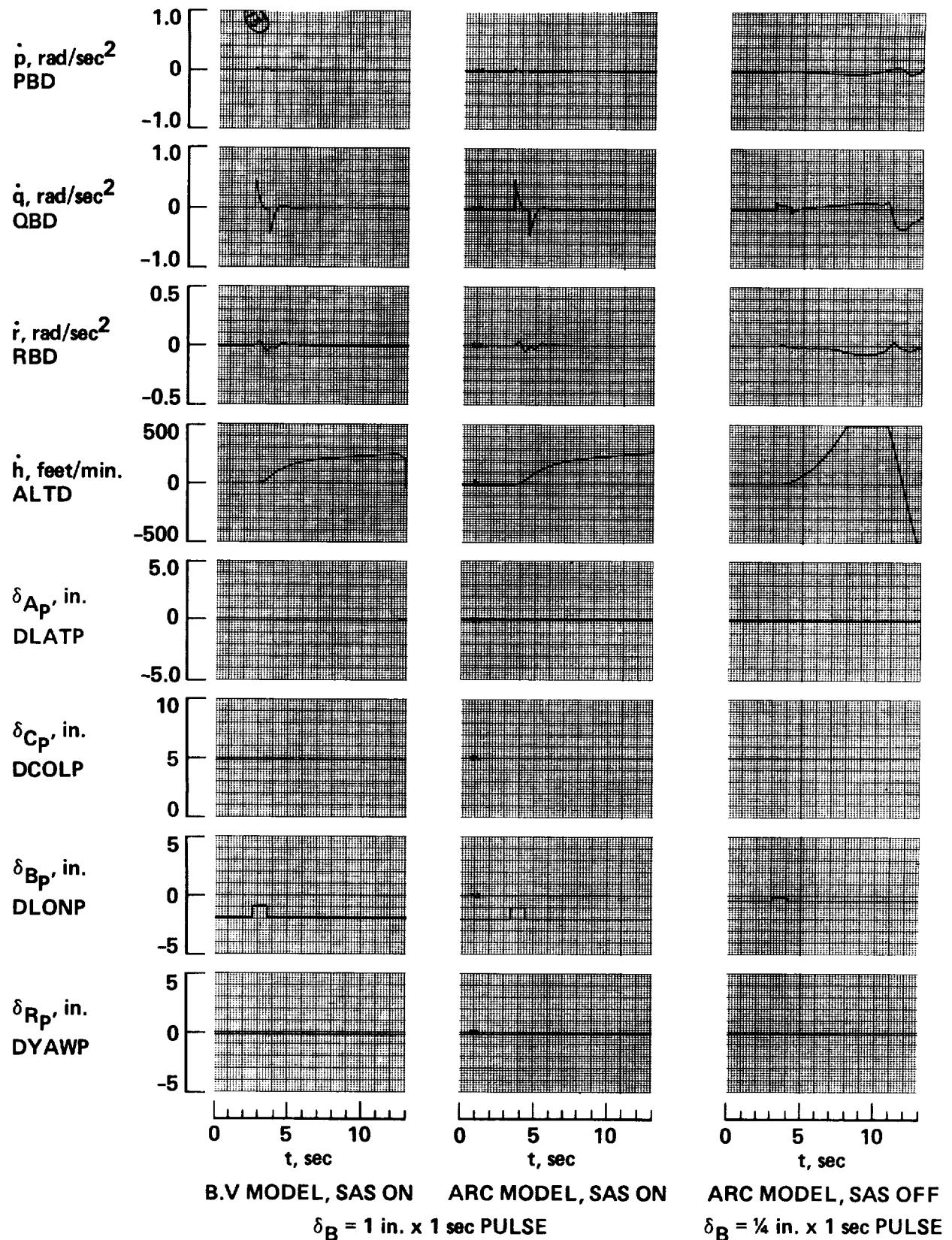


Figure 49.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

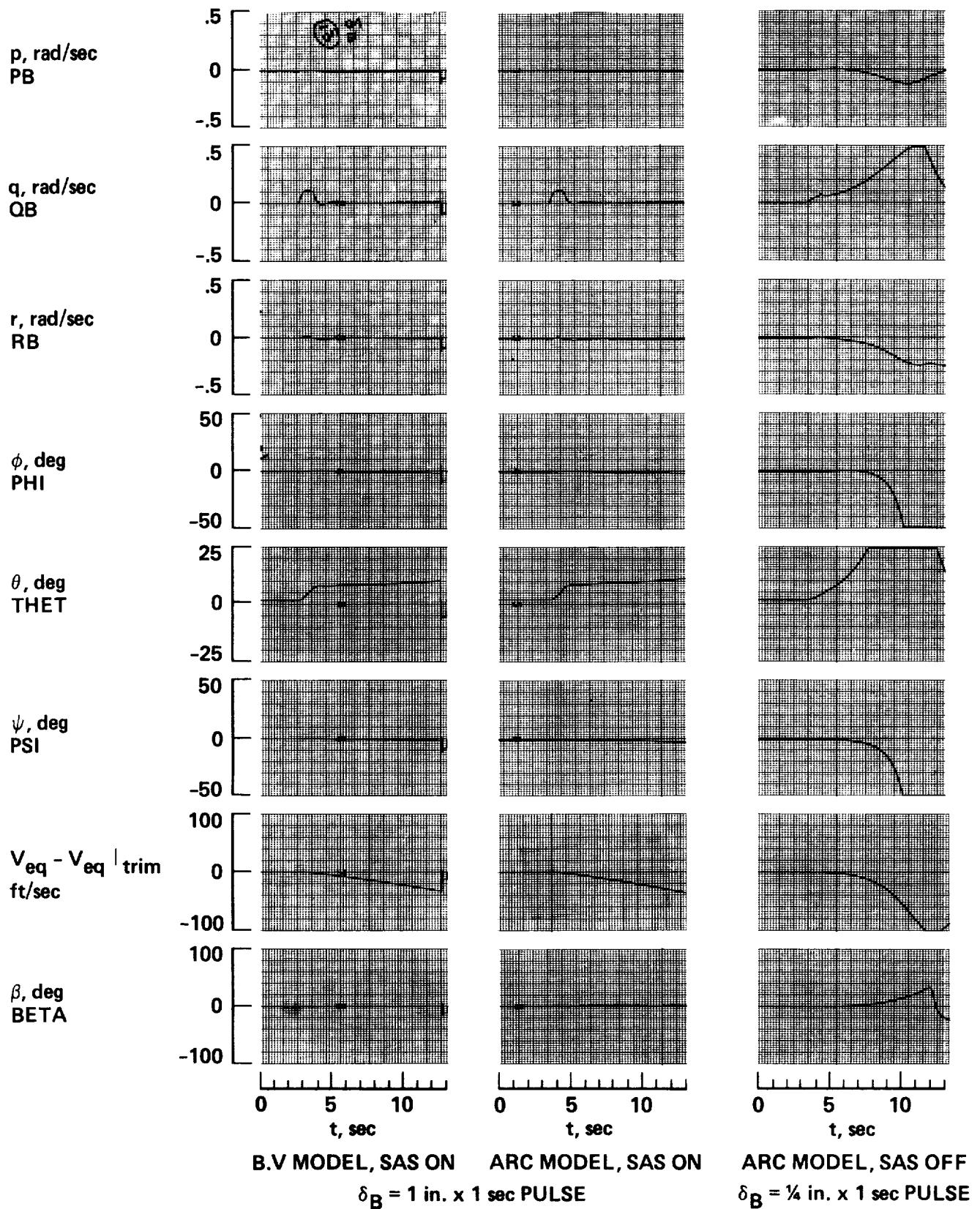


Figure 50.- BV versus ARC simulation response data; $V_{\text{eq}} = 115$ knots.

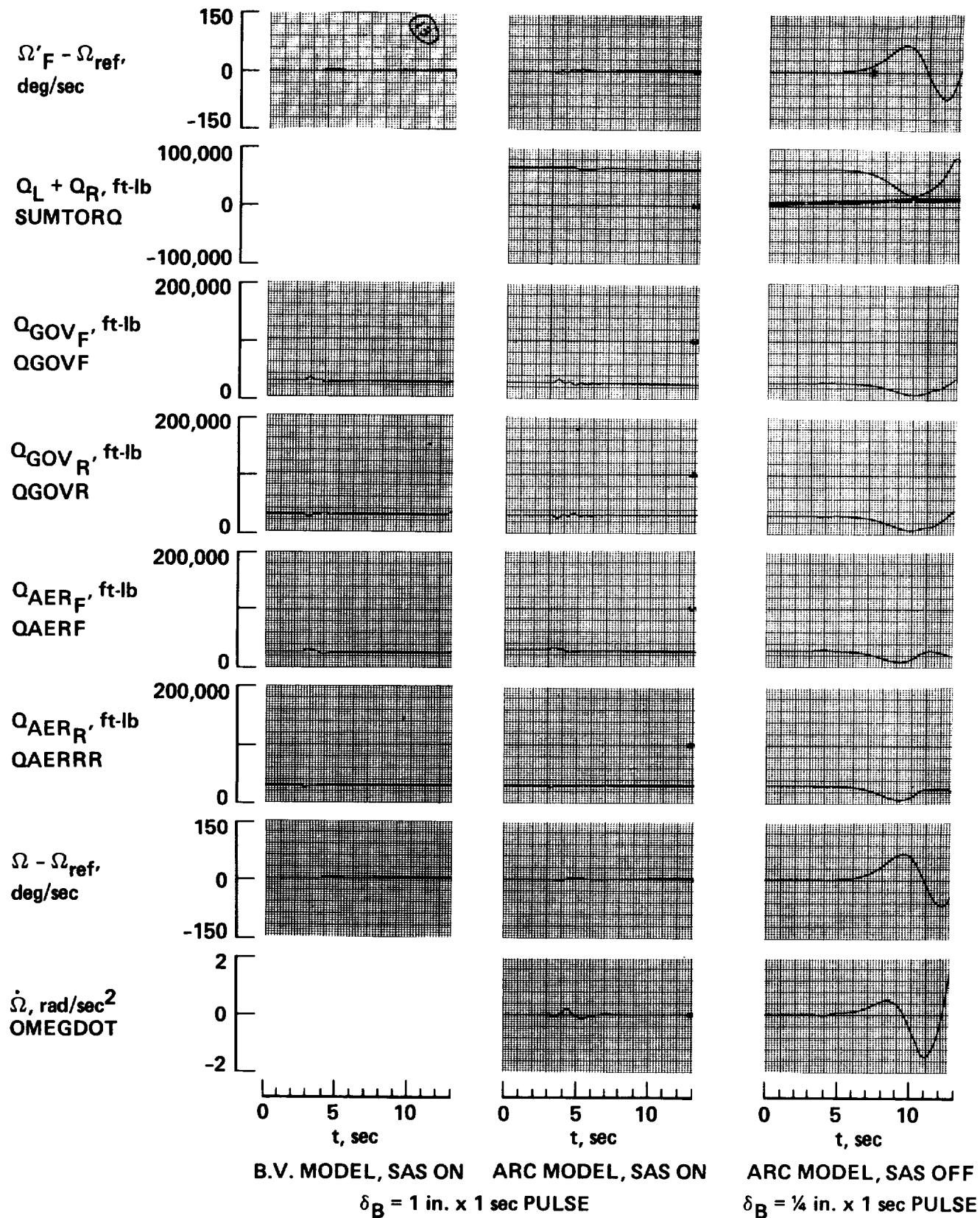


Figure 51.- BV versus ARC simulation response data; $V_{\text{eq}} = 115$ knots.

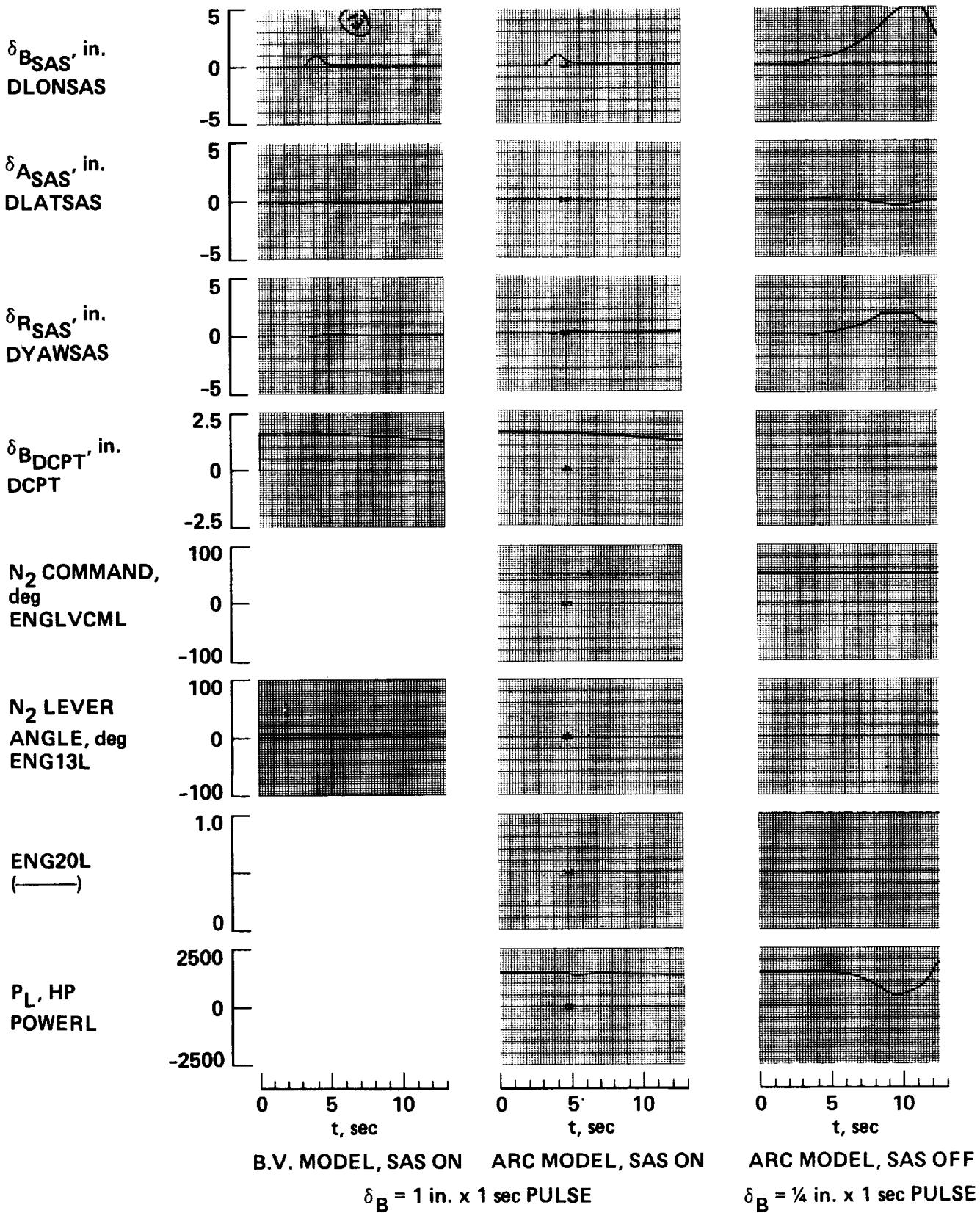


Figure 52.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

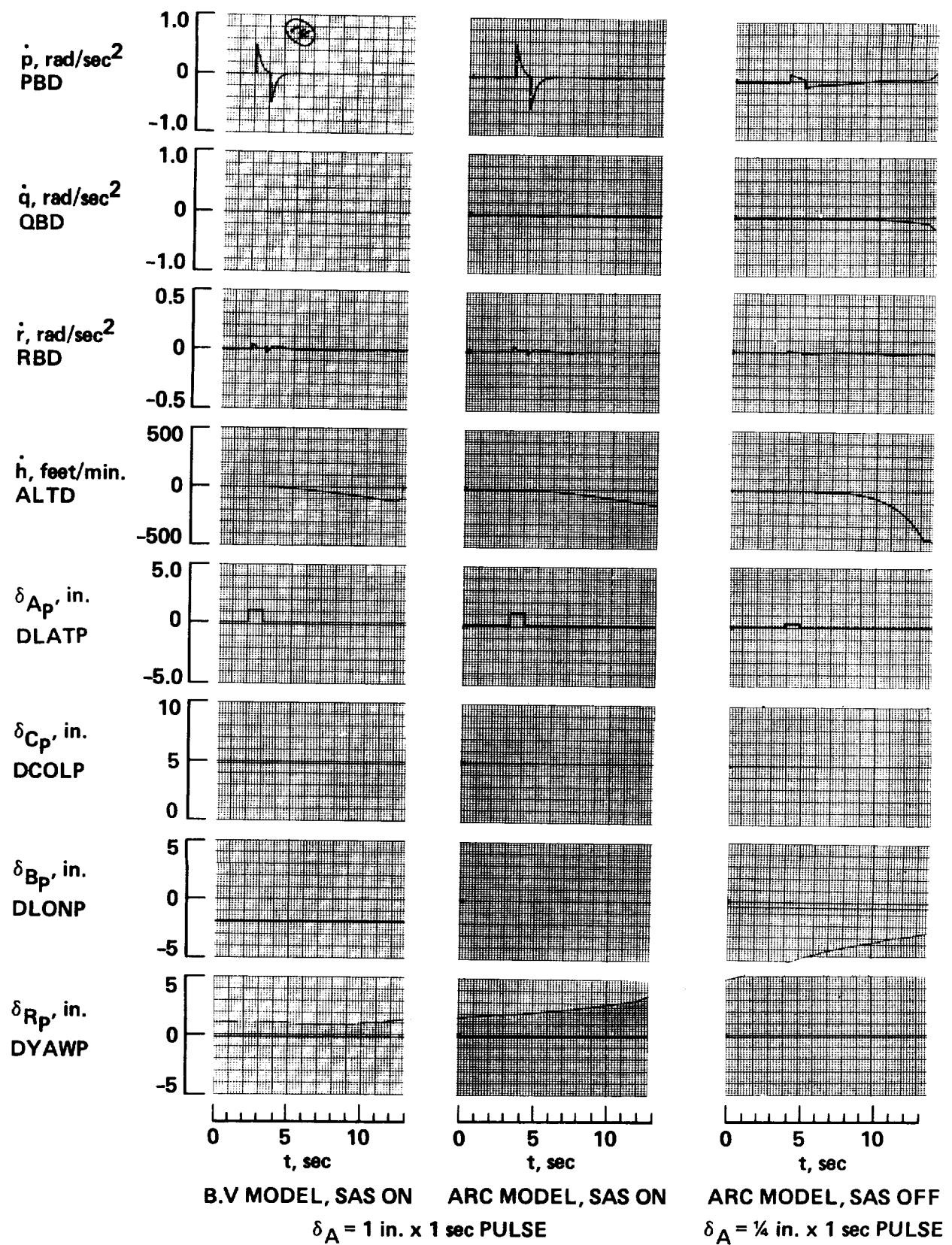


Figure 53.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

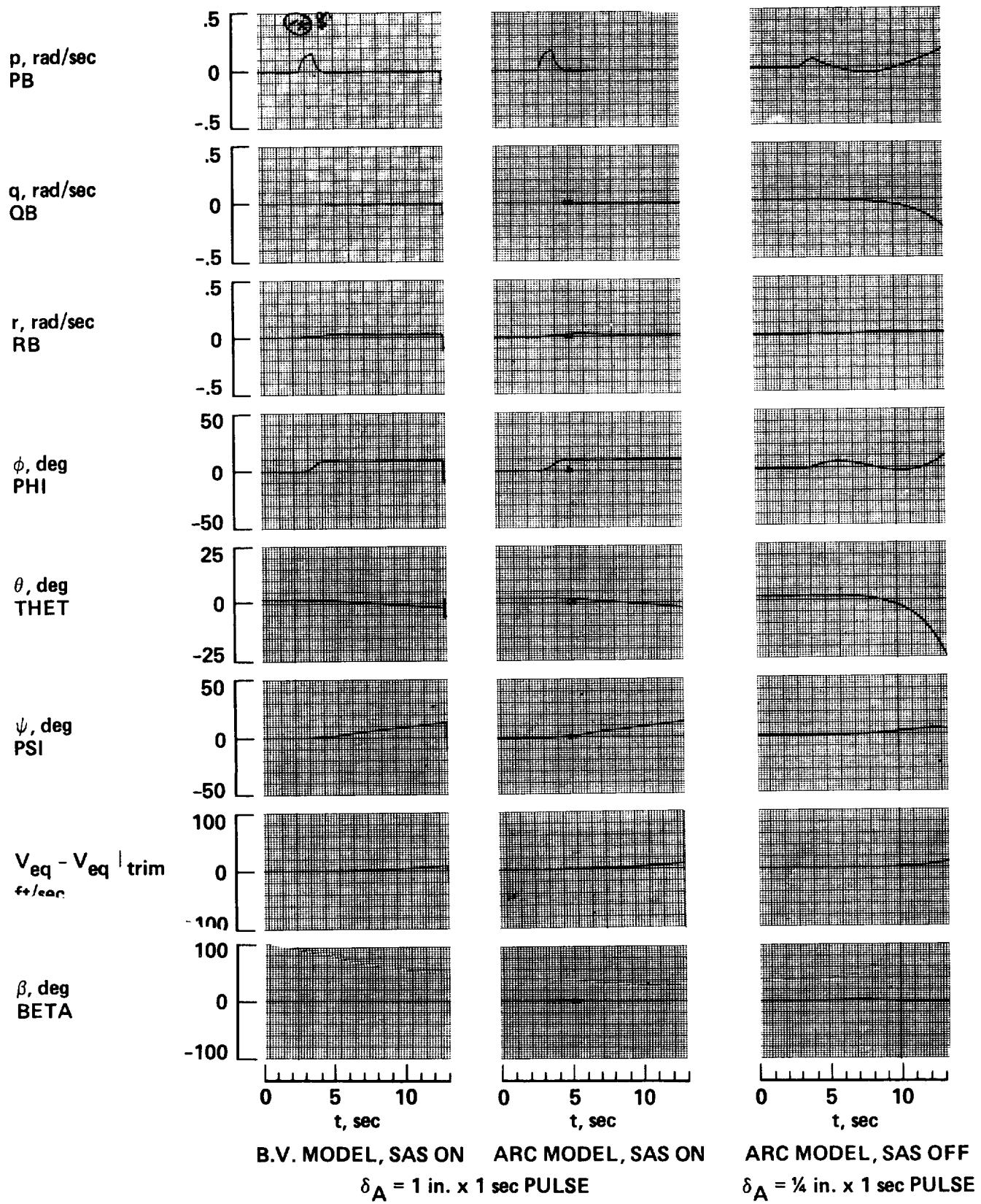


Figure 54.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

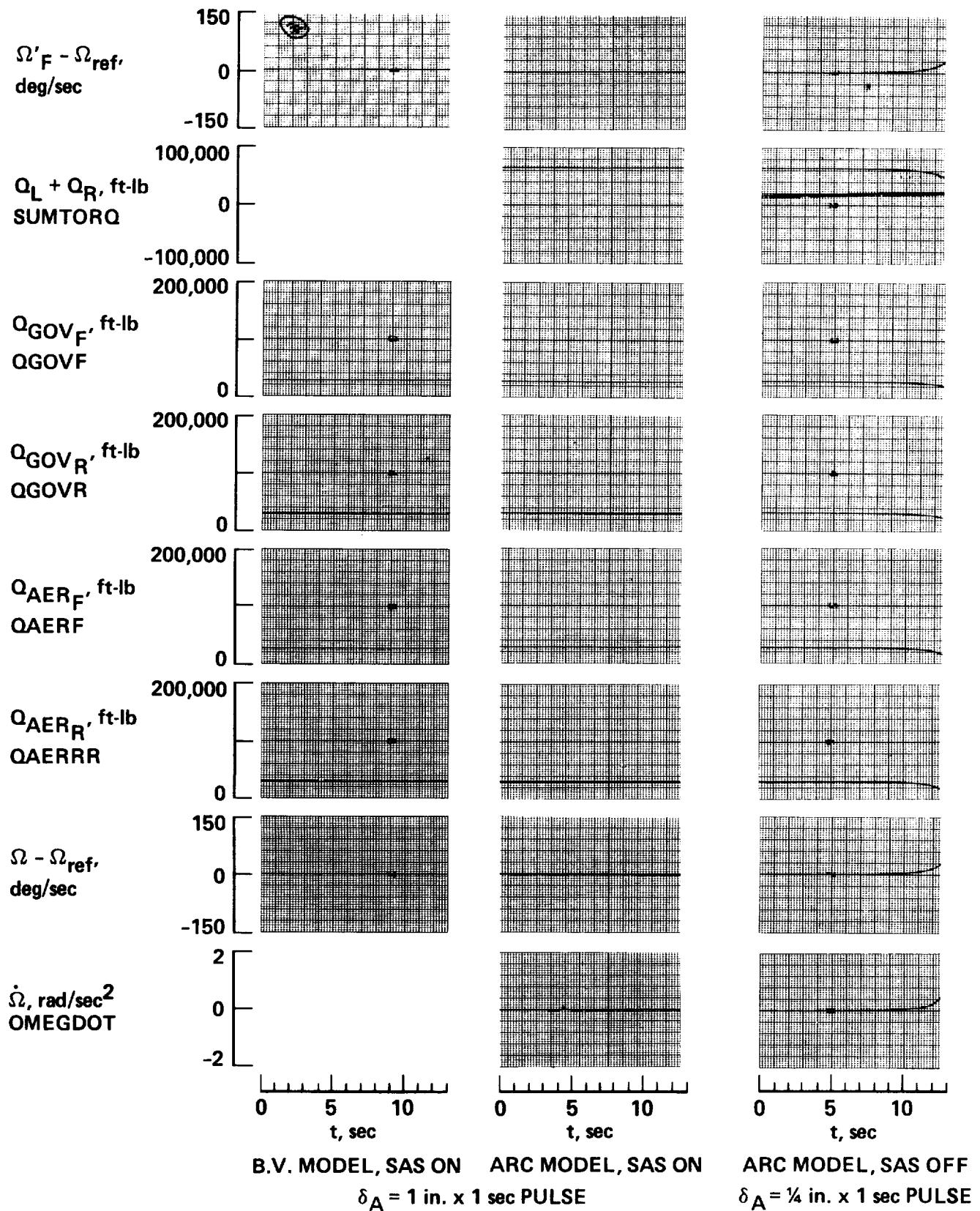


Figure 55. - BV versus ARC simulation response data; $V_{eq} = 115$ knots.

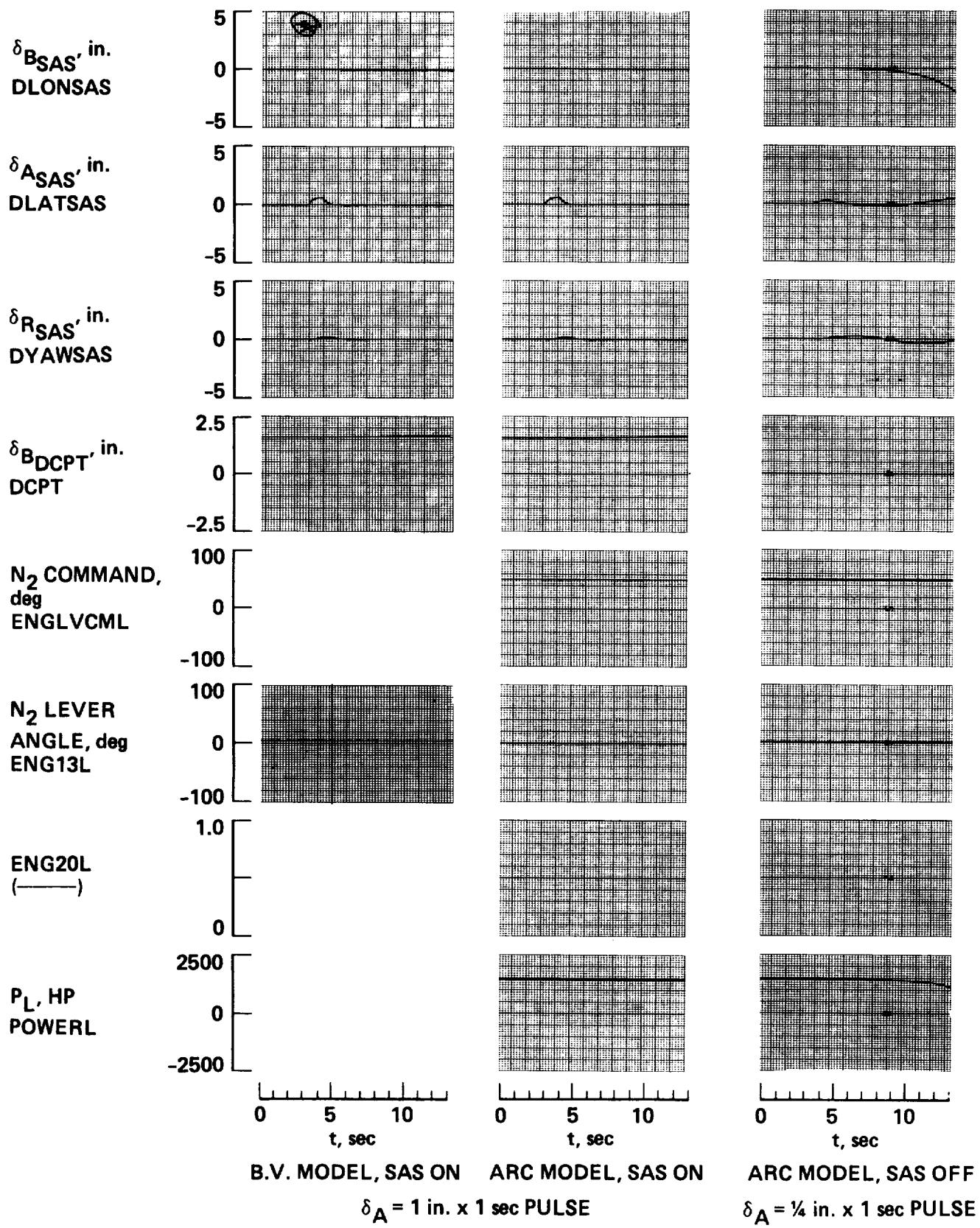


Figure 56.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

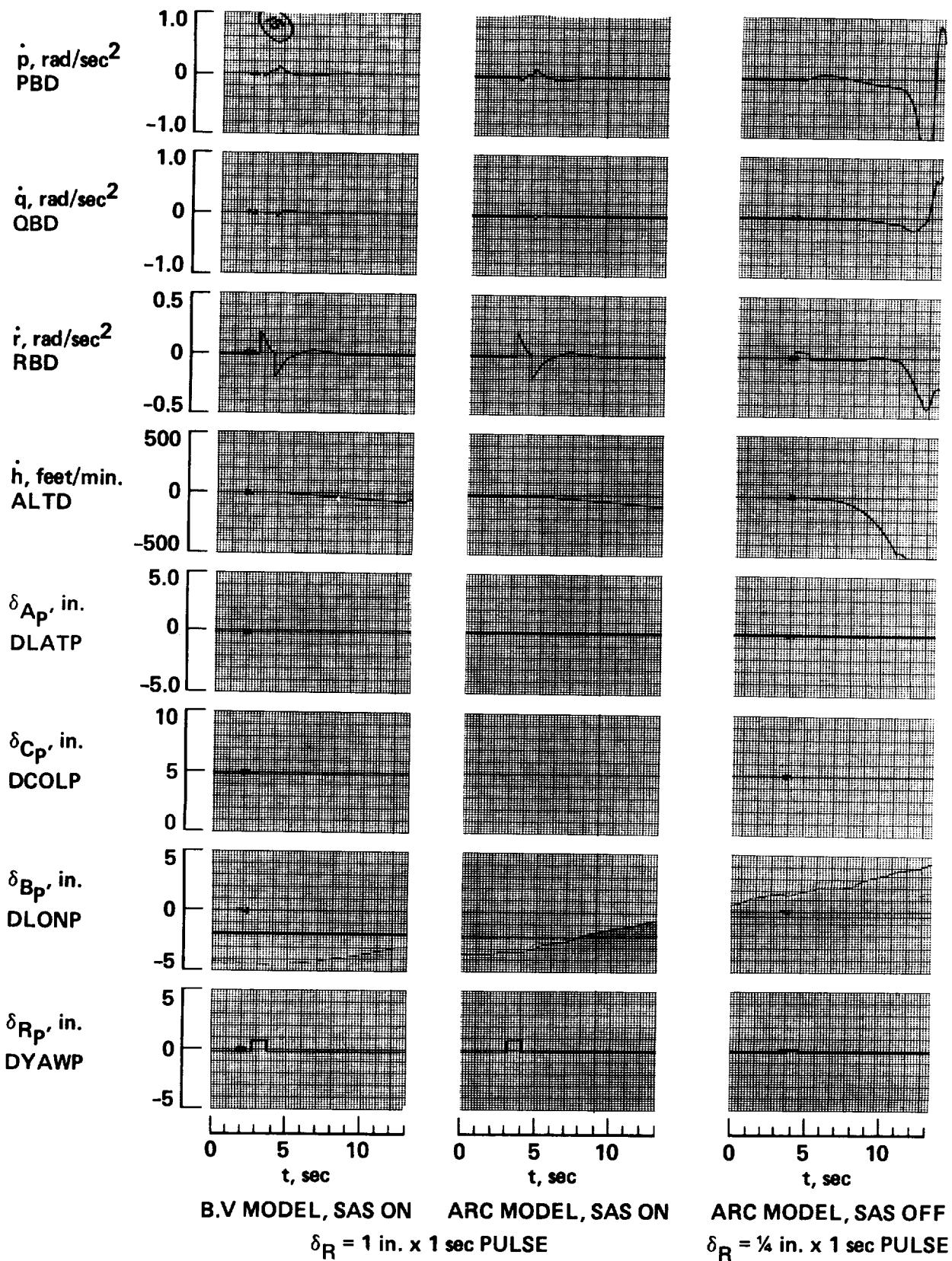


Figure 57.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

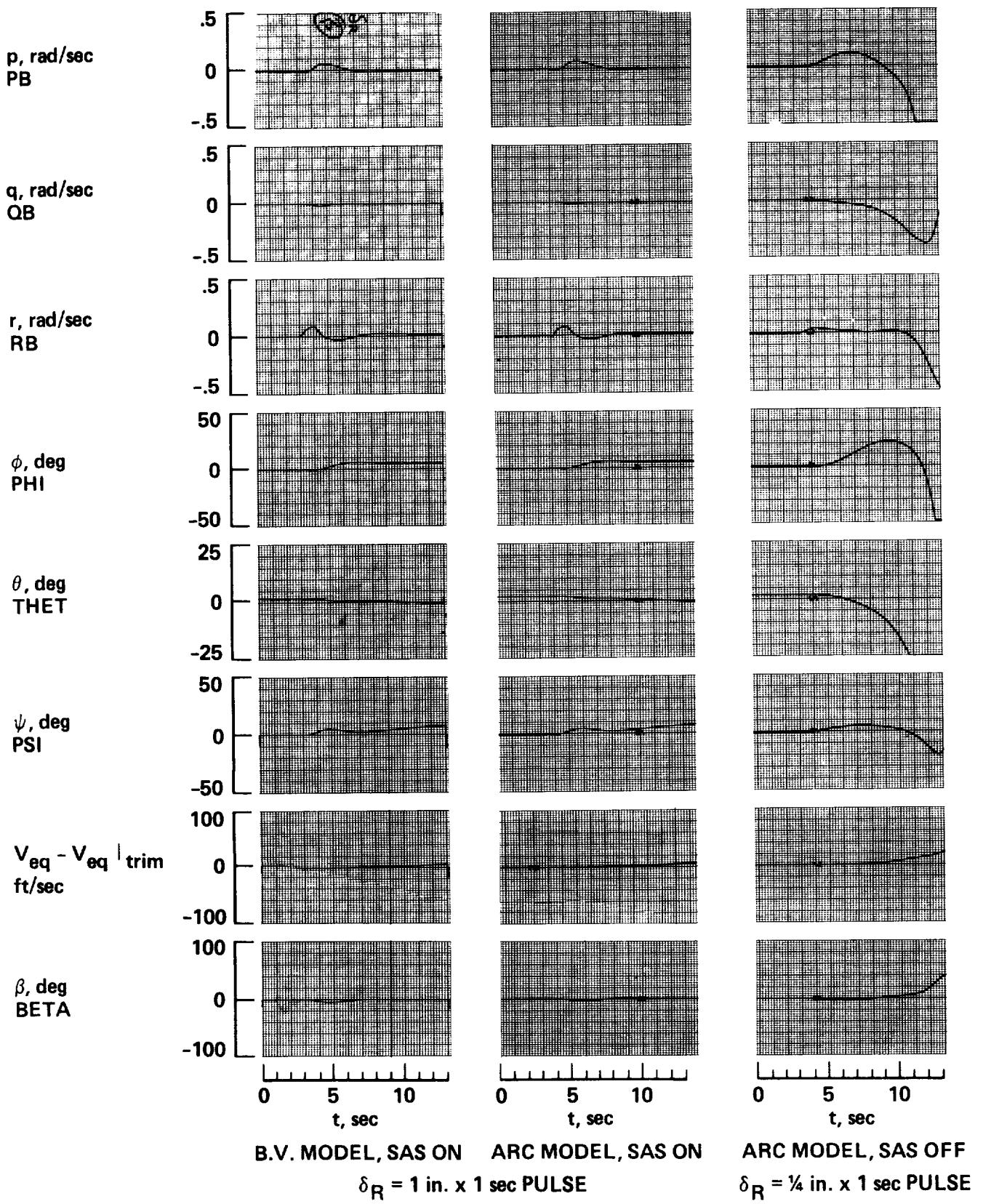


Figure 58.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

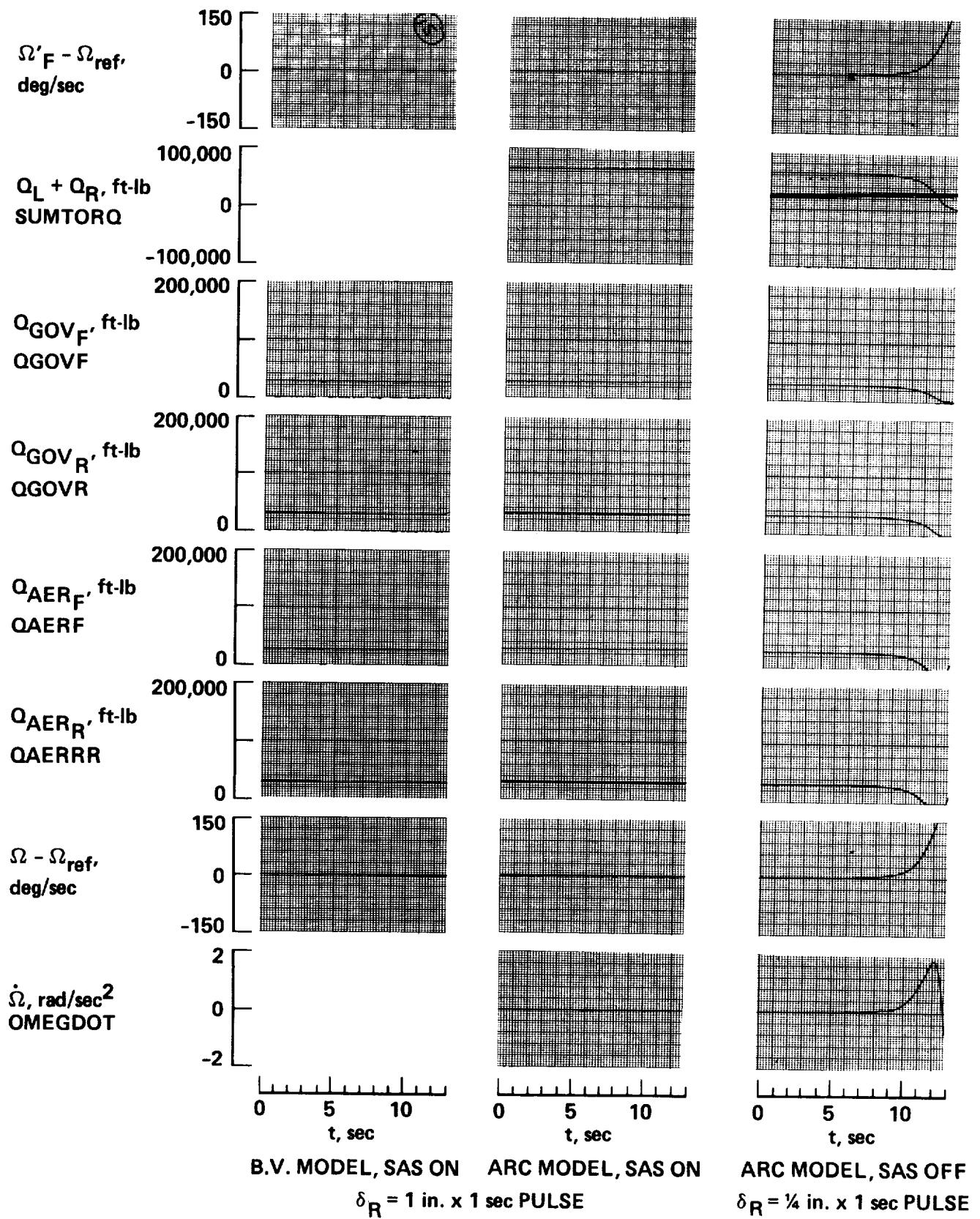


Figure 59.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

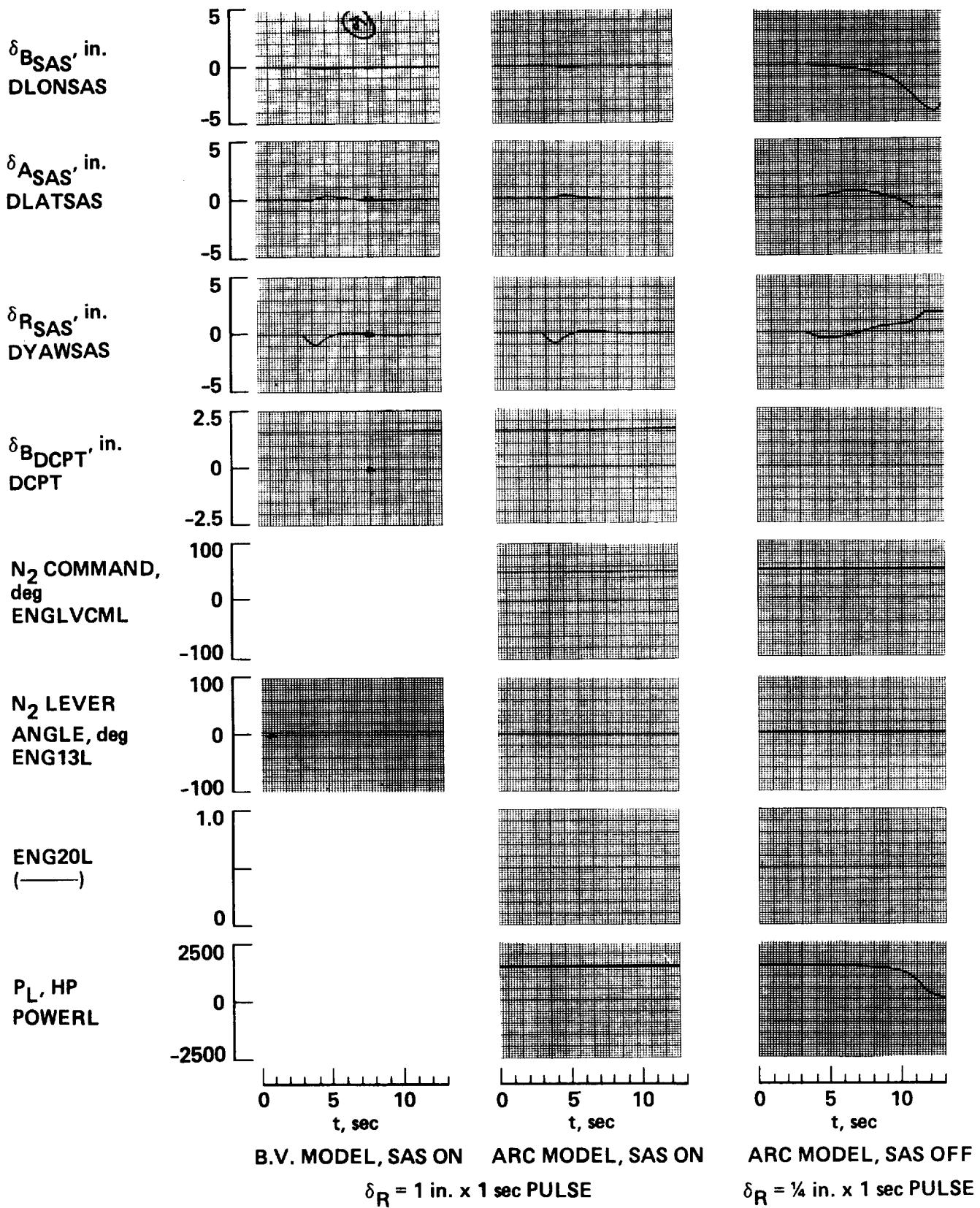


Figure 60.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

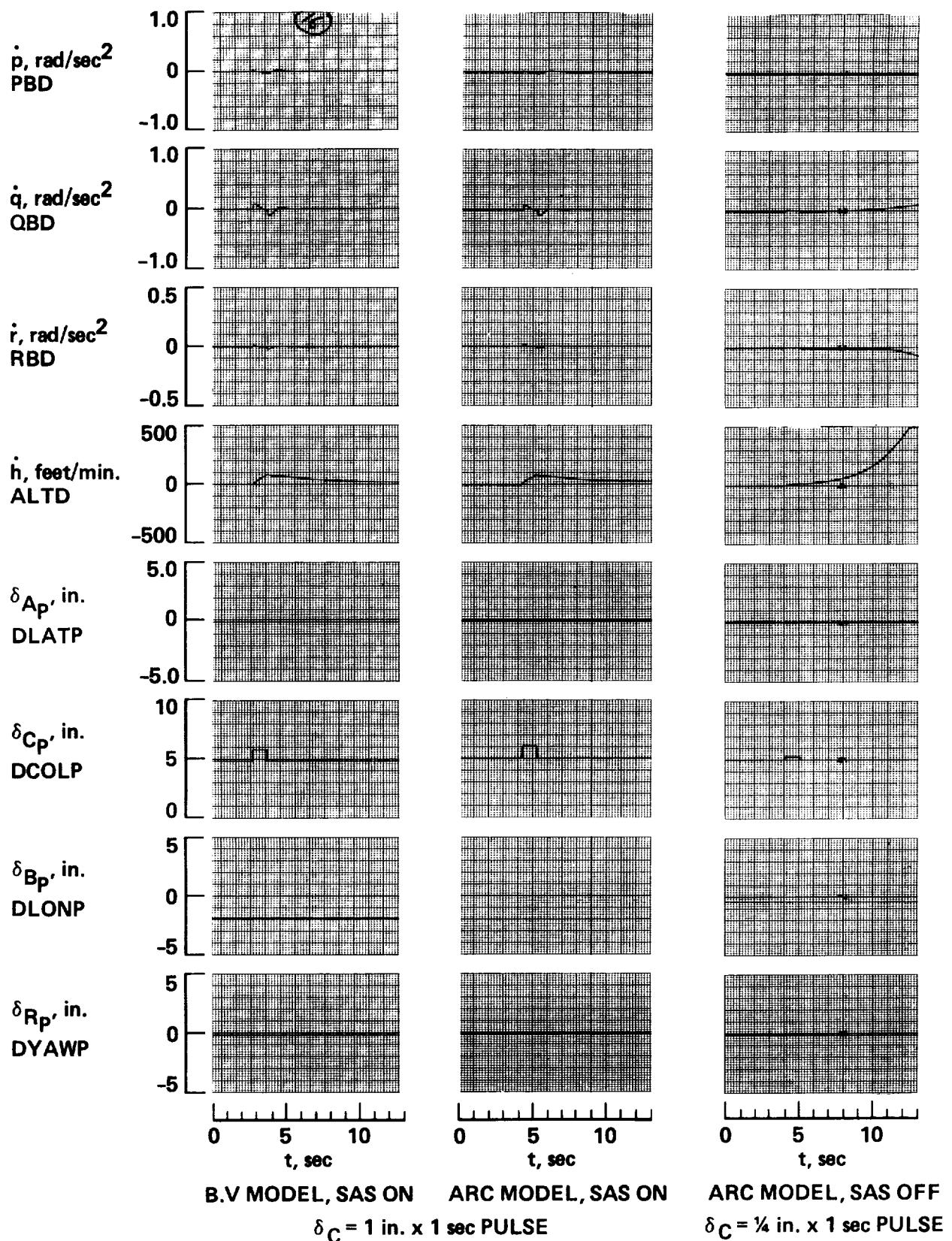


Figure 61.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

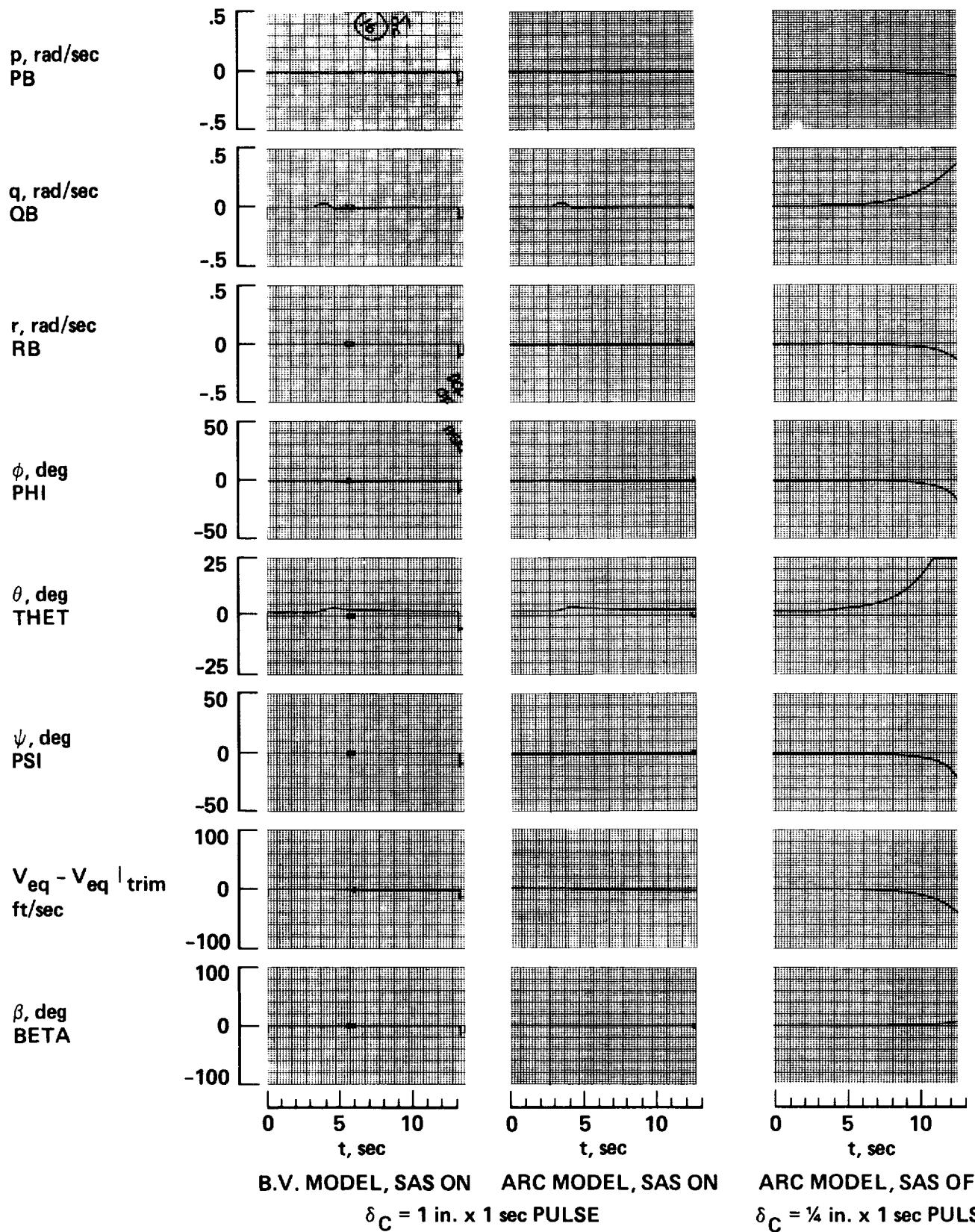


Figure 62.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

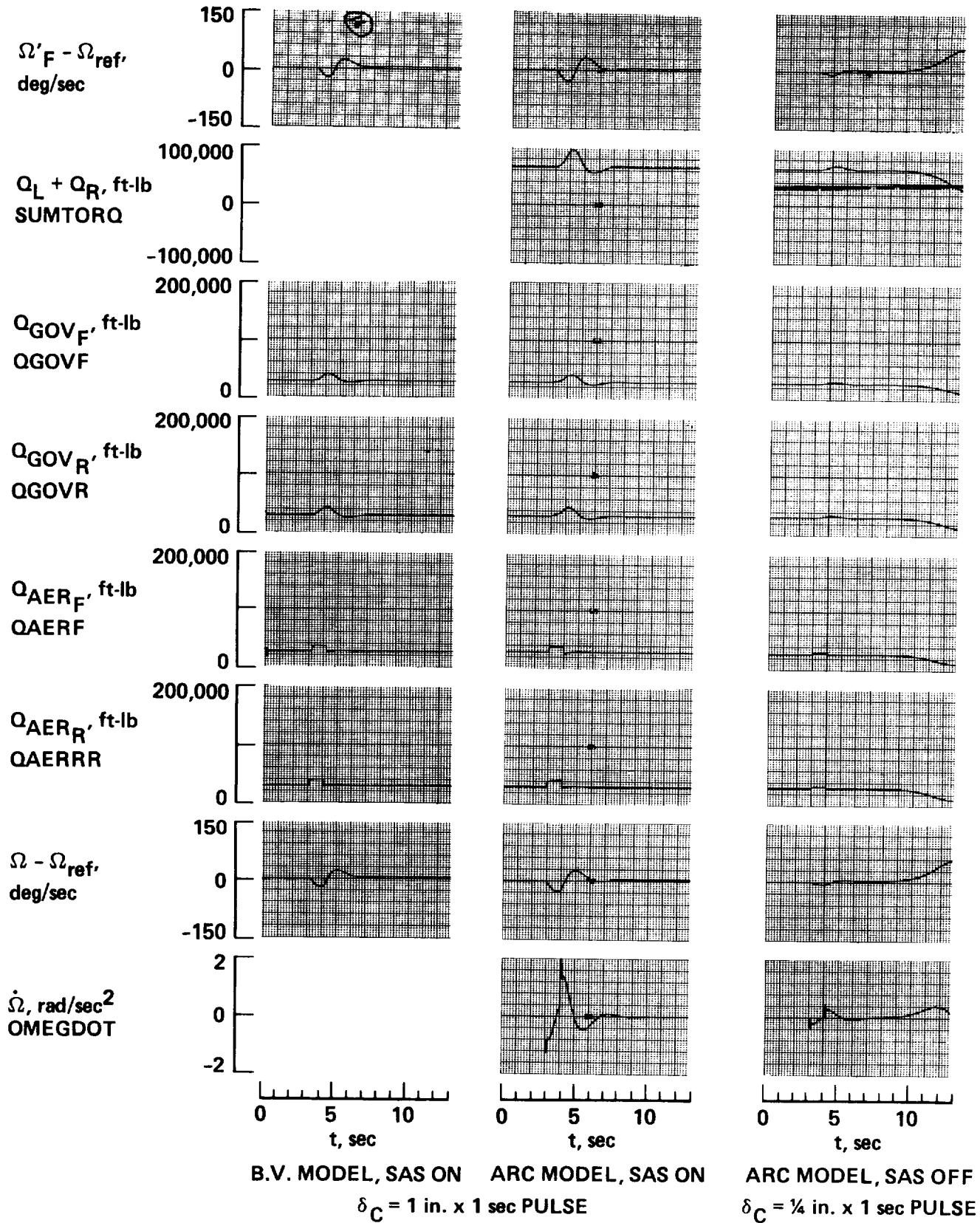


Figure 63.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

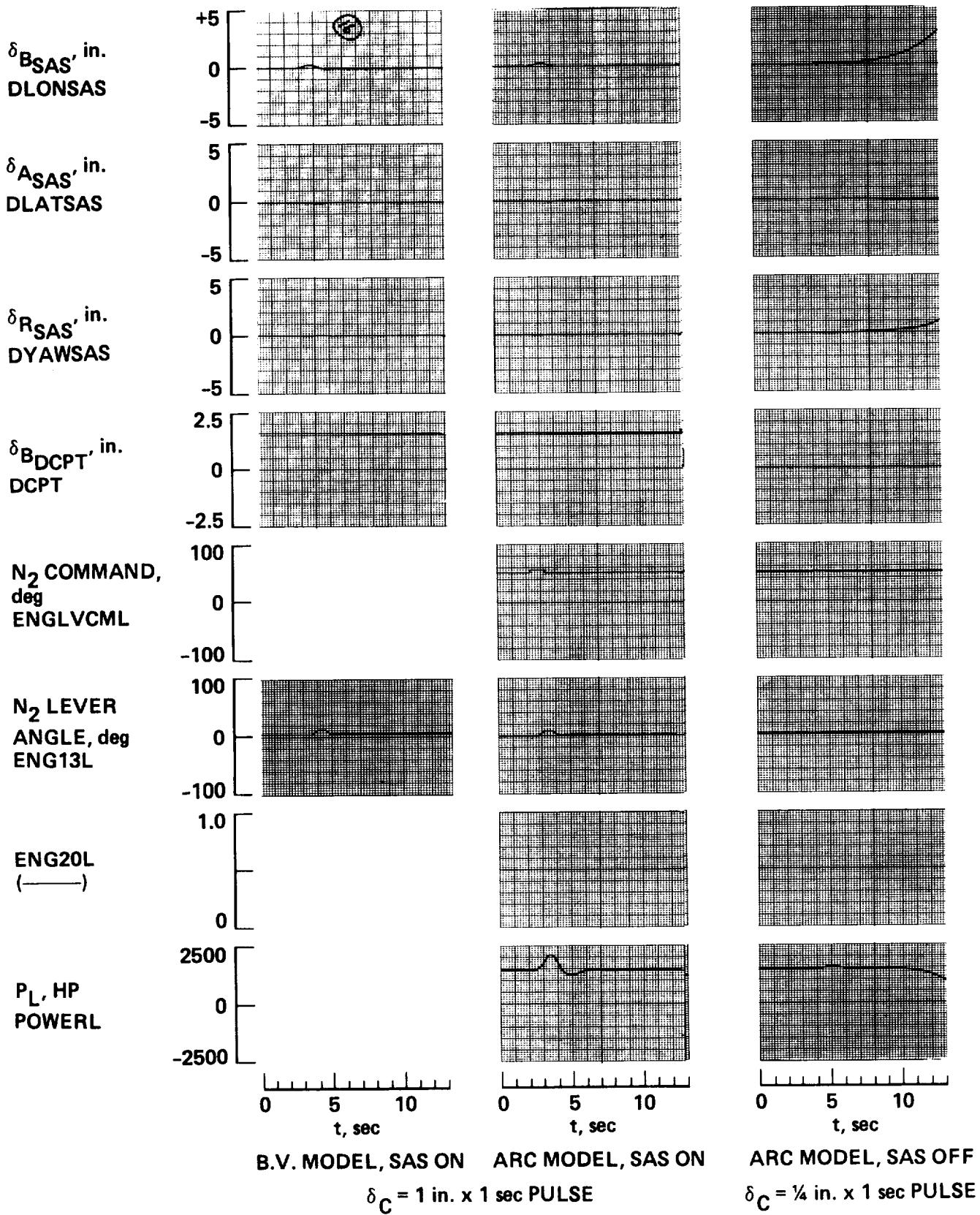


Figure 64.- BV versus ARC simulation response data; $V_{eq} = 115$ knots.

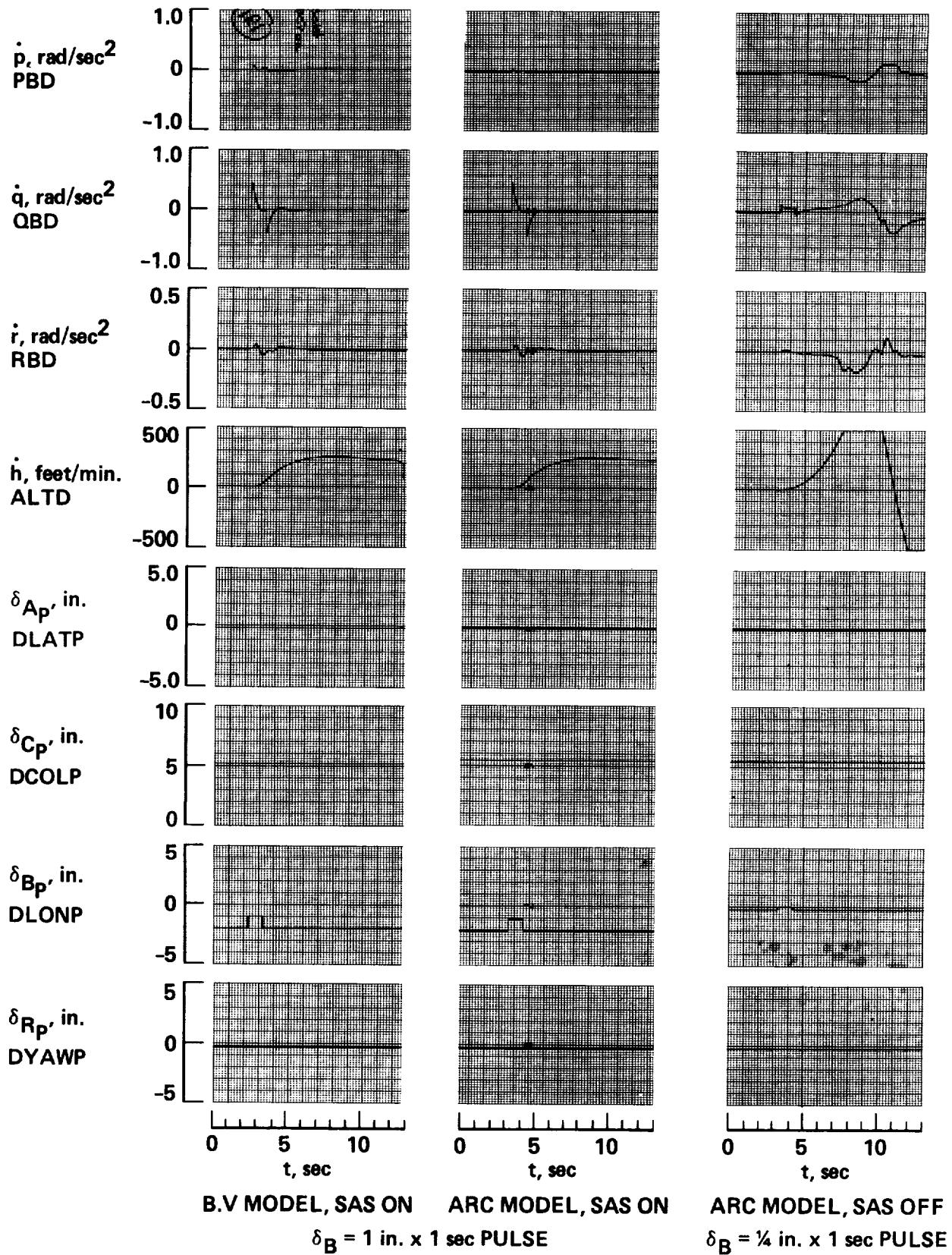


Figure 65.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

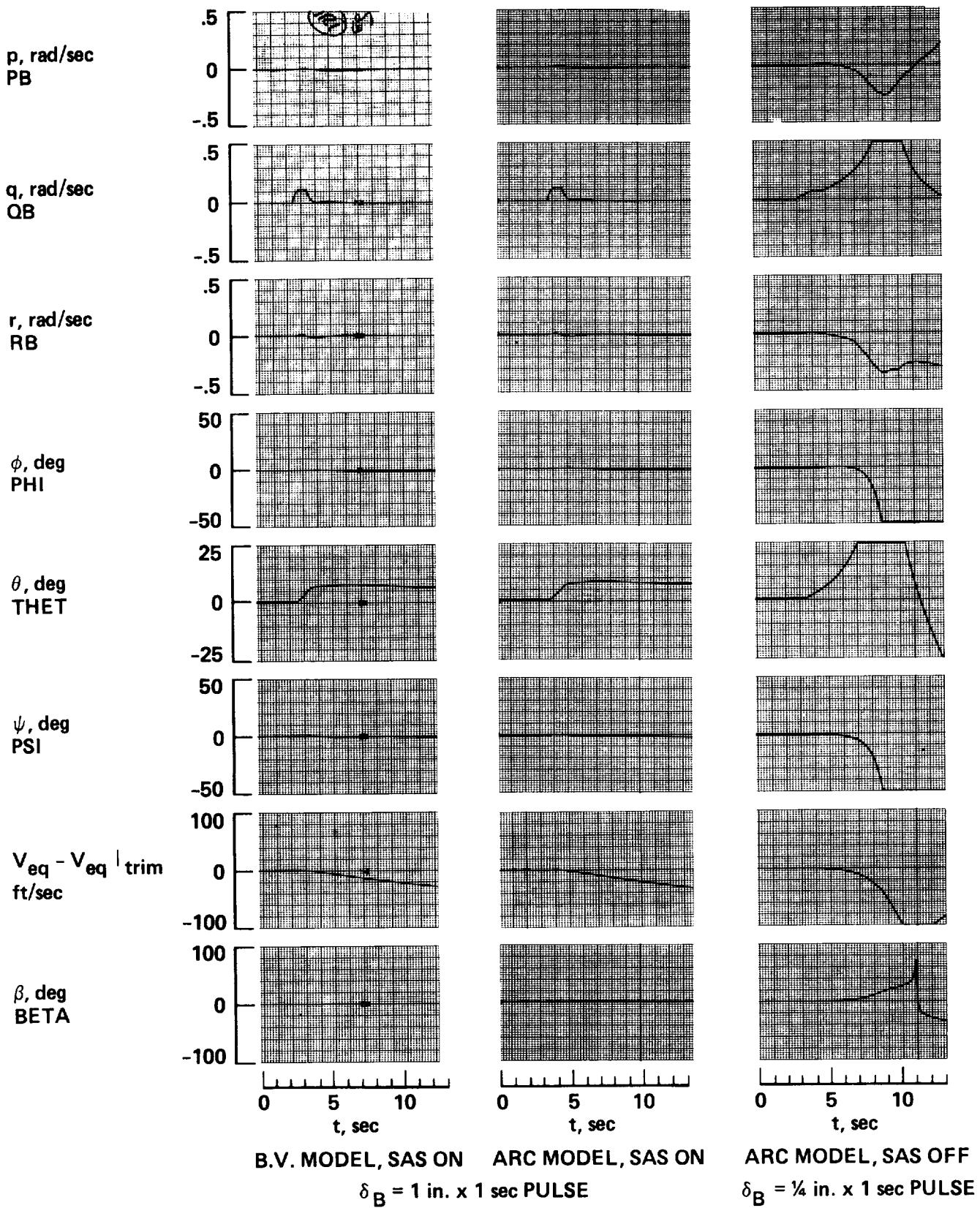


Figure 66.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

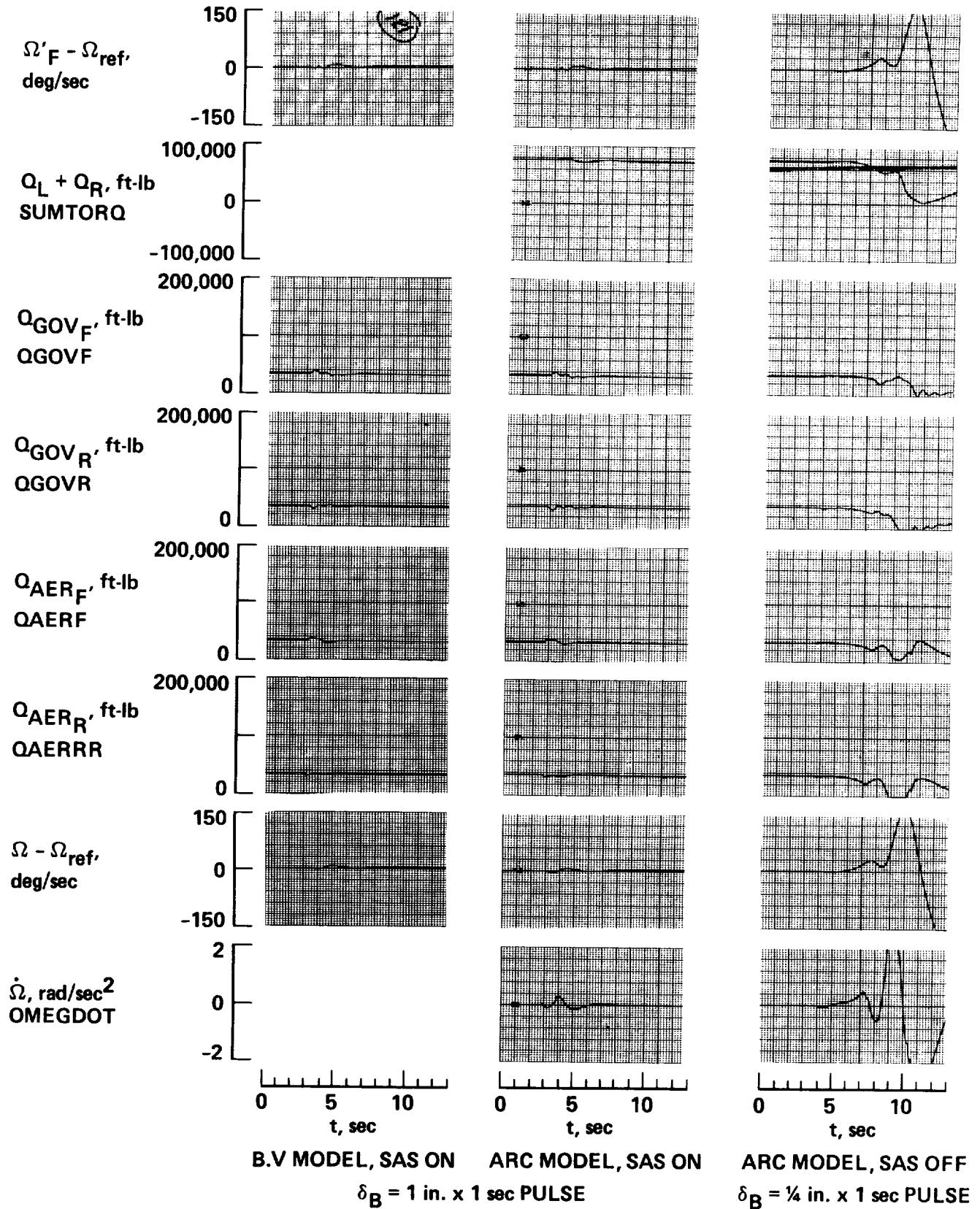


Figure 67.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

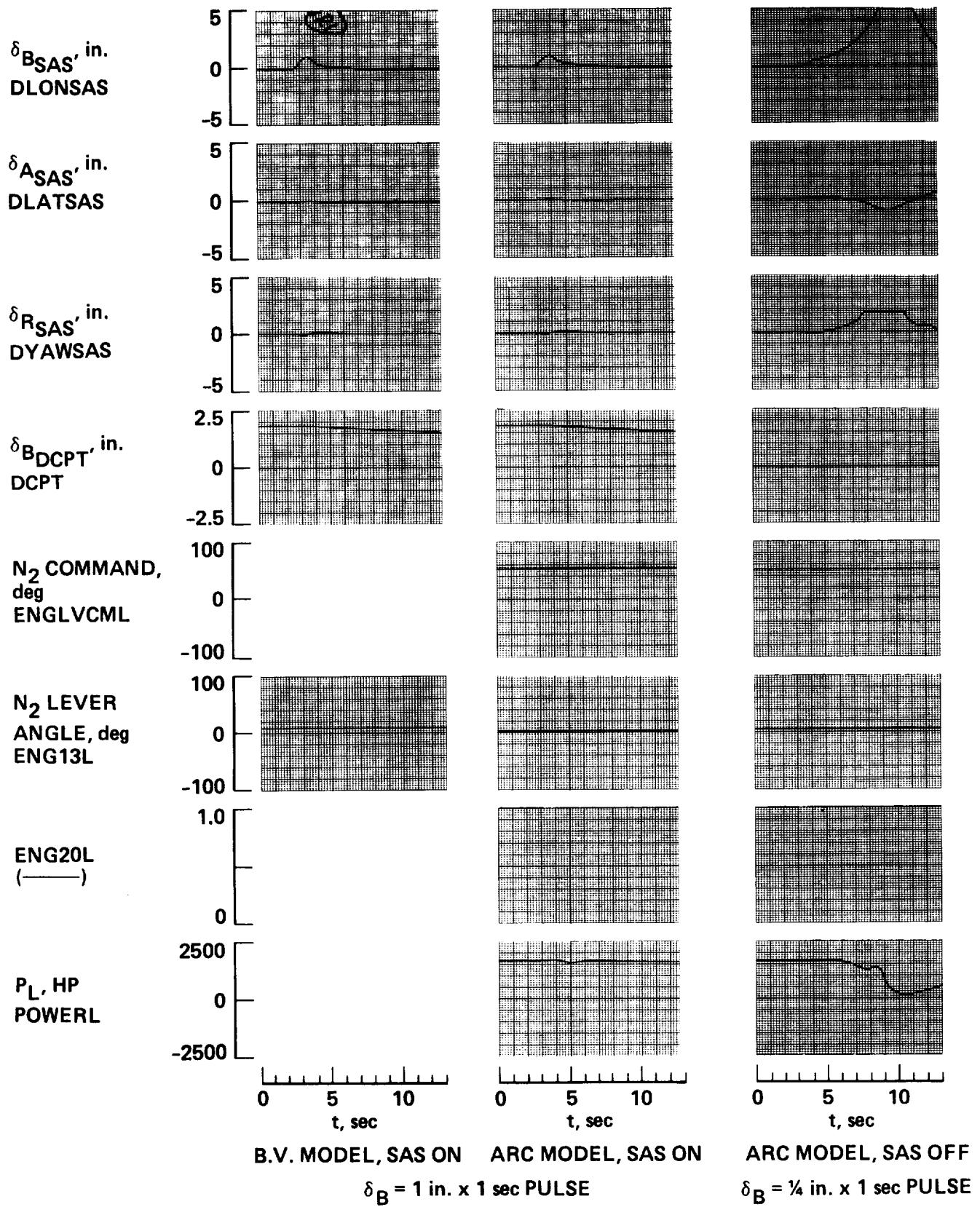


Figure 68.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

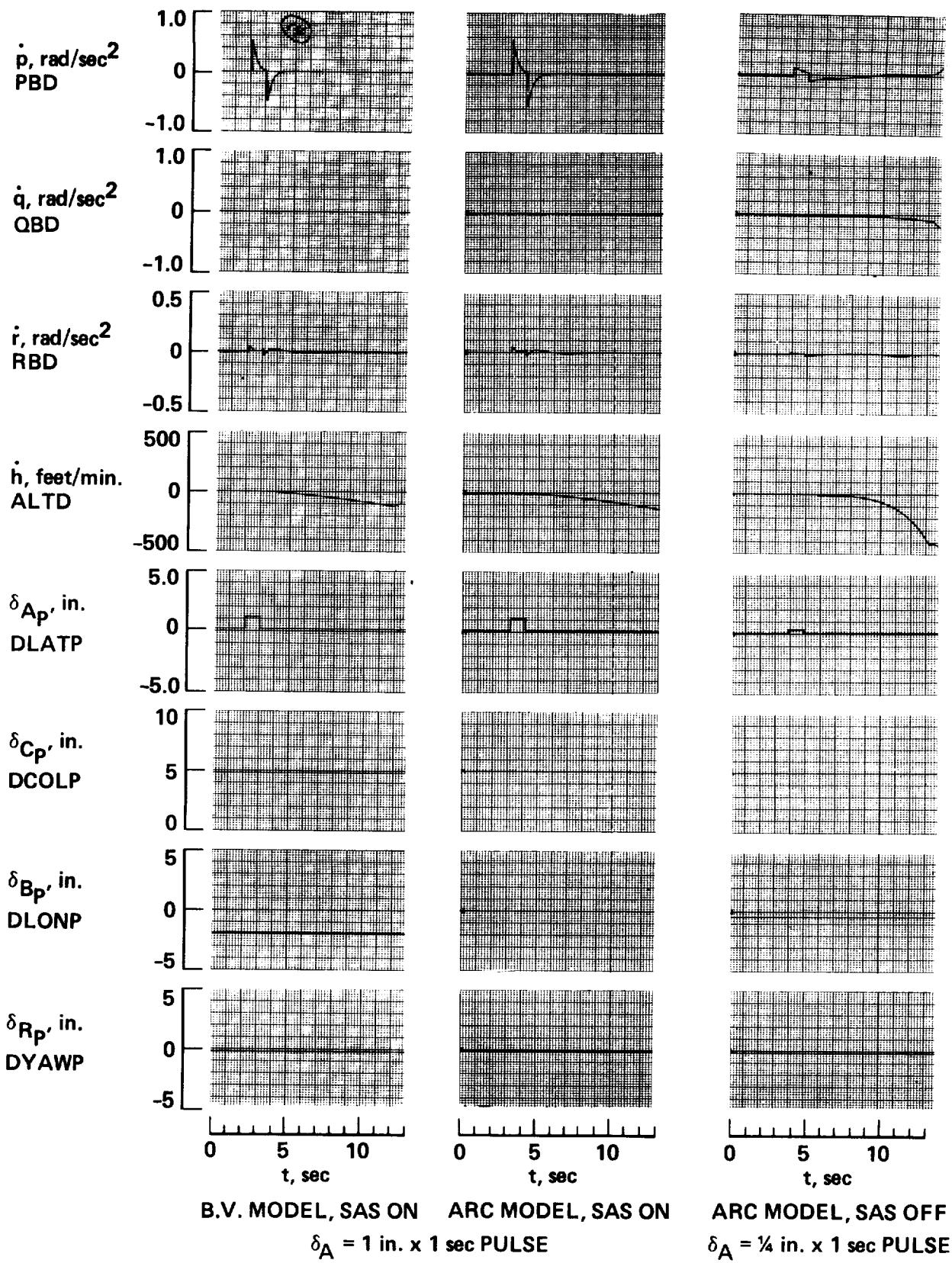


Figure 69.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

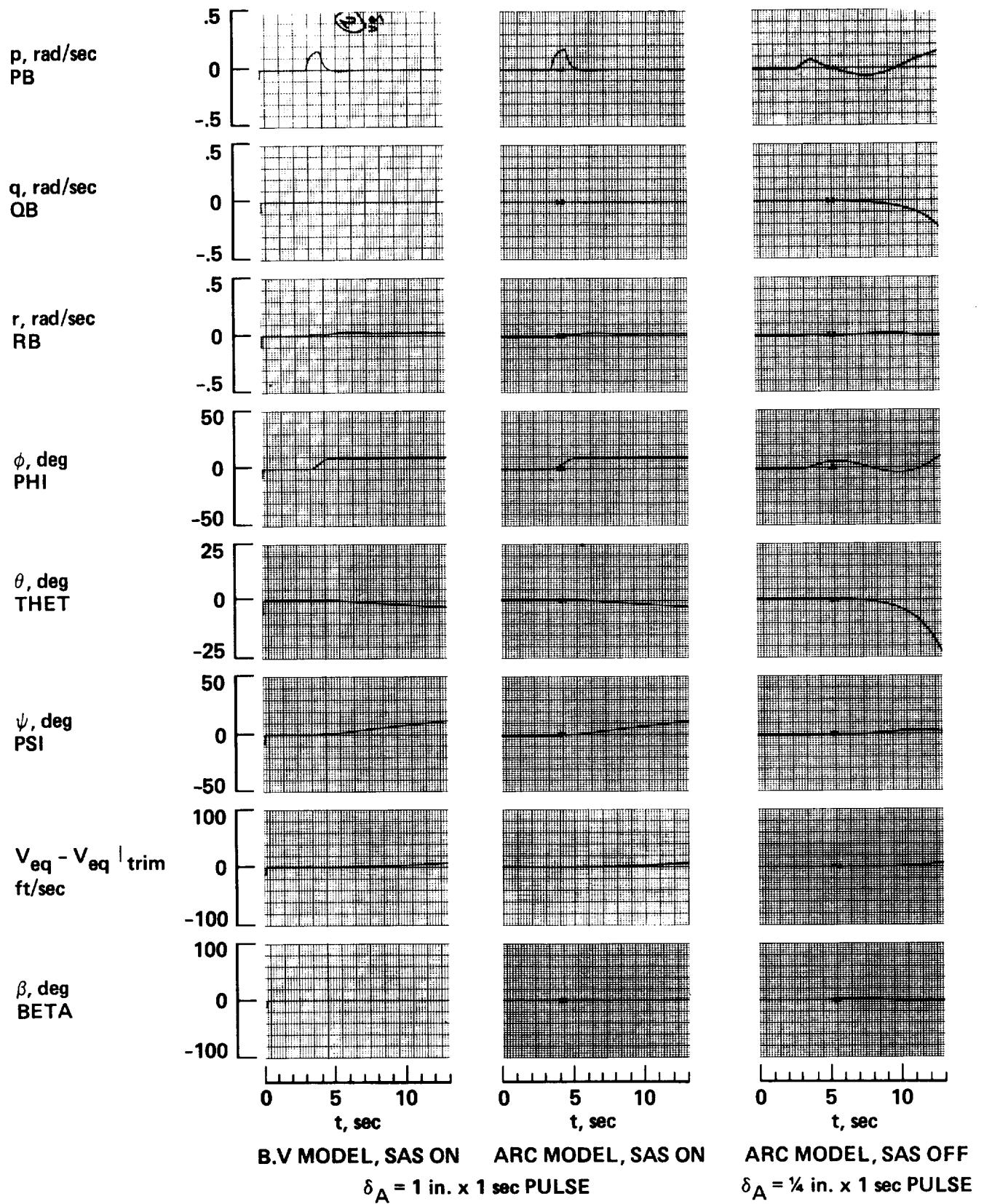


Figure 70.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

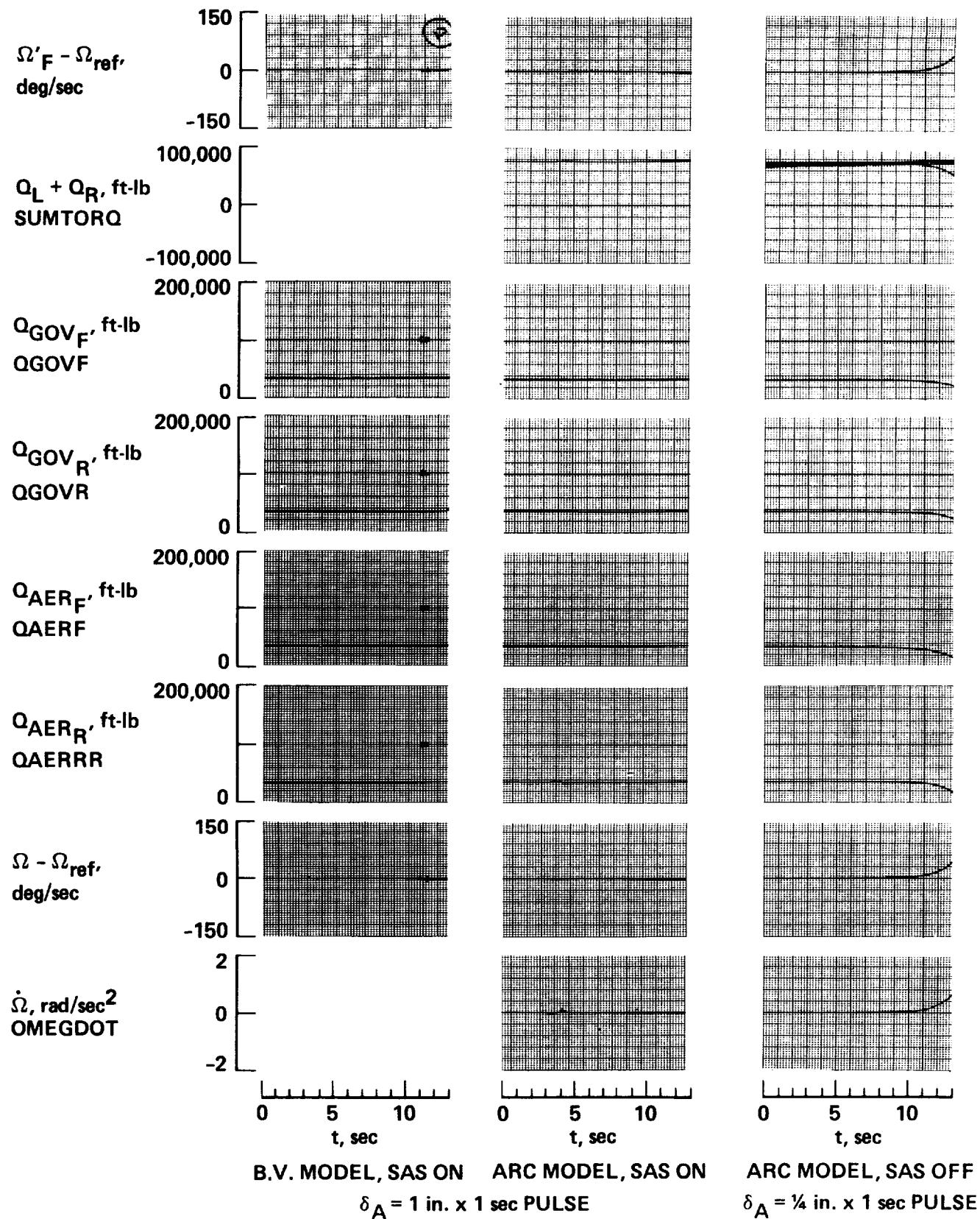


Figure 71.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

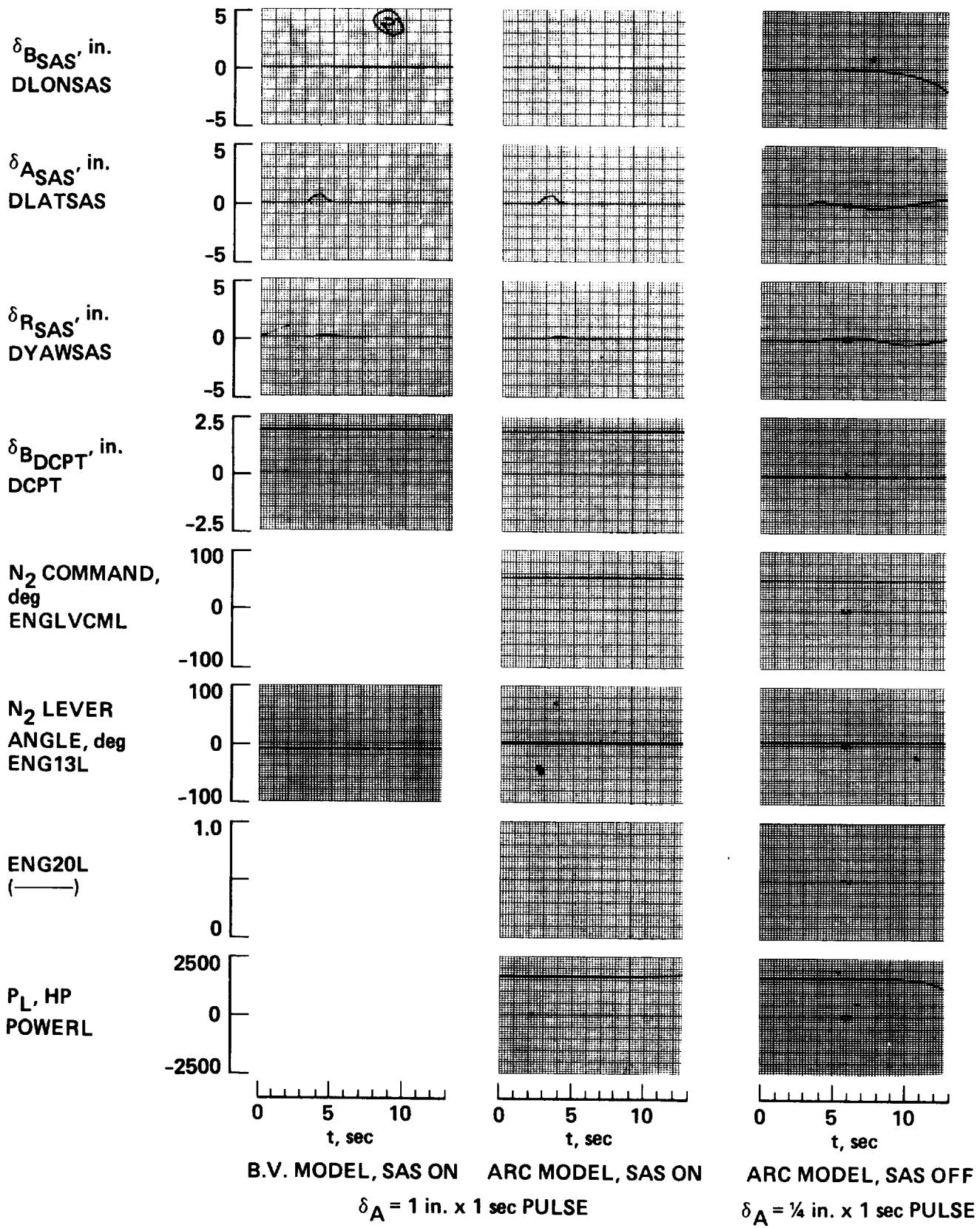


Figure 72.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

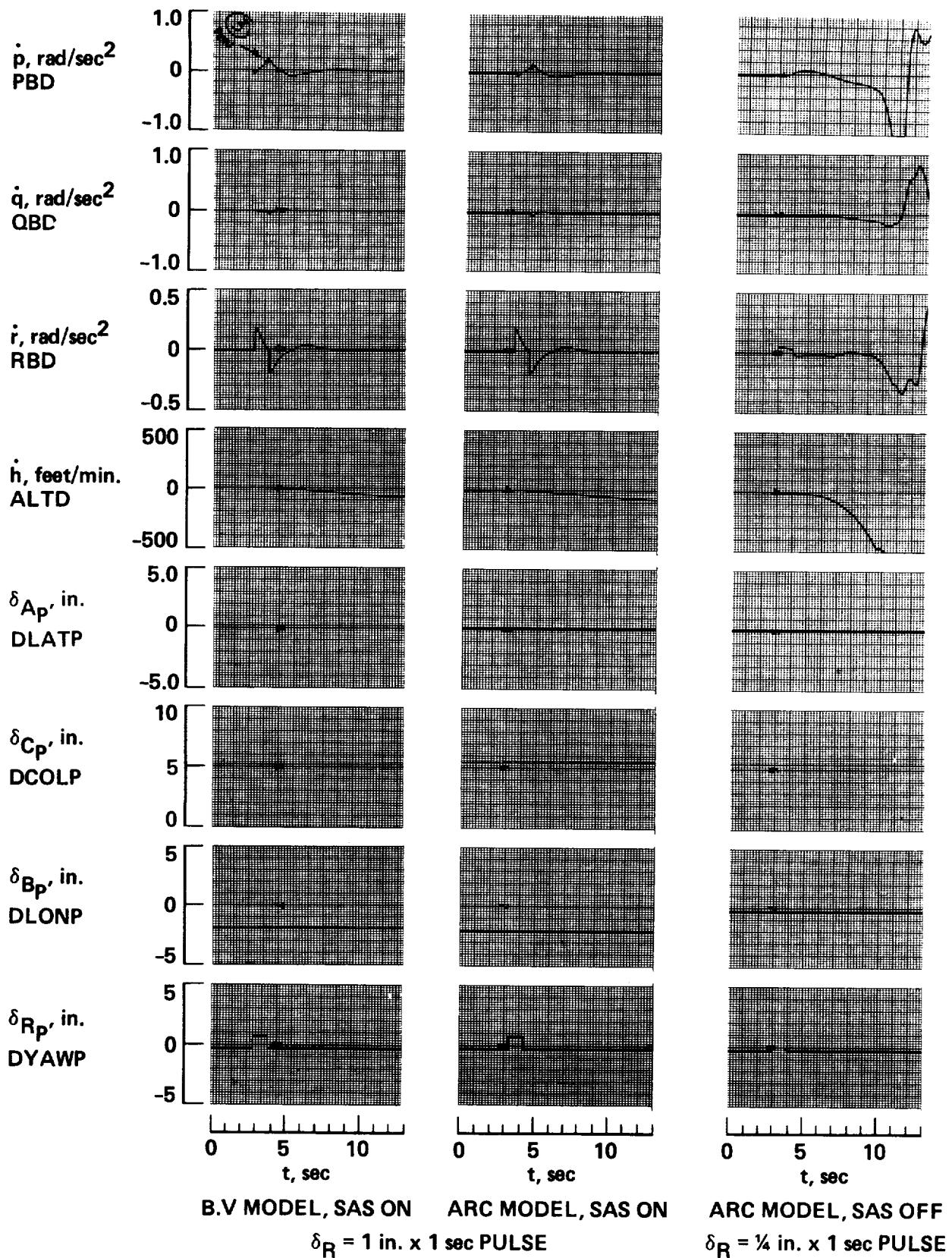


Figure 73.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

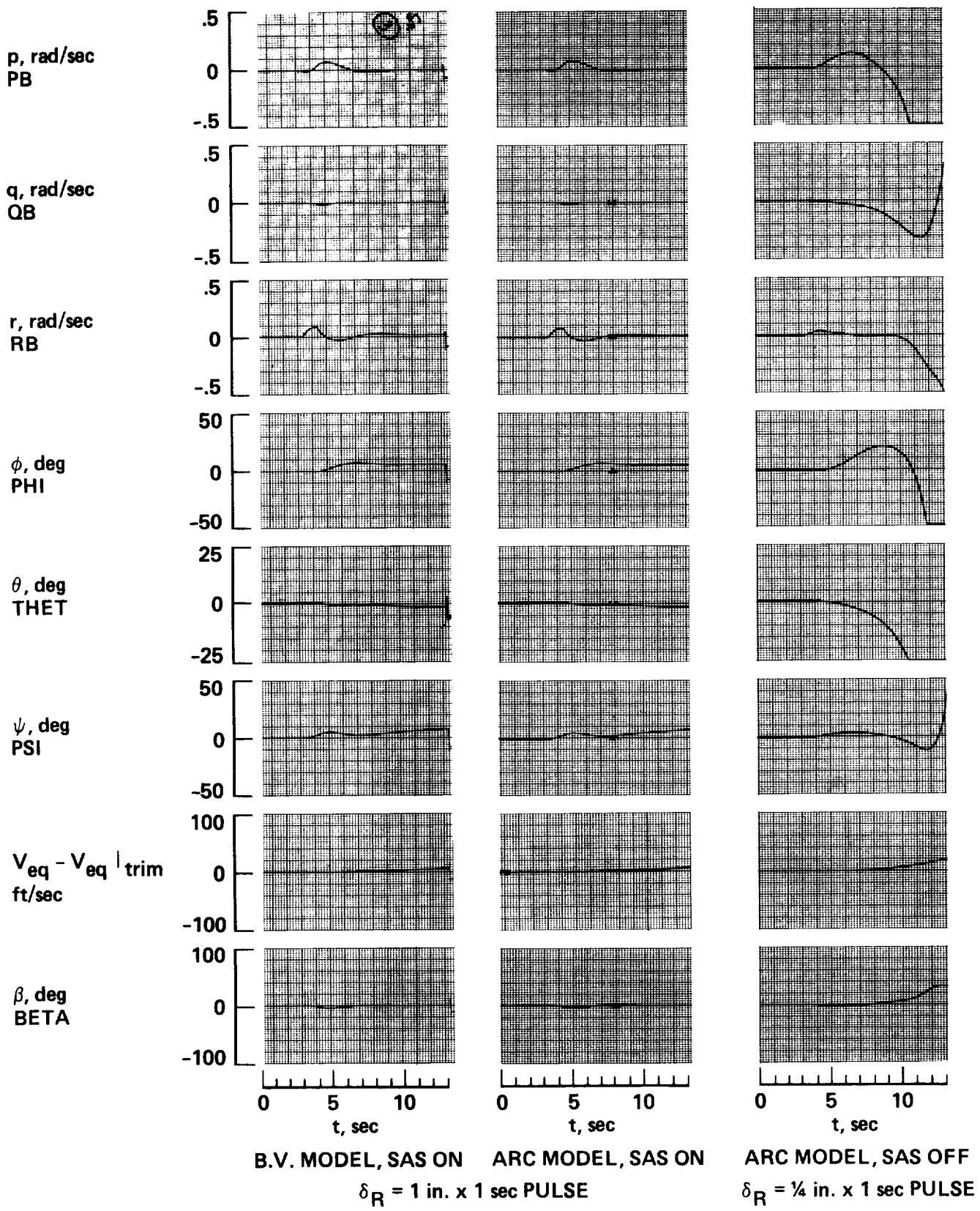


Figure 74.- BV versus ARC simulation response data; $V_{\text{eq}} = 130$ knots.

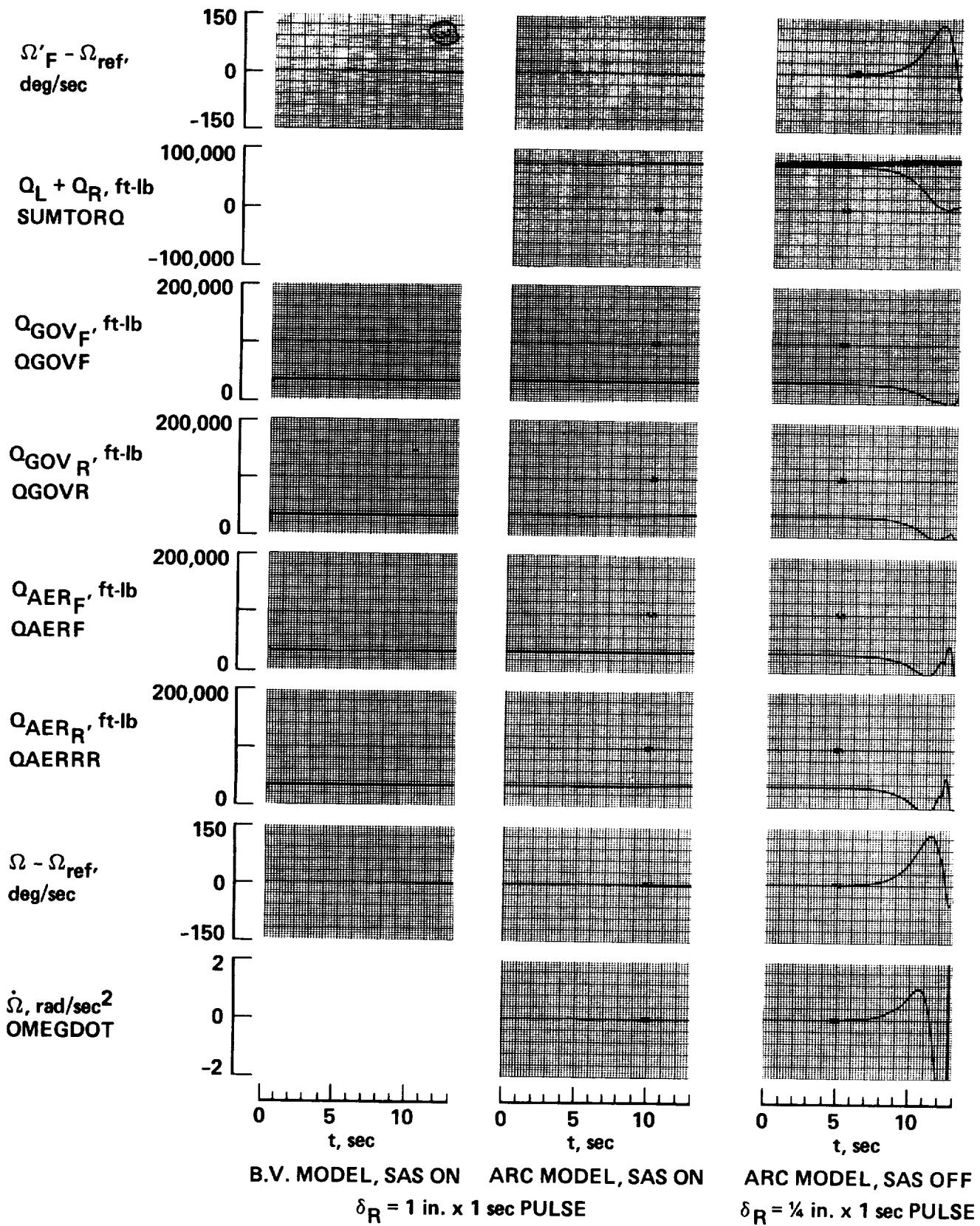


Figure 75.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

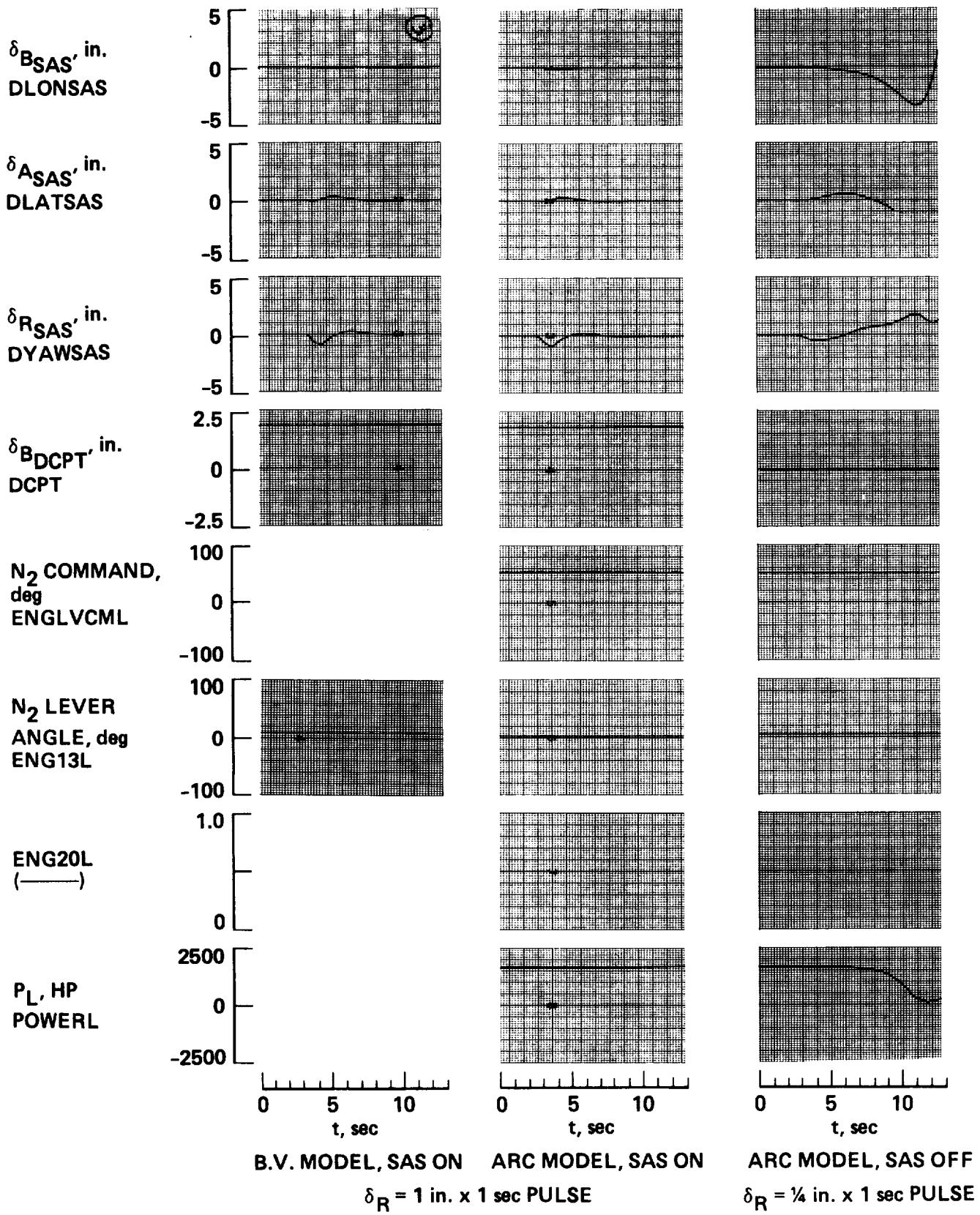


Figure 76.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

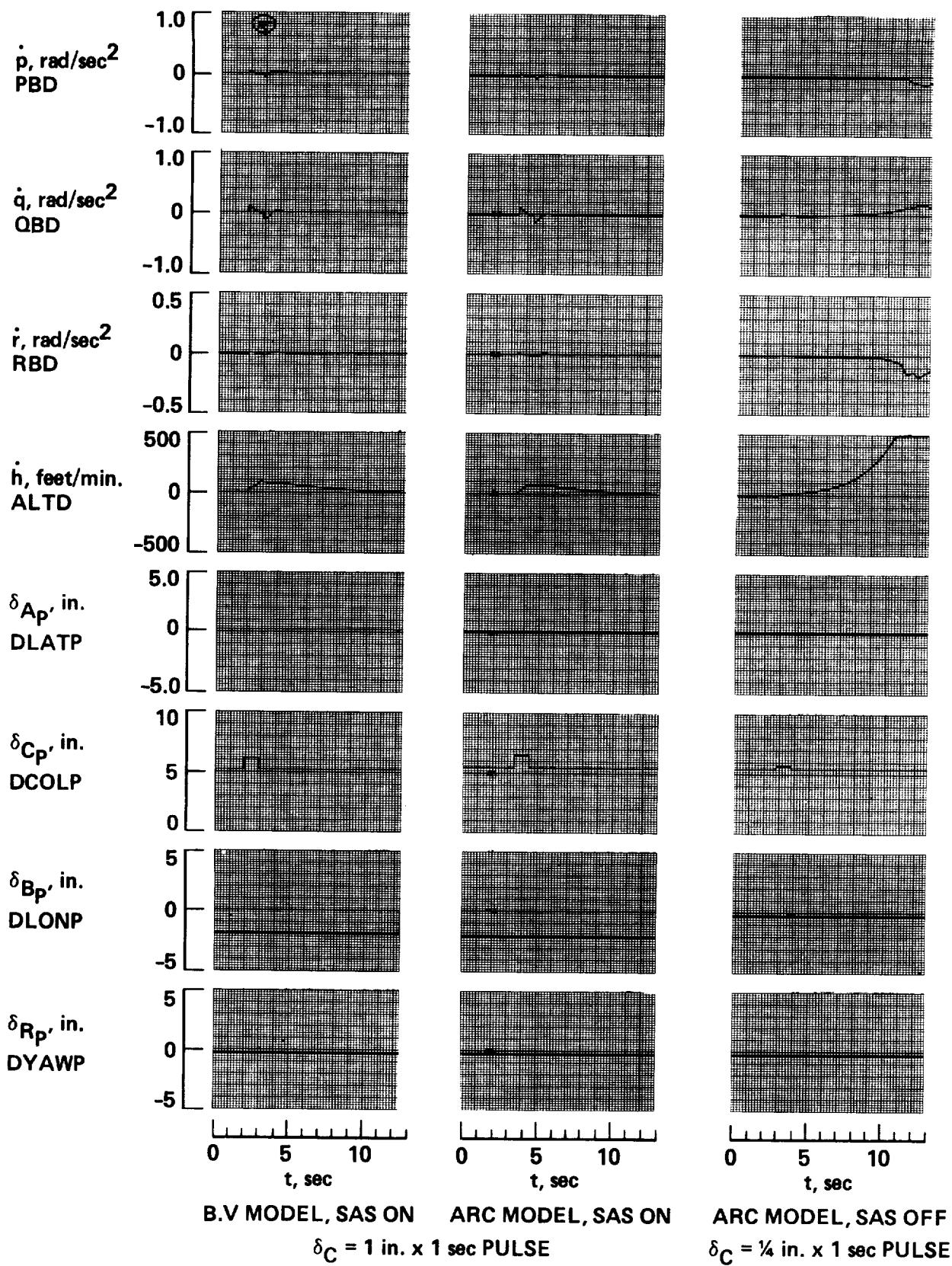


Figure 77.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

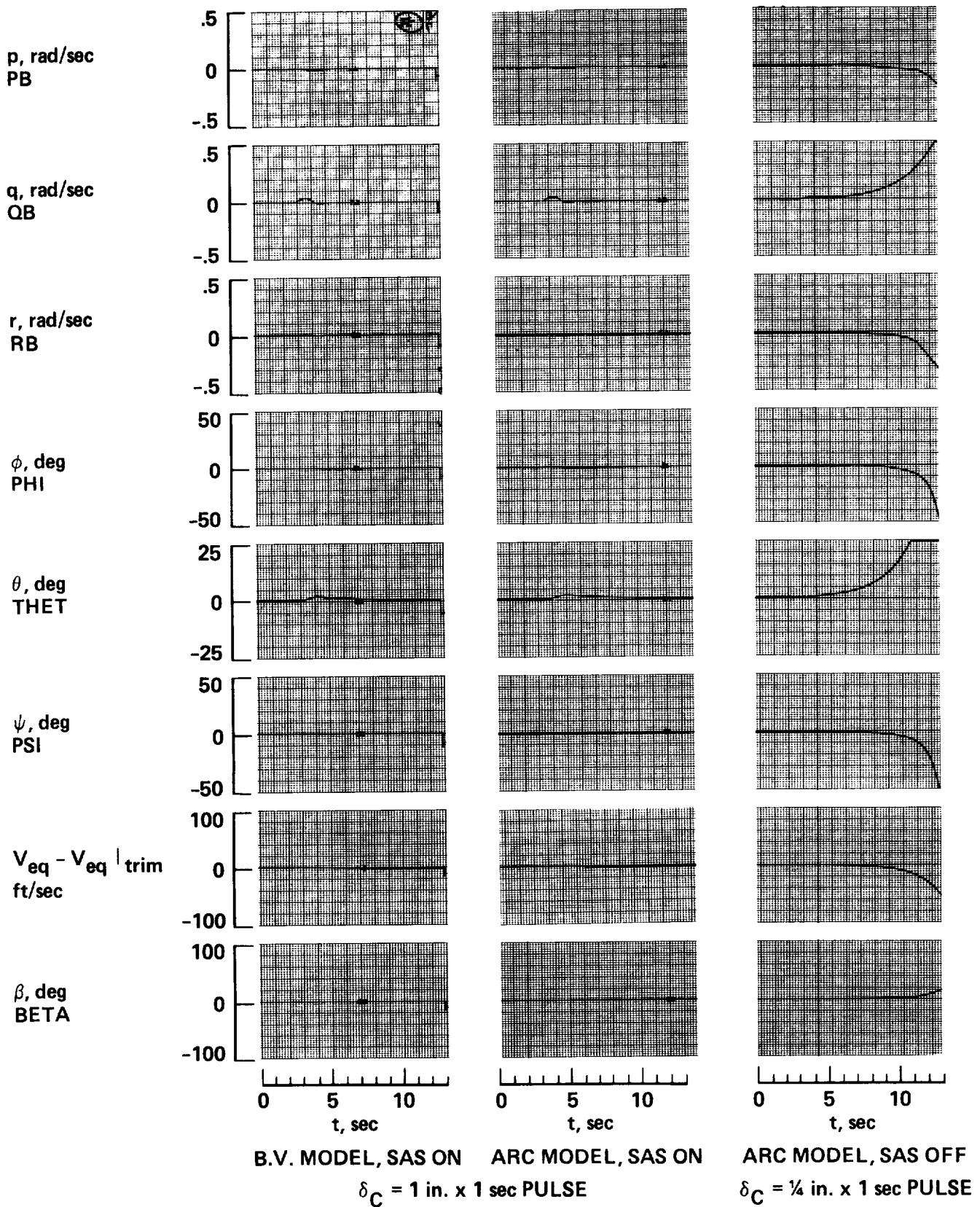


Figure 78.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

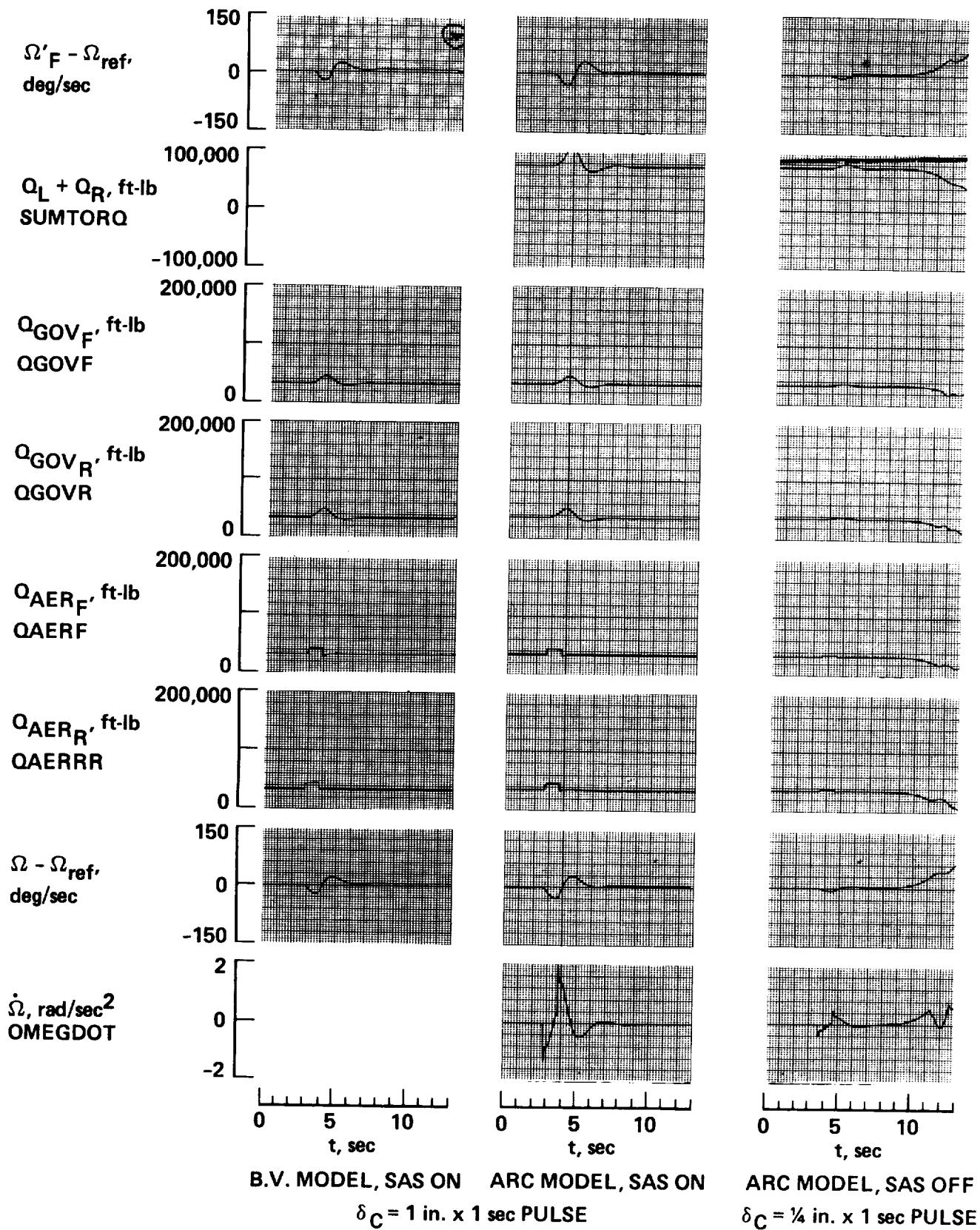


Figure 79.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

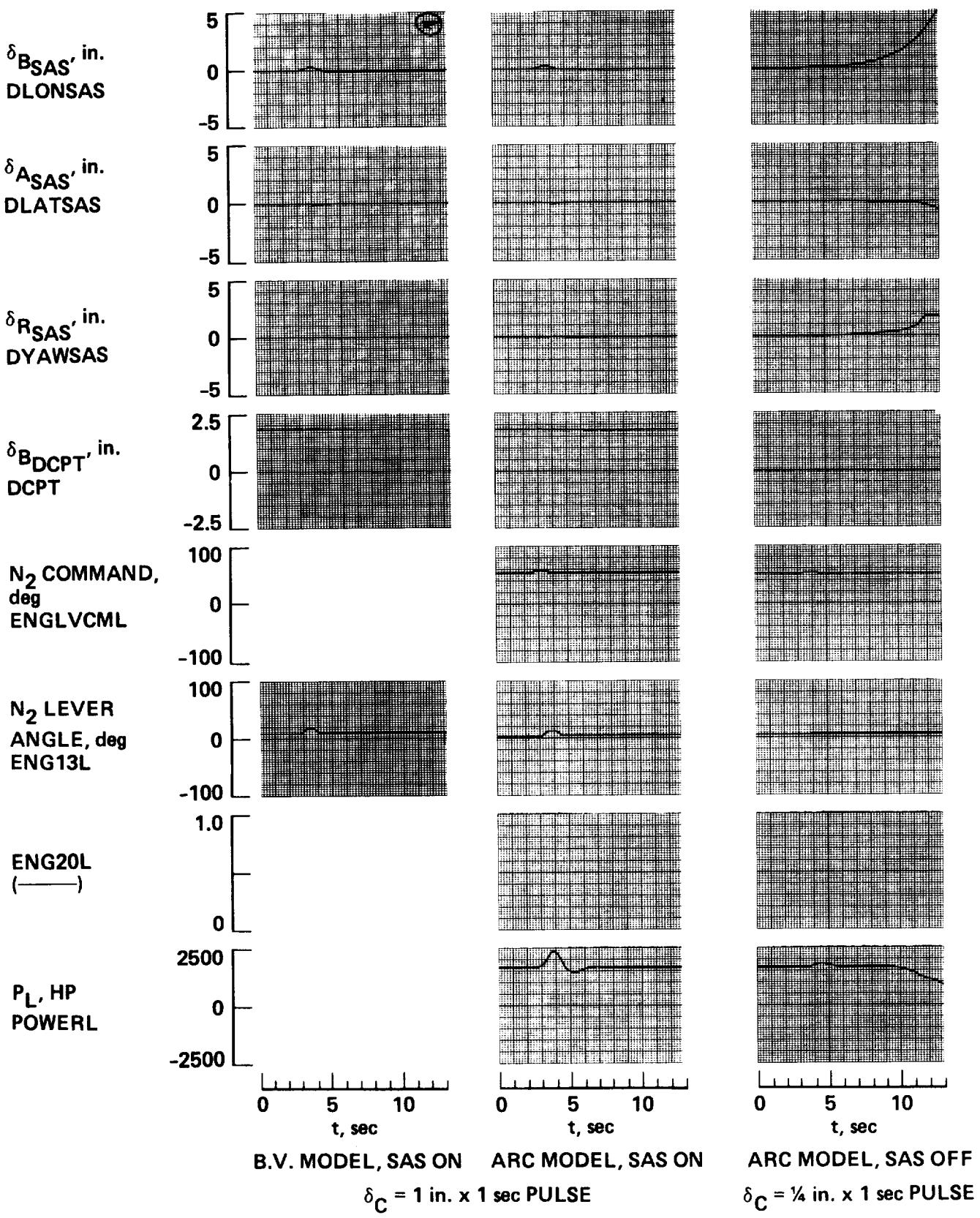


Figure 80.- BV versus ARC simulation response data; $V_{eq} = 130$ knots.

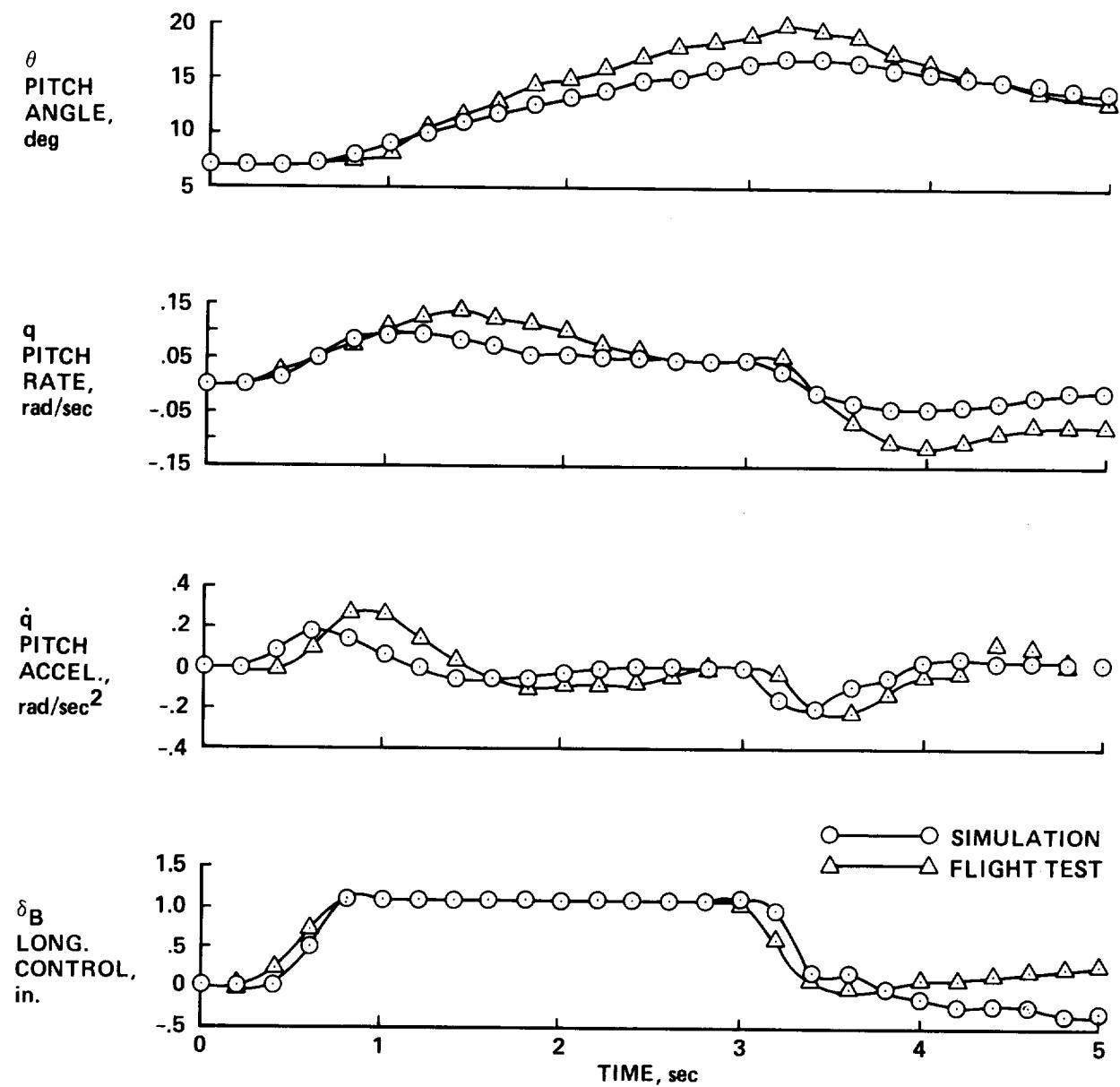


Figure 81.- BV simulation versus flight test dynamic response data (refs. 2,4), hover.

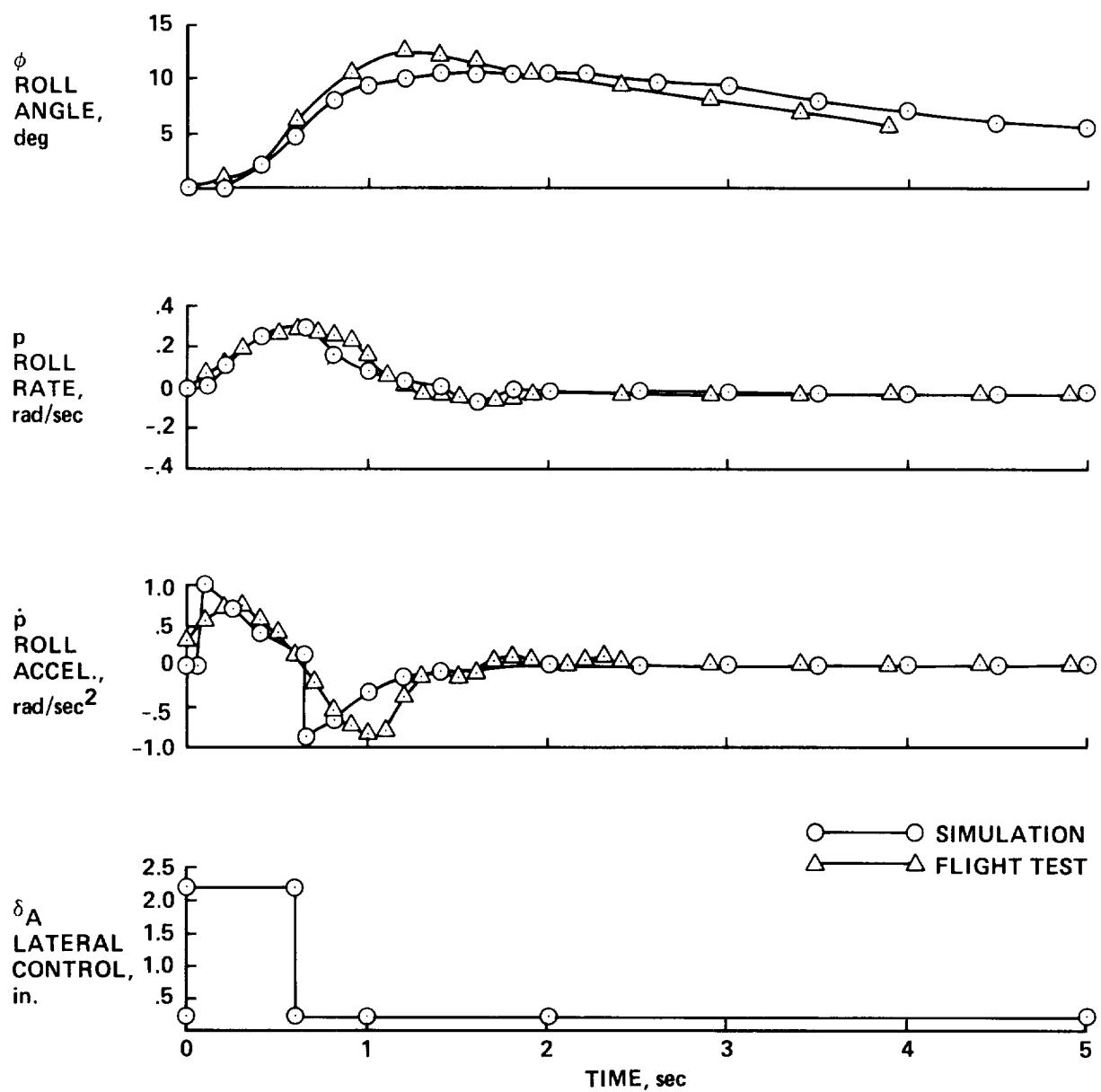


Figure 82.- BV simulation versus flight test dynamic response data (refs. 2,4),
 $V_{eq} = 35$ knots.

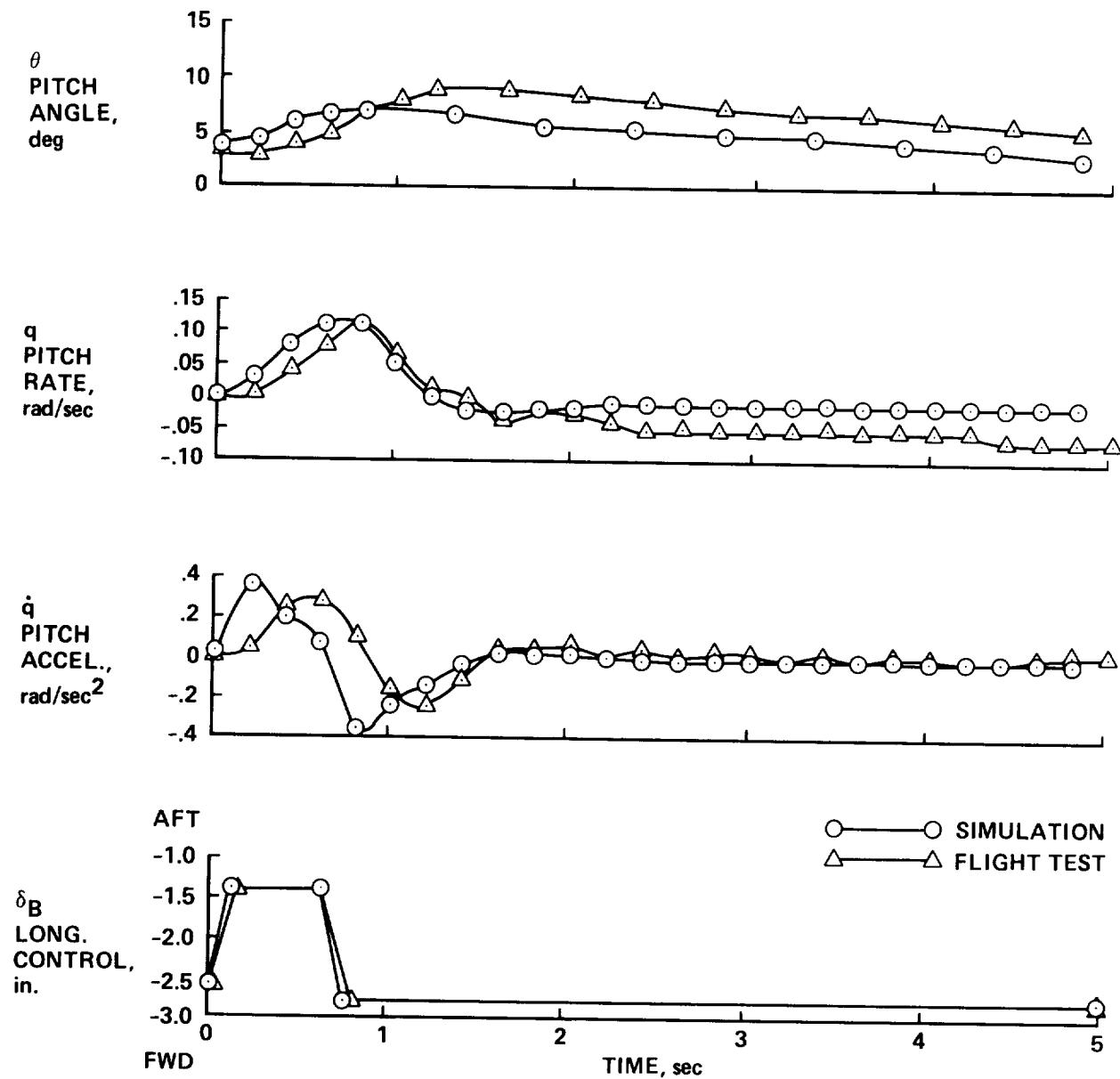


Figure 83.- BV simulation versus flight test dynamic response data (refs. 2,4),
 $V_{eq} = 70$ knots.

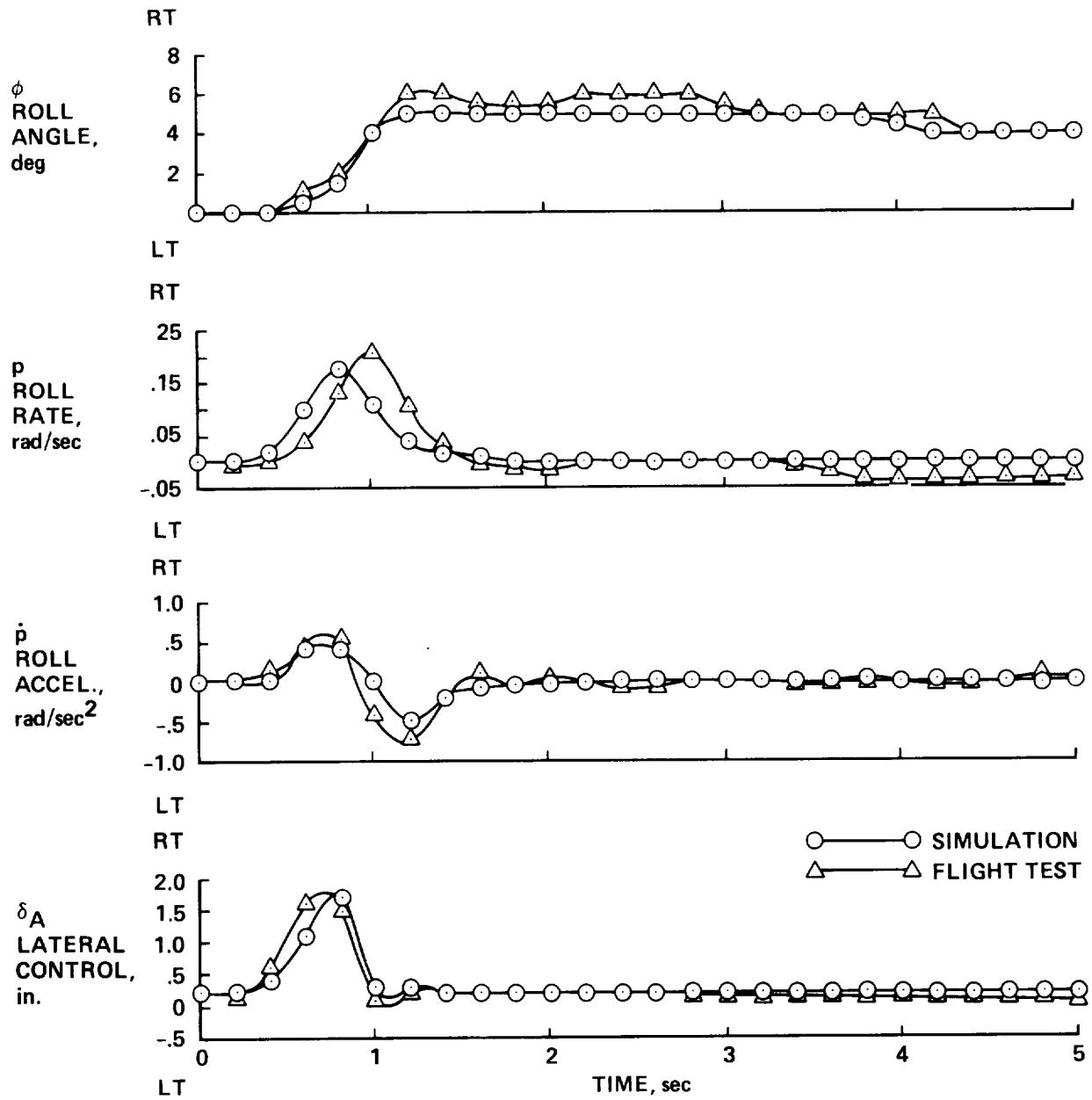


Figure 84.- BV simulation versus flight test dynamic response data (refs. 2,4),
 $V_{eq} = 110$ knots.

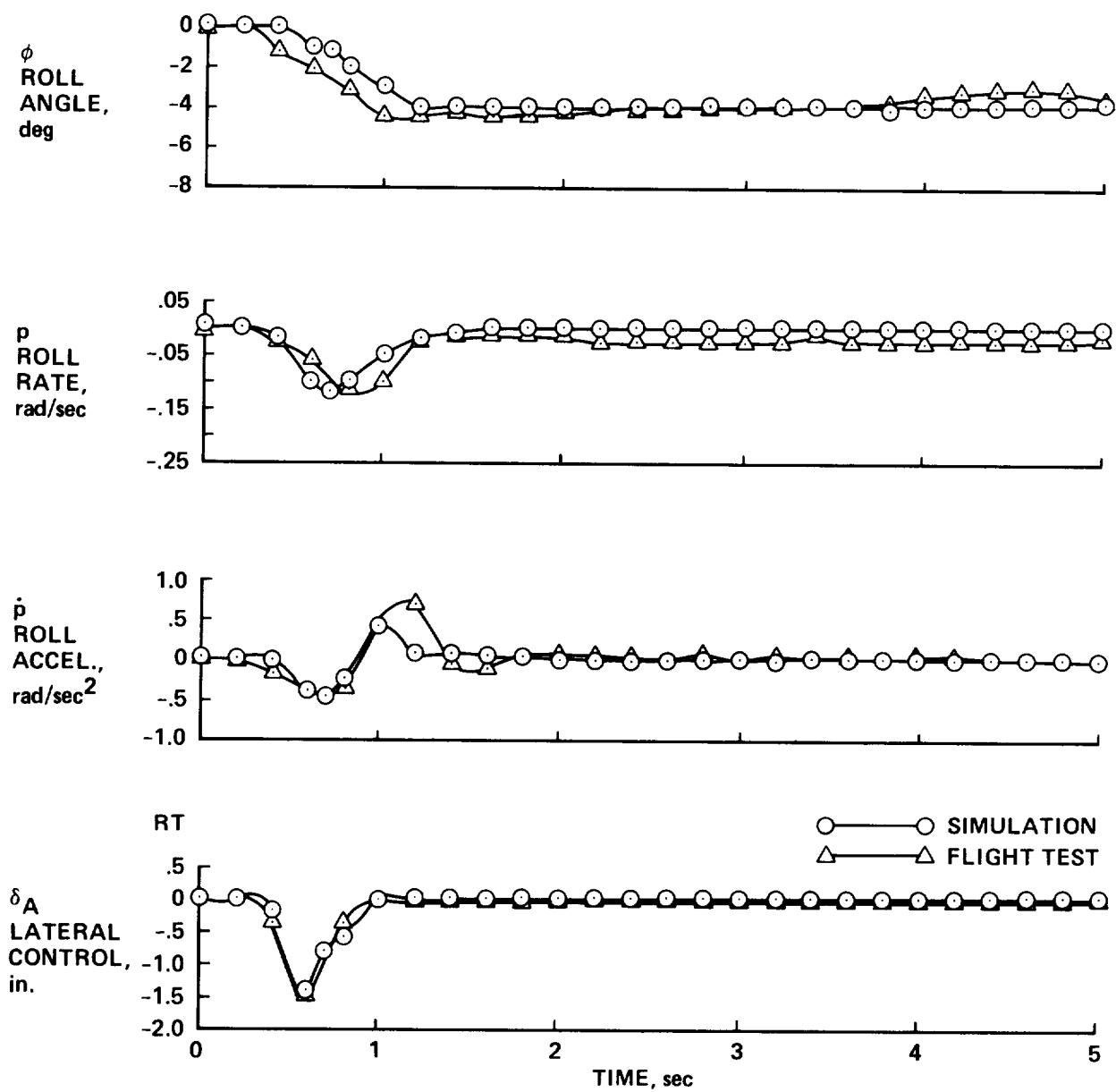


Figure 85.- BV simulation versus flight test dynamic response data (refs. 2,4),
 $V_{eq} = 115$ knots.

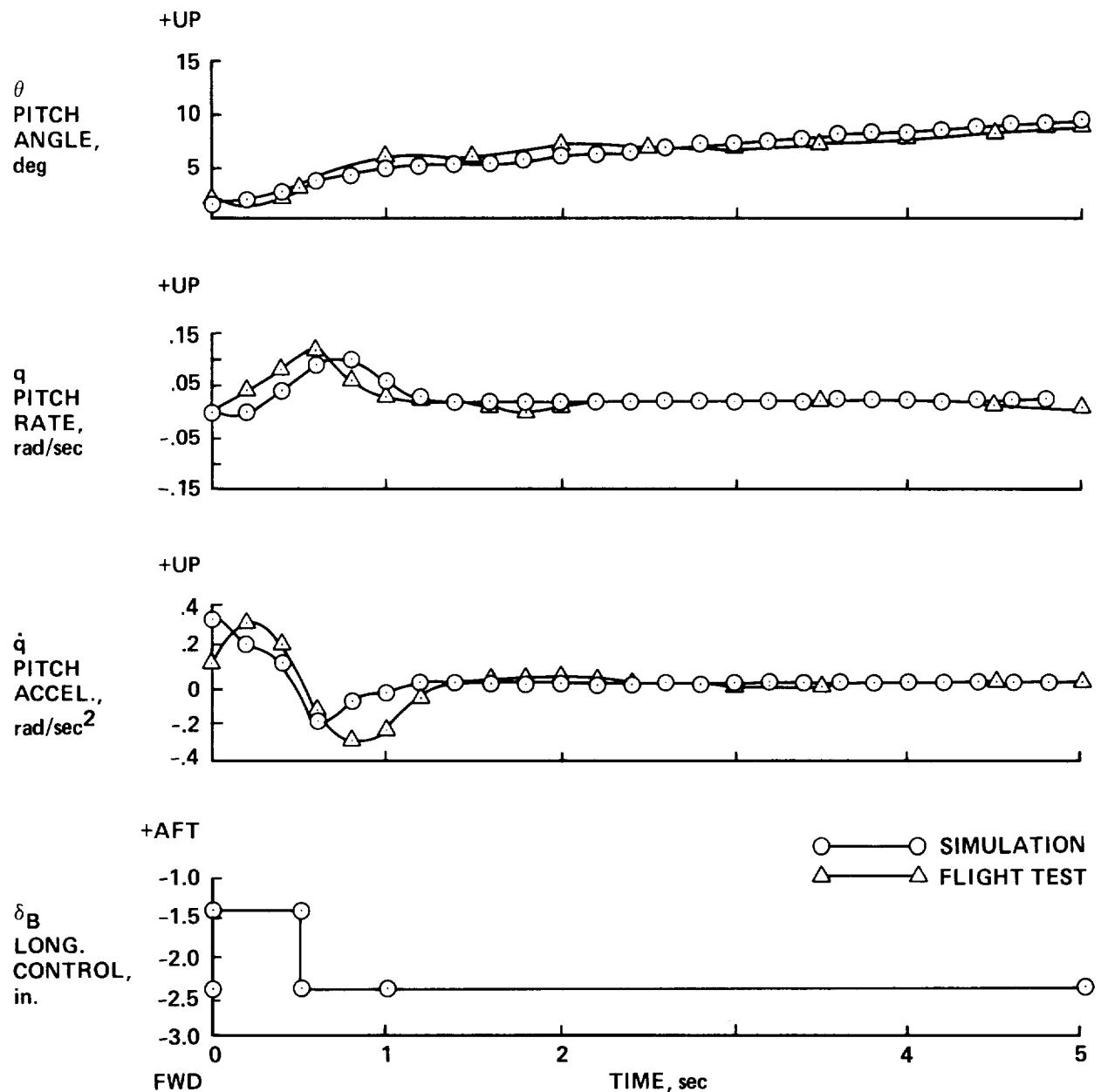


Figure 86.- BV simulation versus flight test dynamic response data (refs. 2,4),
 $V_{eq} = 127$ knots.

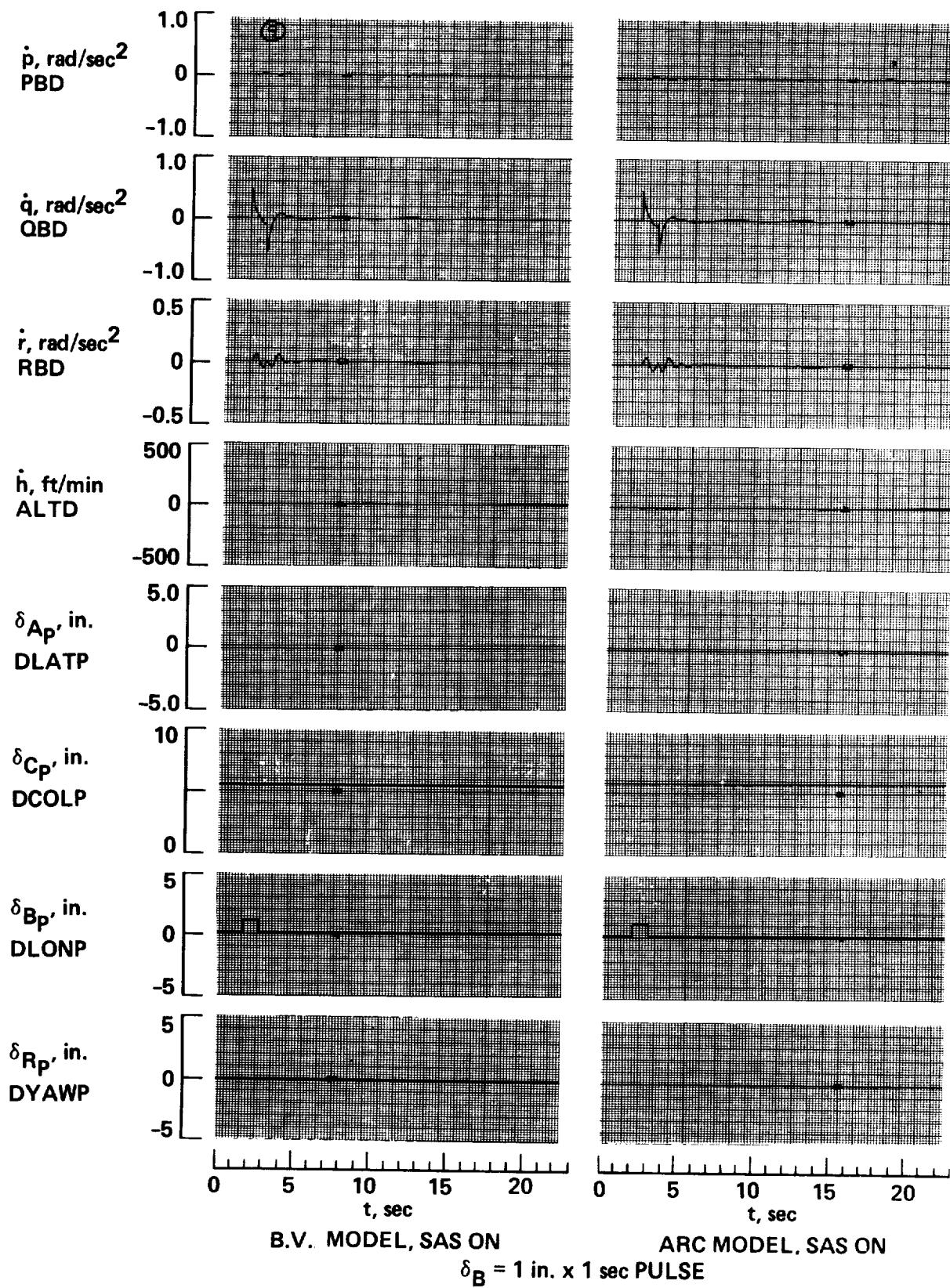


Figure 87.- BV versus ARC simulation response data, slung load attached; hover.

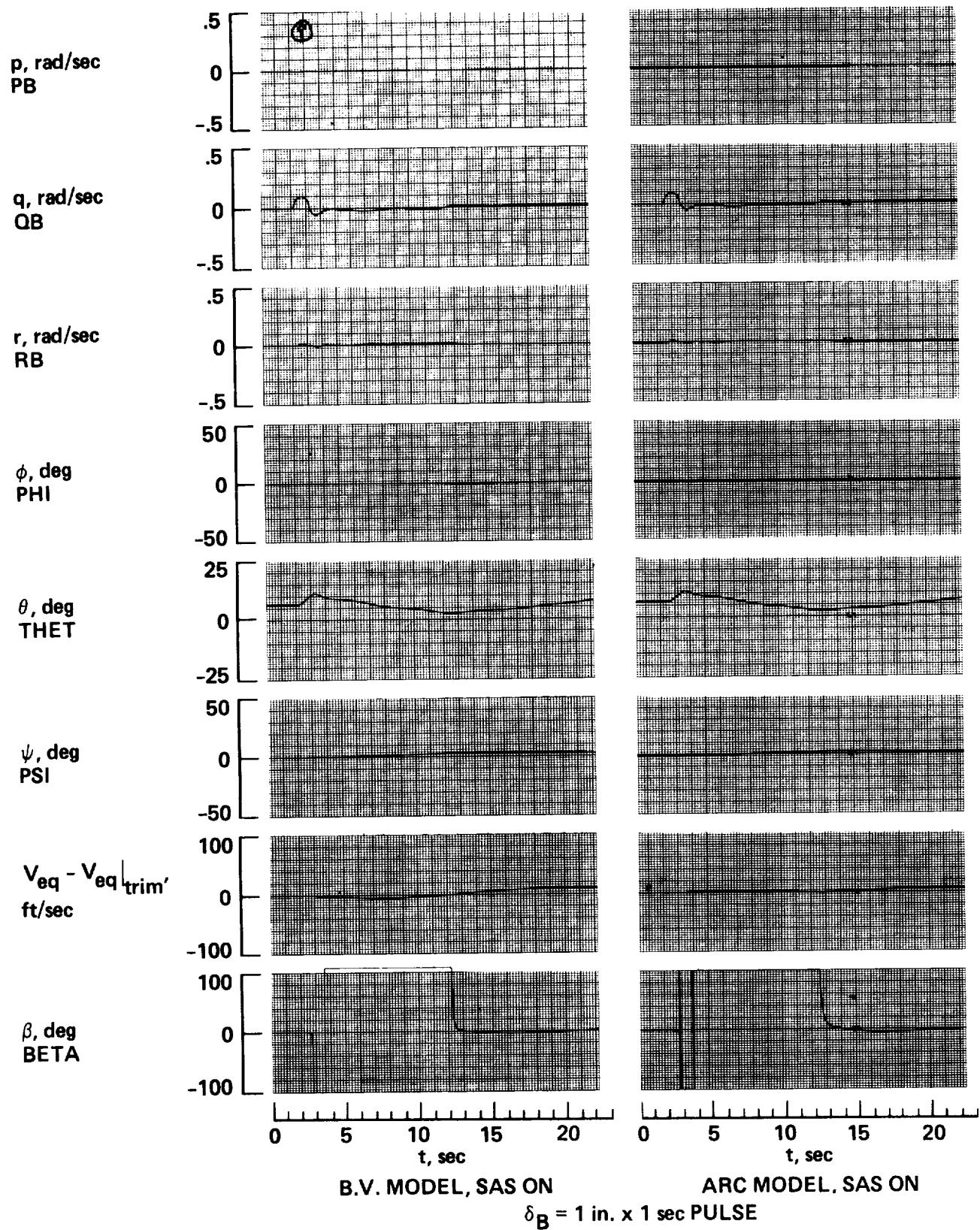


Figure 88.- BV versus ARC simulation response data, slung load attached; hover.

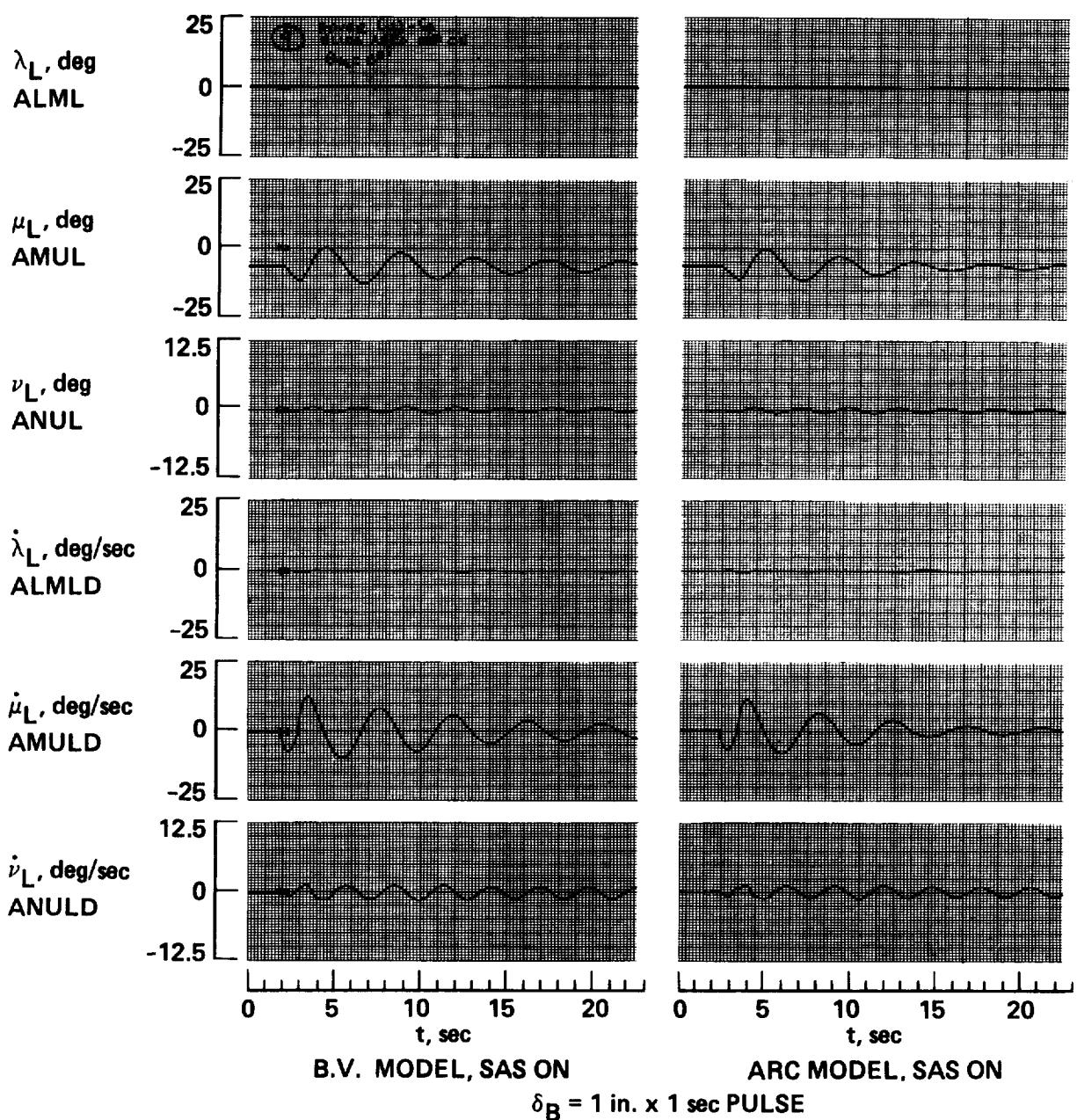


Figure 89.- BV versus ARC simulation response data, slung load attached; hover.

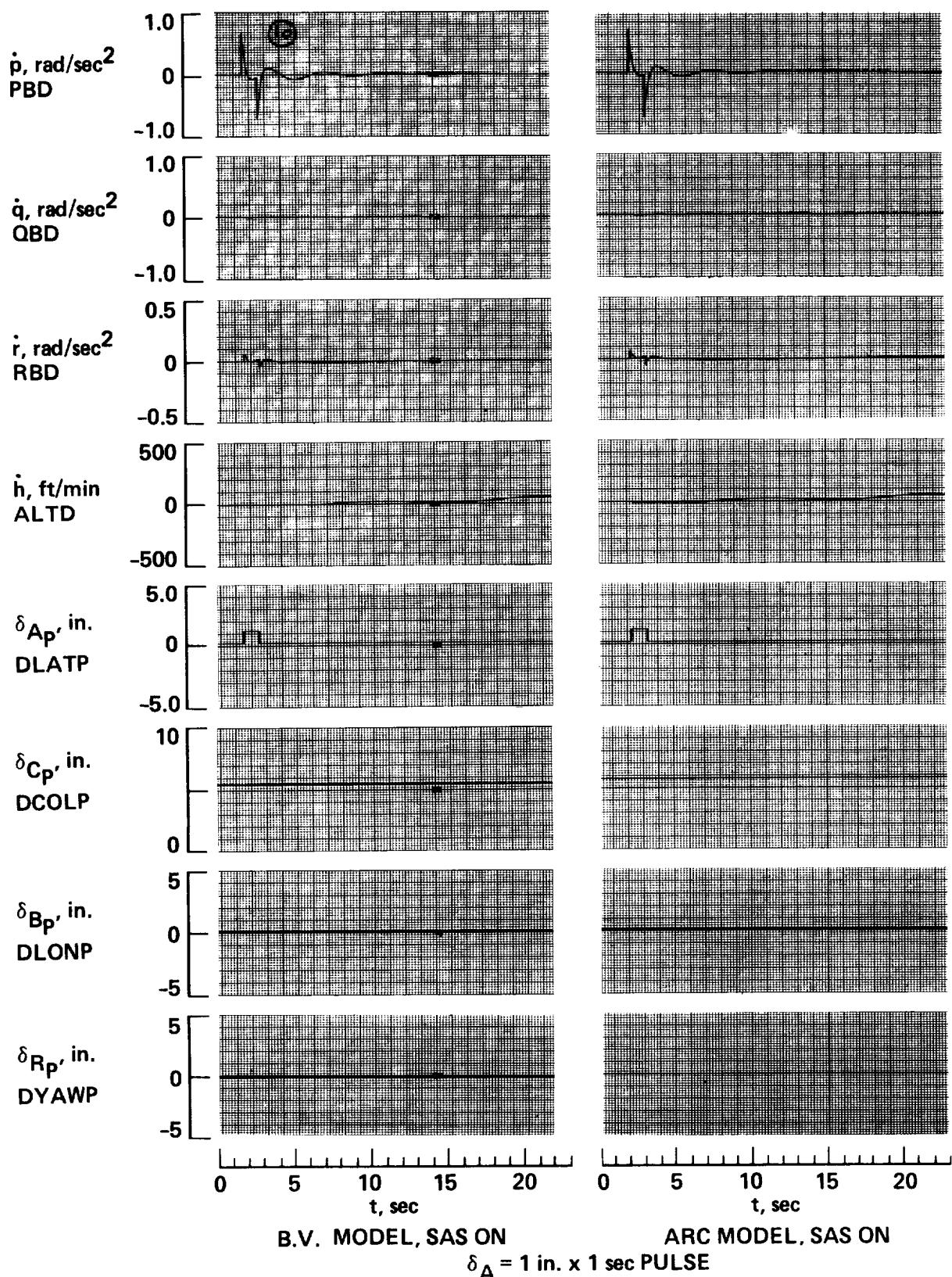


Figure 90.- BV versus ARC simulation response data, slung load attached; hover.

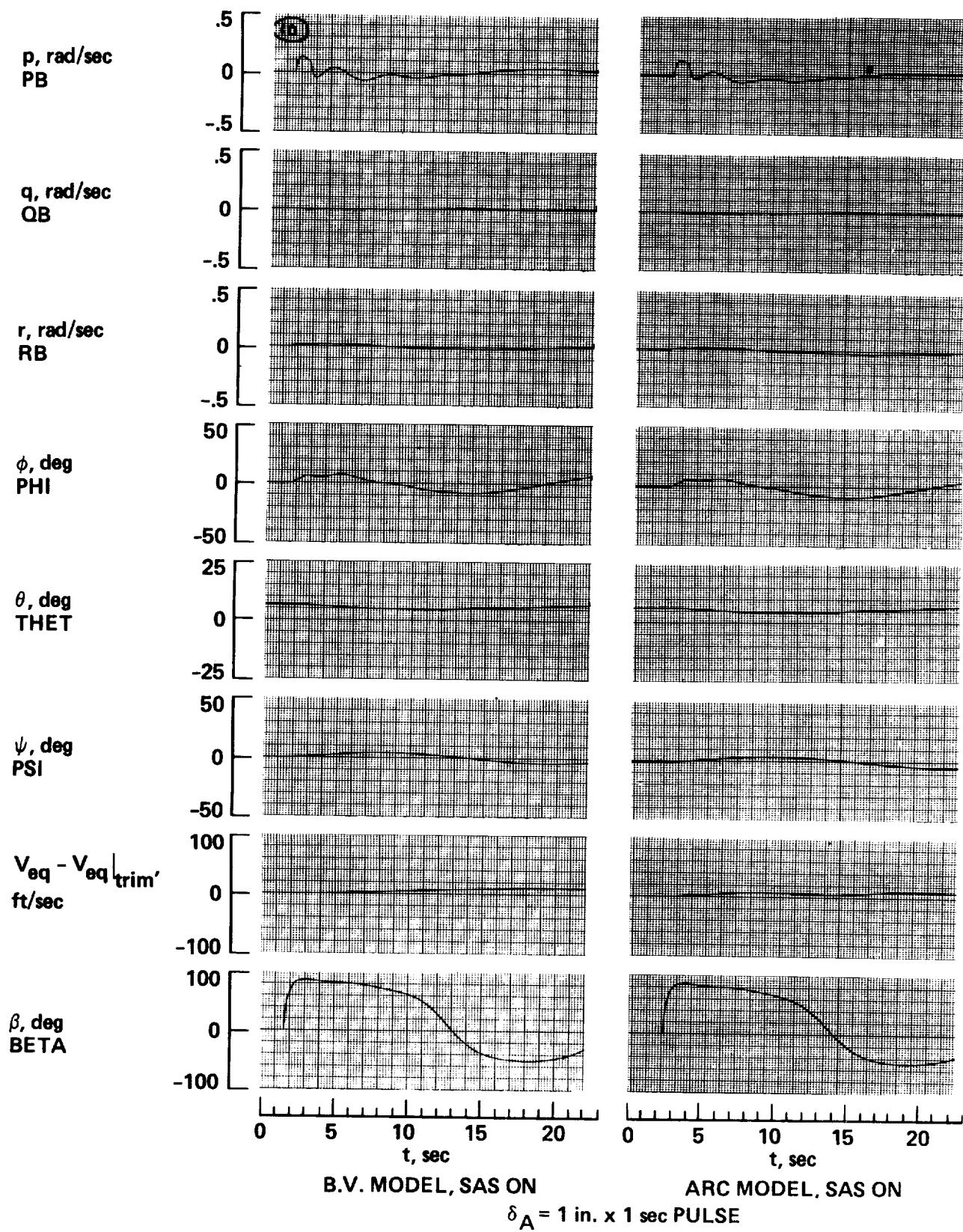


Figure 91.- BV versus ARC simulation response data, slung load attached; hover.

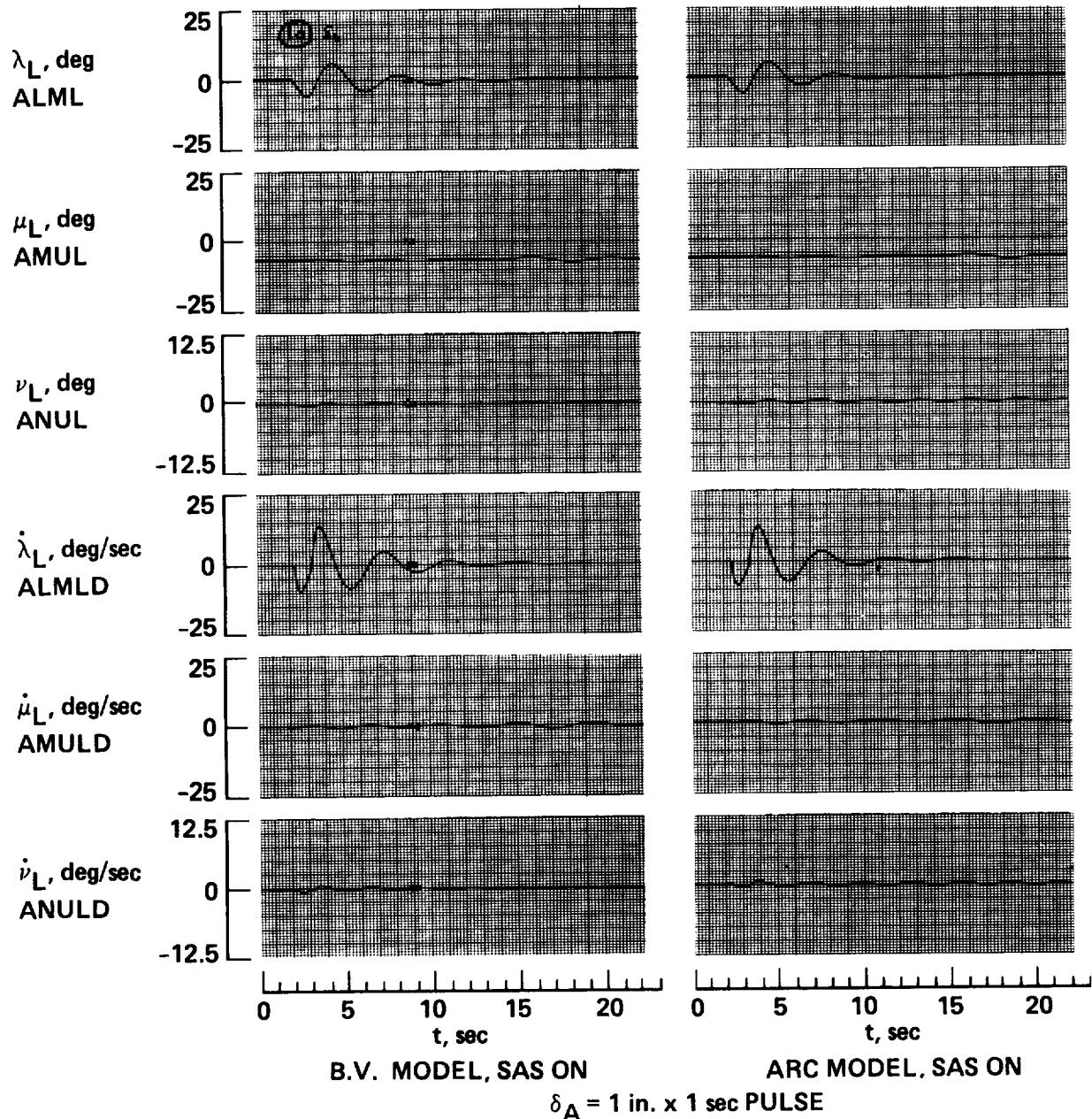


Figure 92.- BV versus ARC simulation response data, slung load attached; hover.

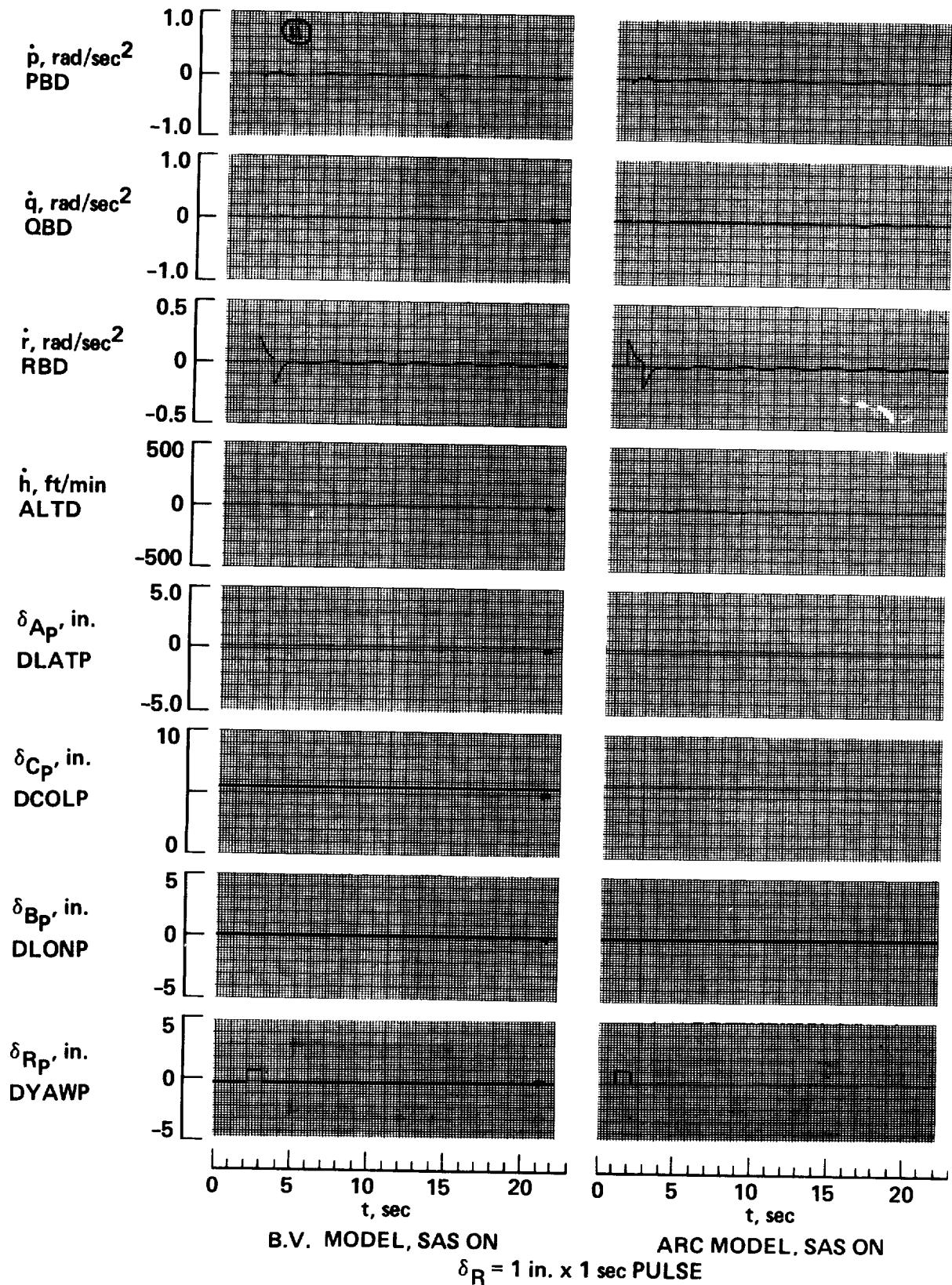


Figure 93.- BV versus ARC simulation response data, slung load attached; hover.

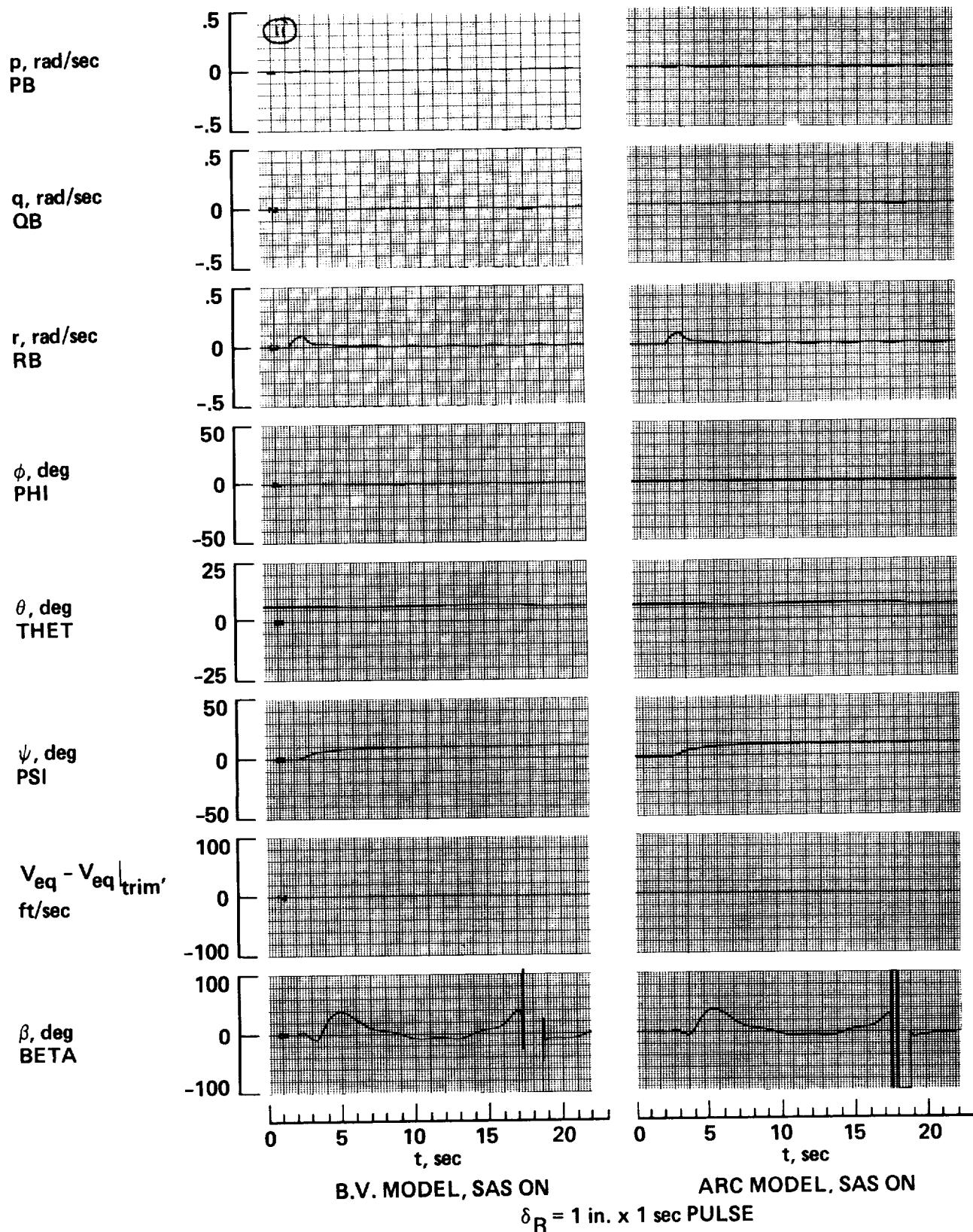


Figure 94.- BV versus ARC simulation response data, slung load attached; hover.

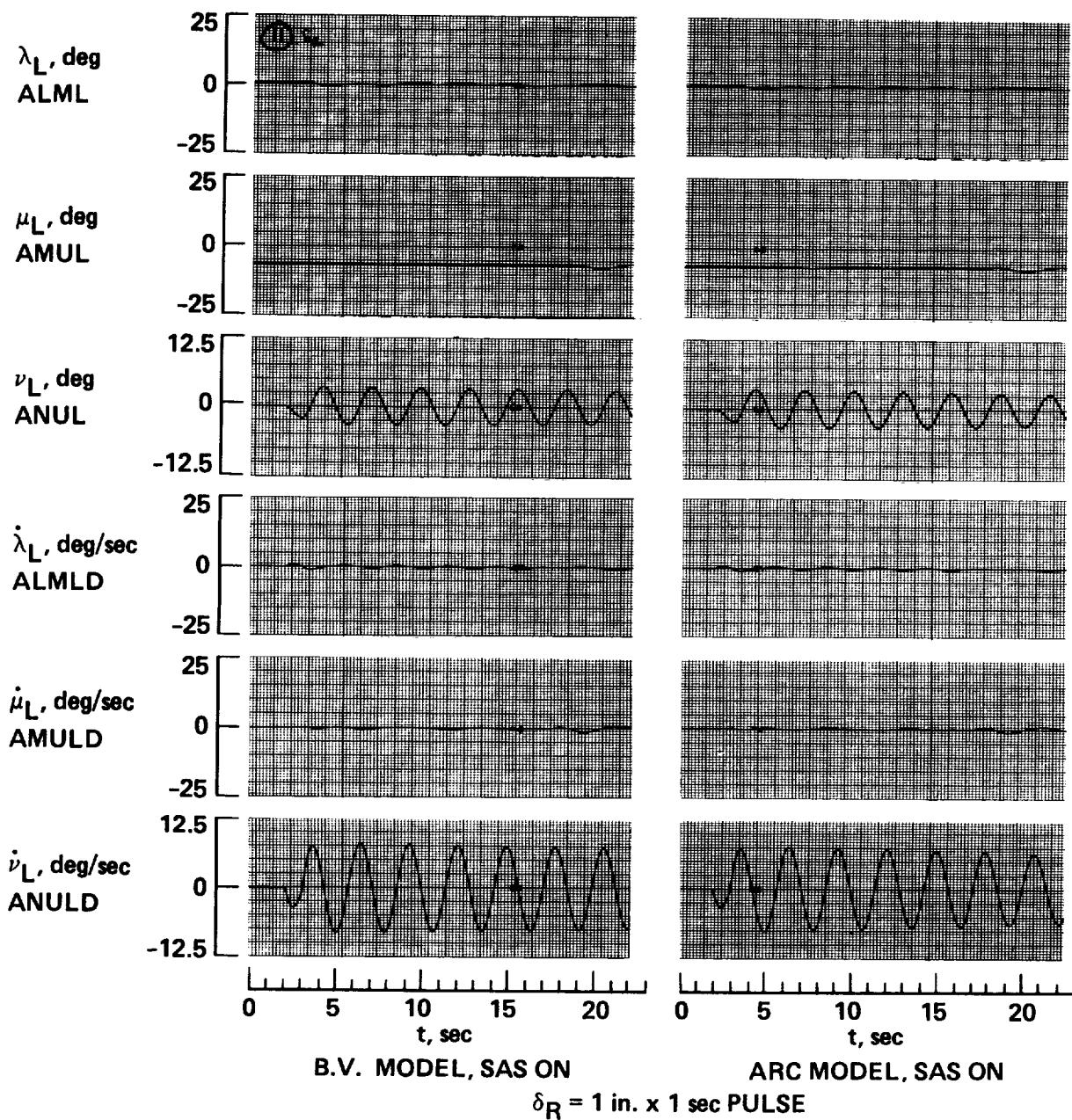


Figure 95.- BV versus ARC simulation response data, slung load attached; hover.

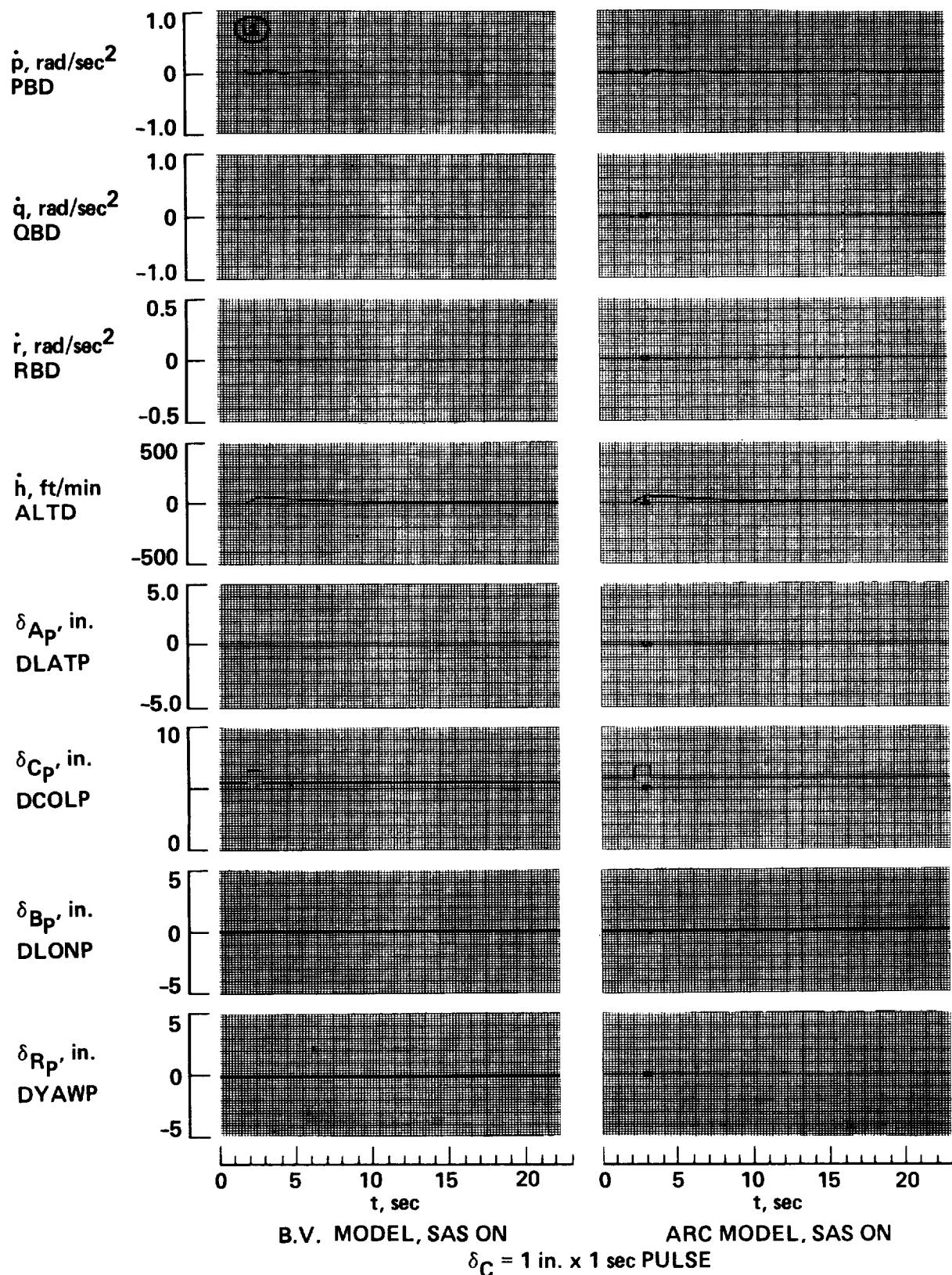


Figure 96.- BV versus ARC simulation response data, slung load attached; hover.

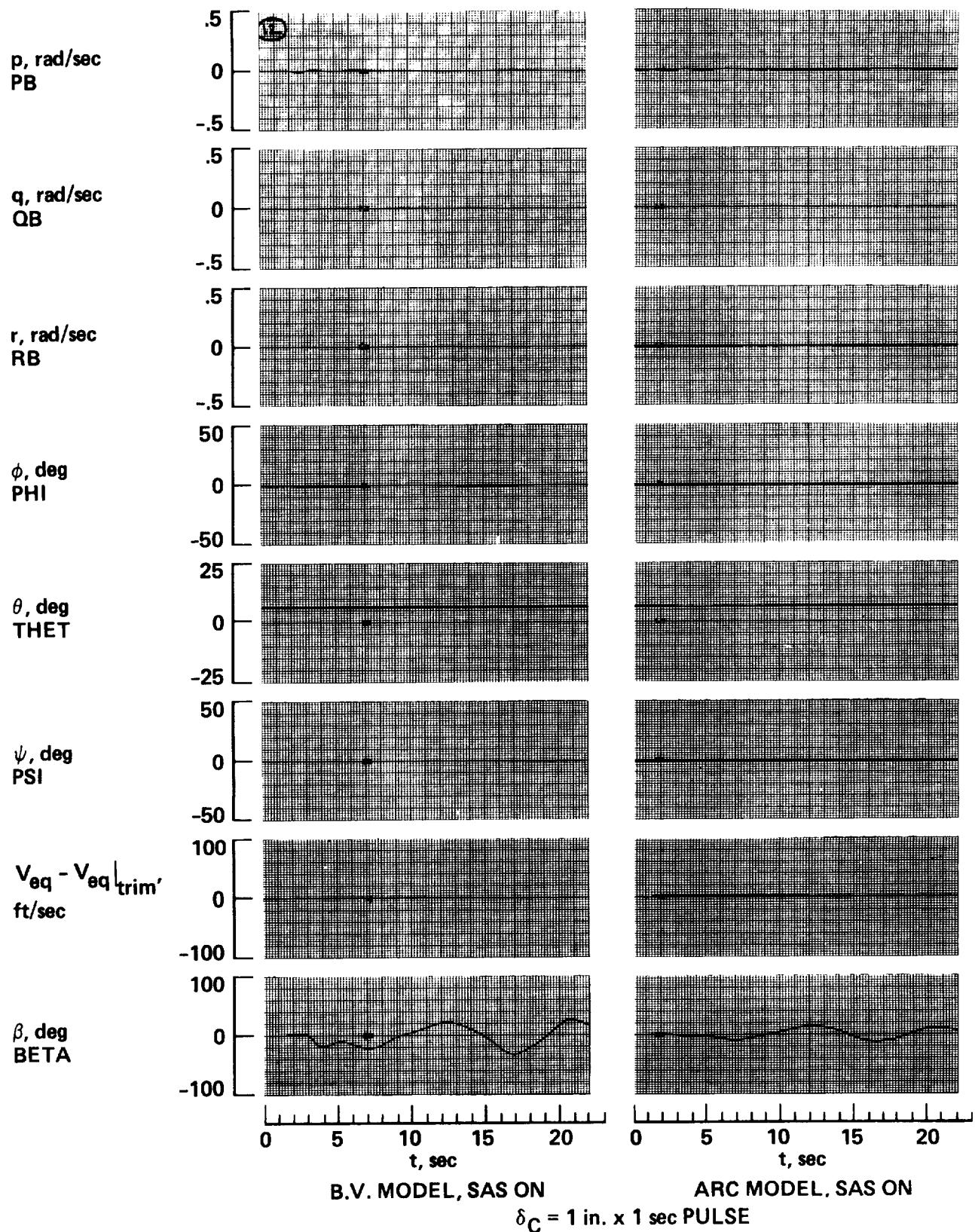


Figure 97.- BV versus ARC simulation response data, slung load attached; hover.

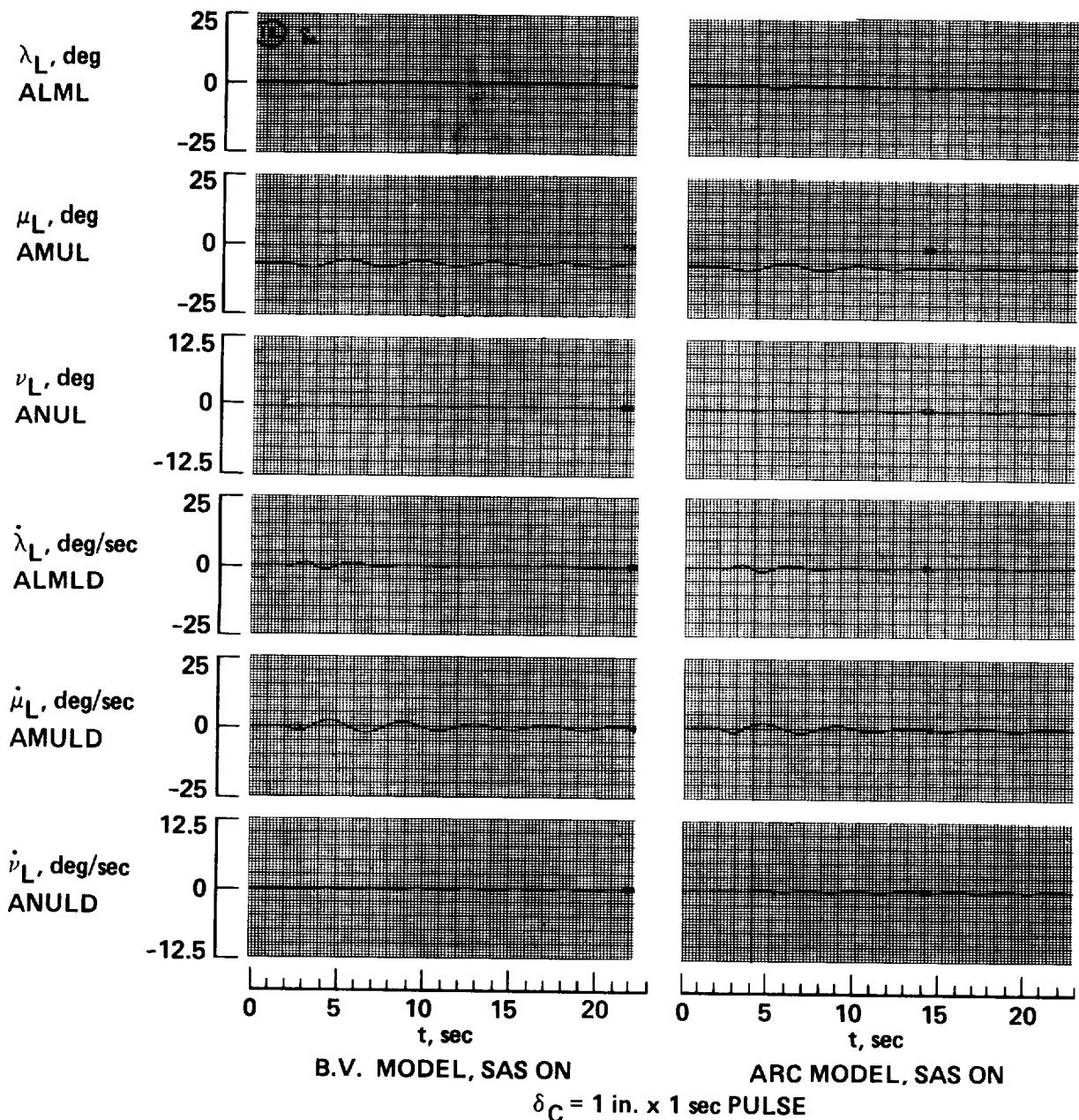


Figure 98.- BV versus ARC simulation response data, slung load attached; hover.

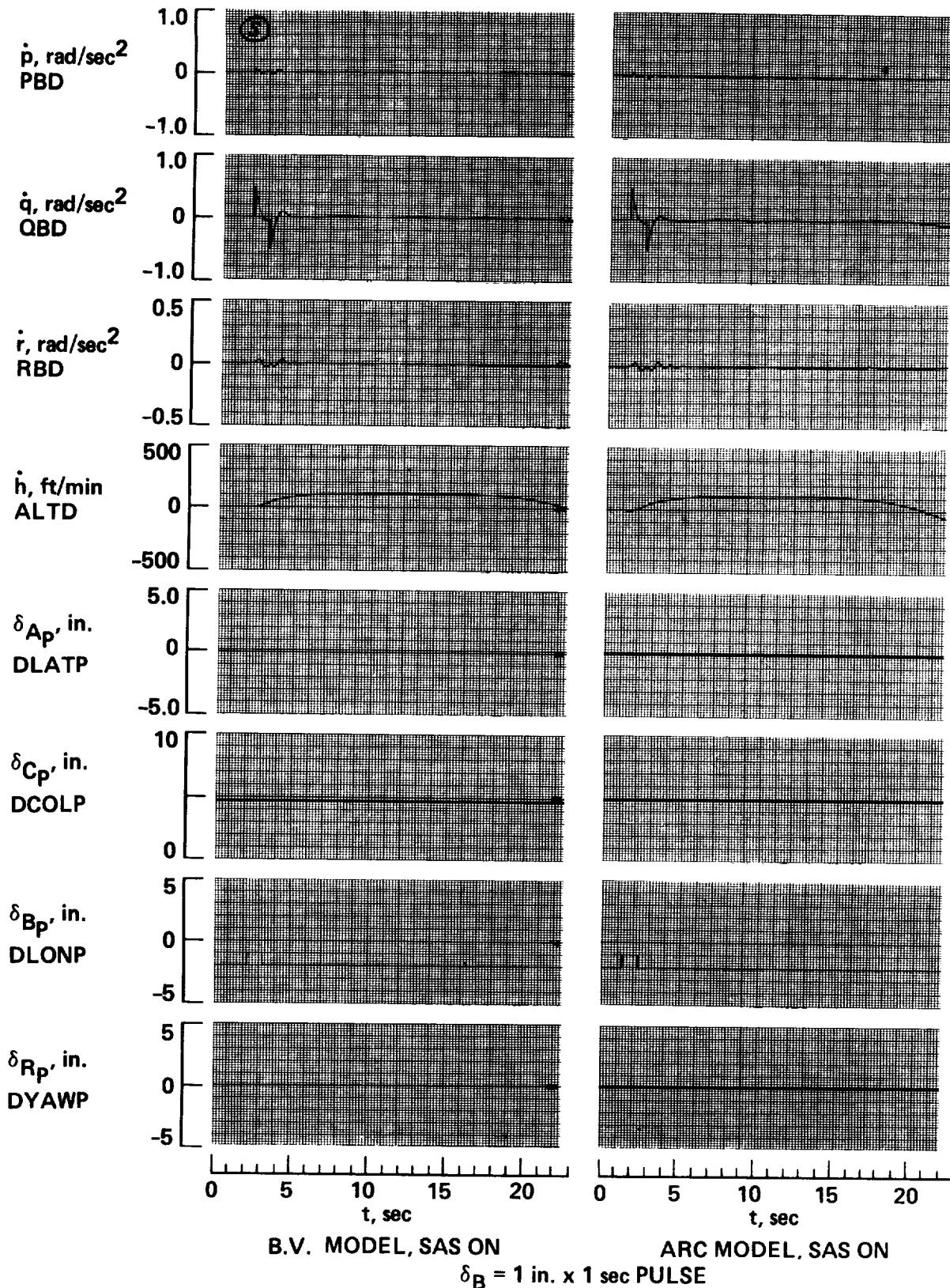


Figure 99.- BV versus ARC simulation response data, slung load attached; $V_{eq} = 75$ knots.

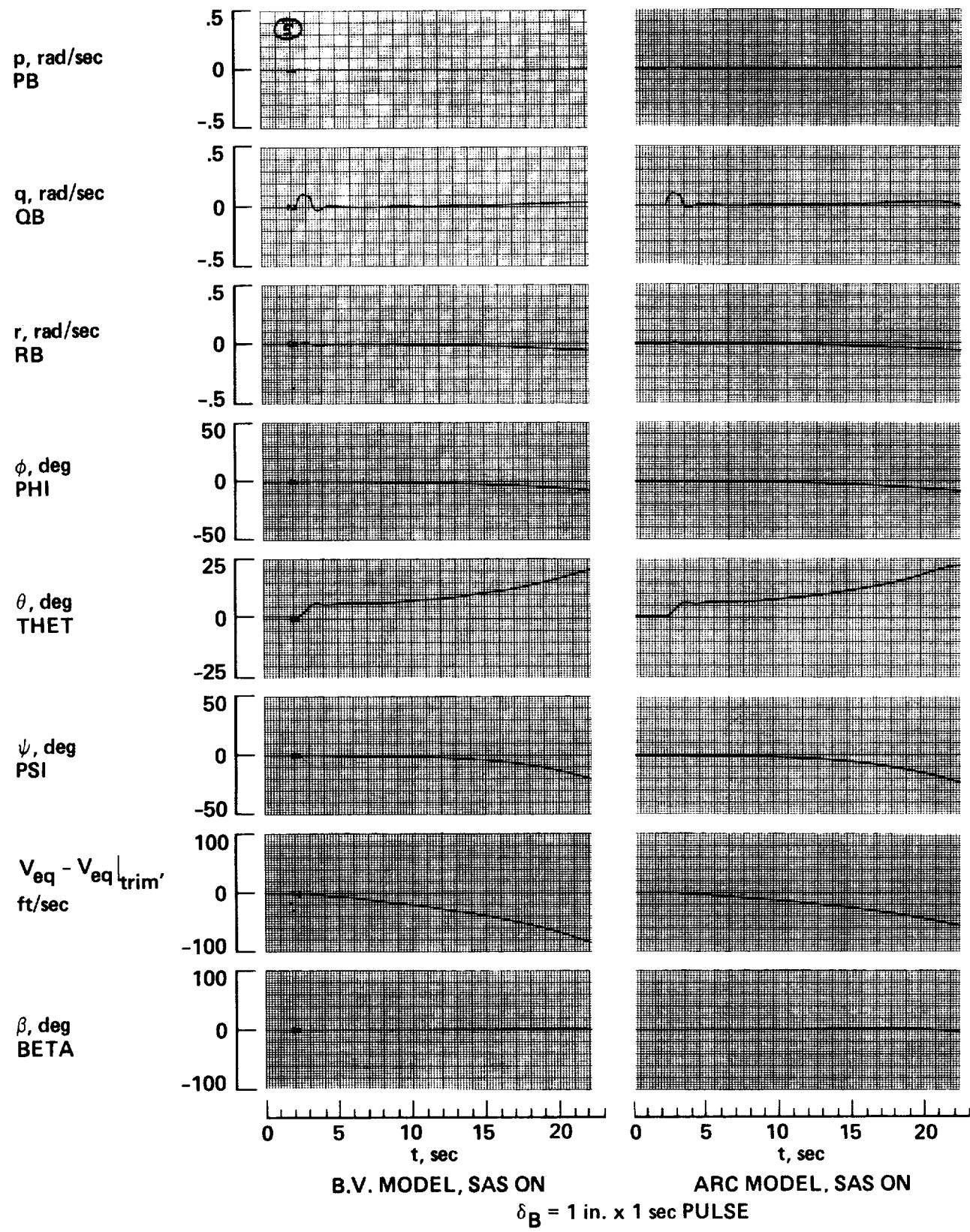


Figure 100.-- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

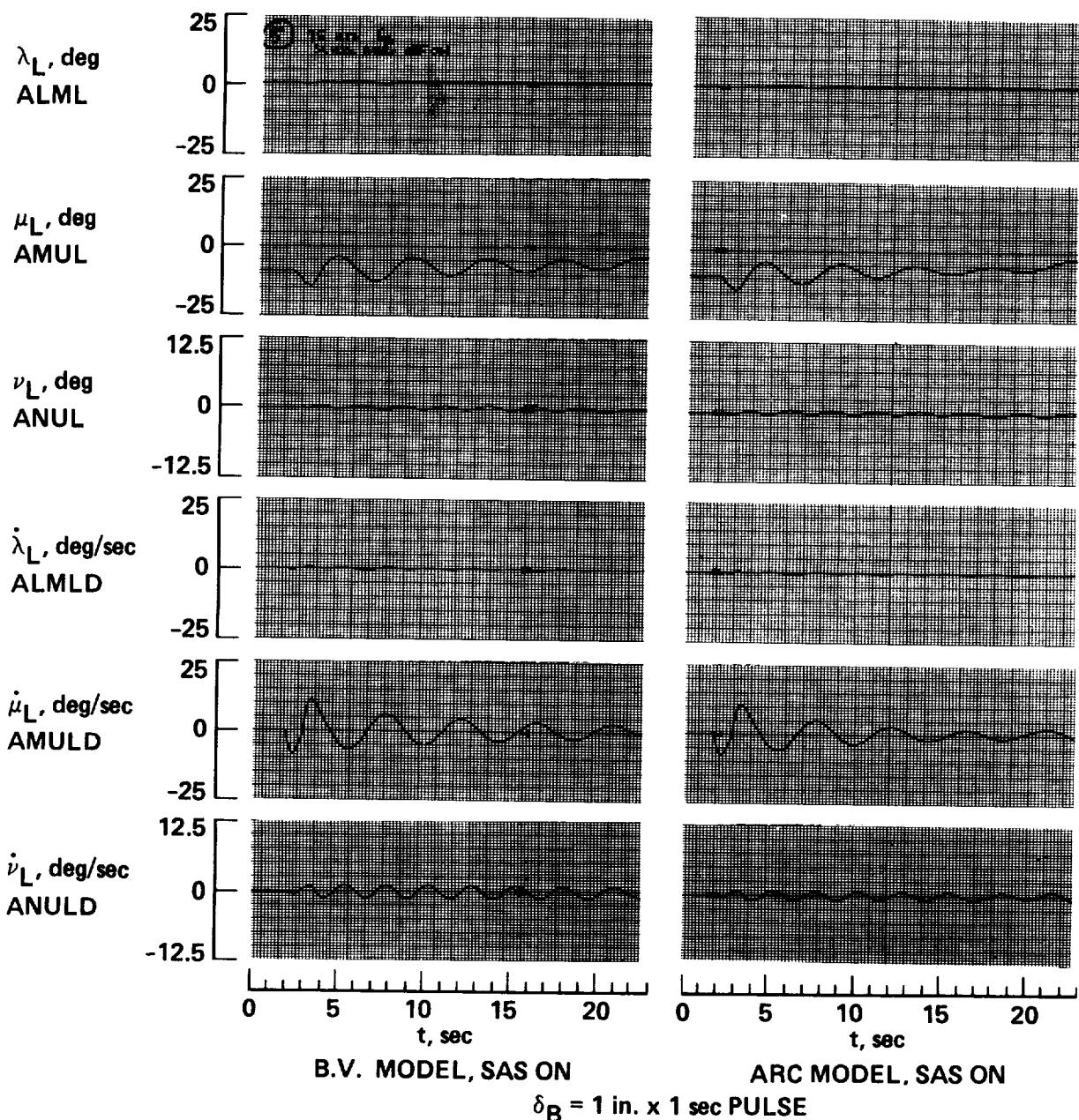


Figure 101.- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

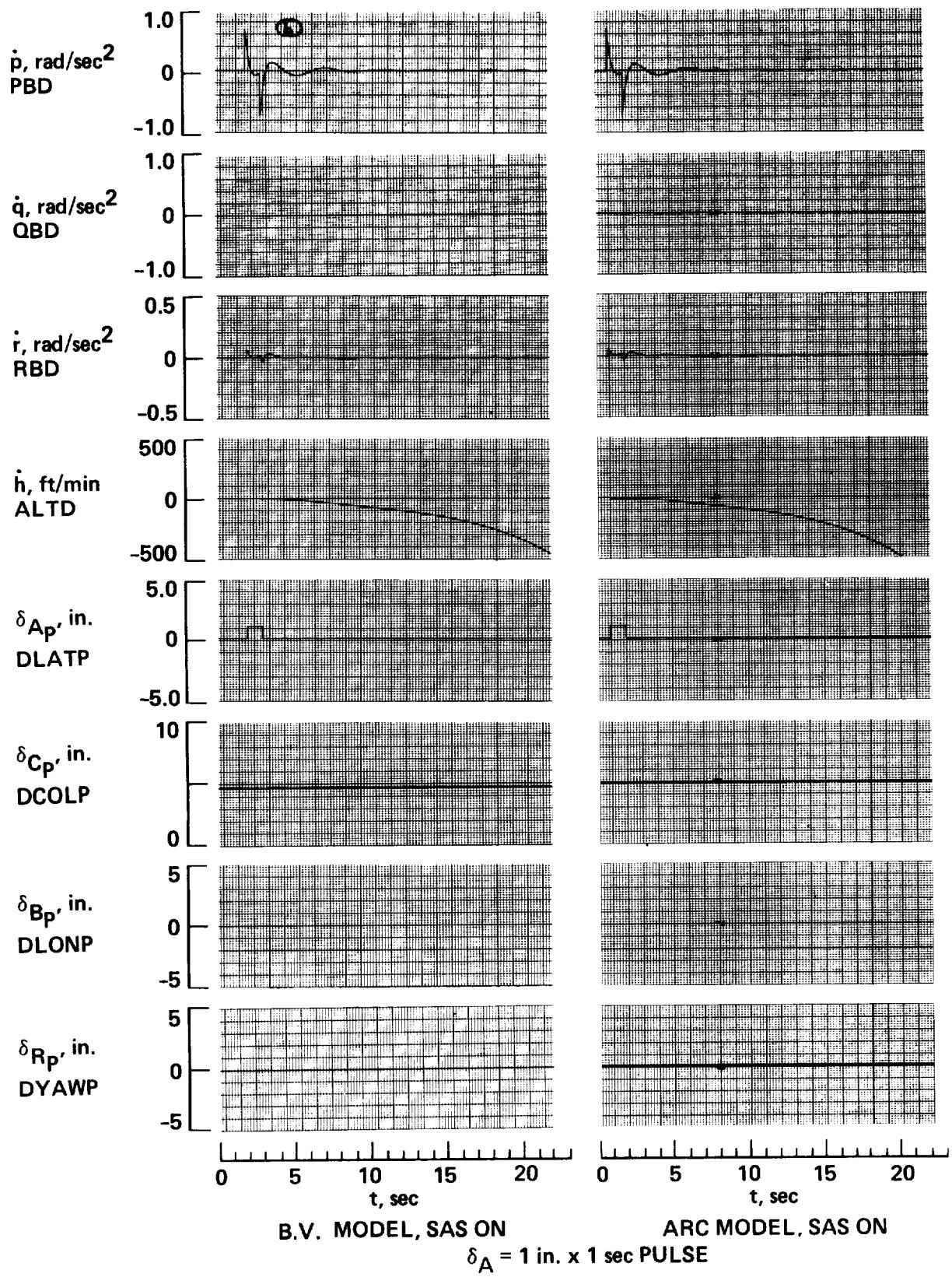


Figure 102.- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

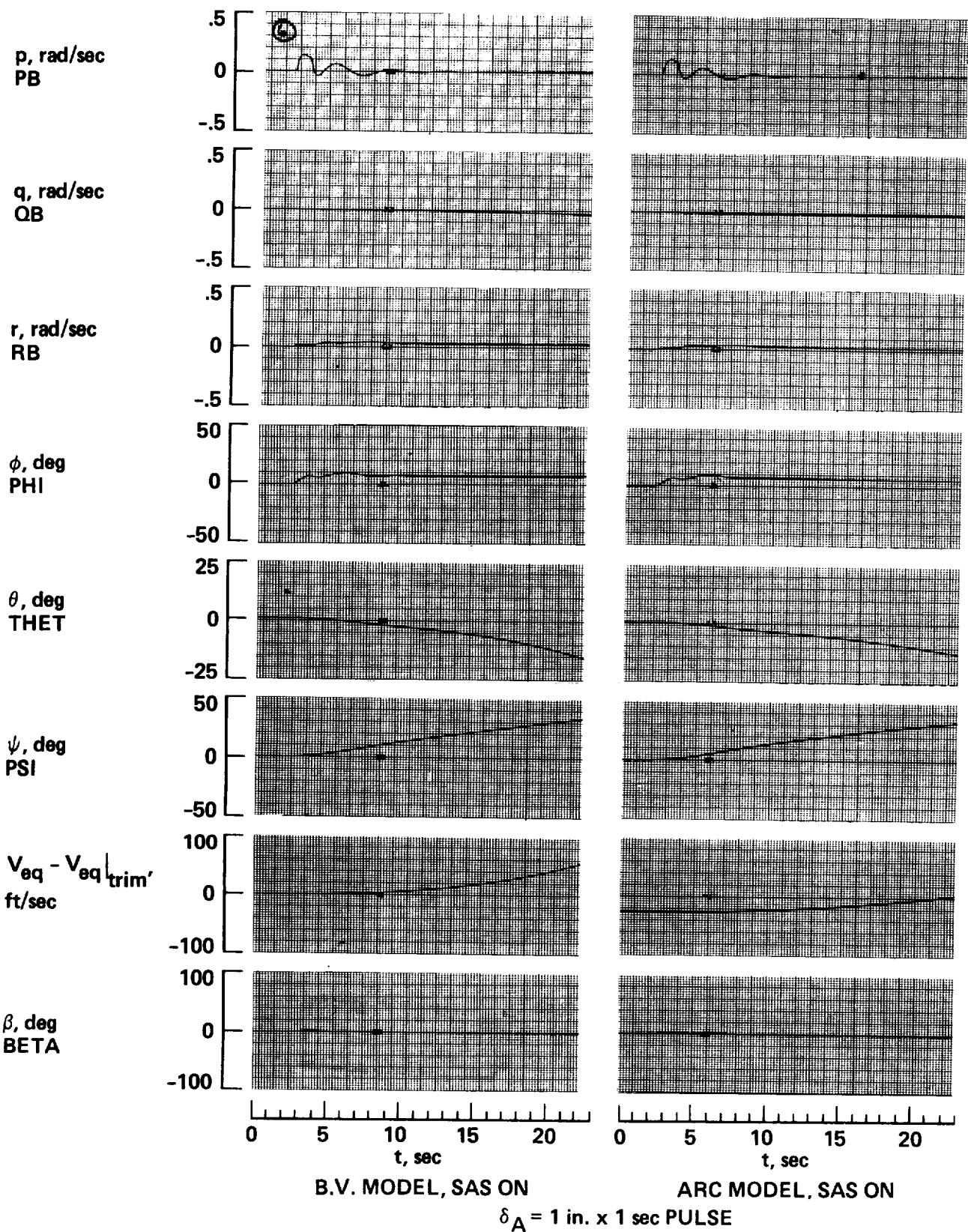


Figure 103.- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

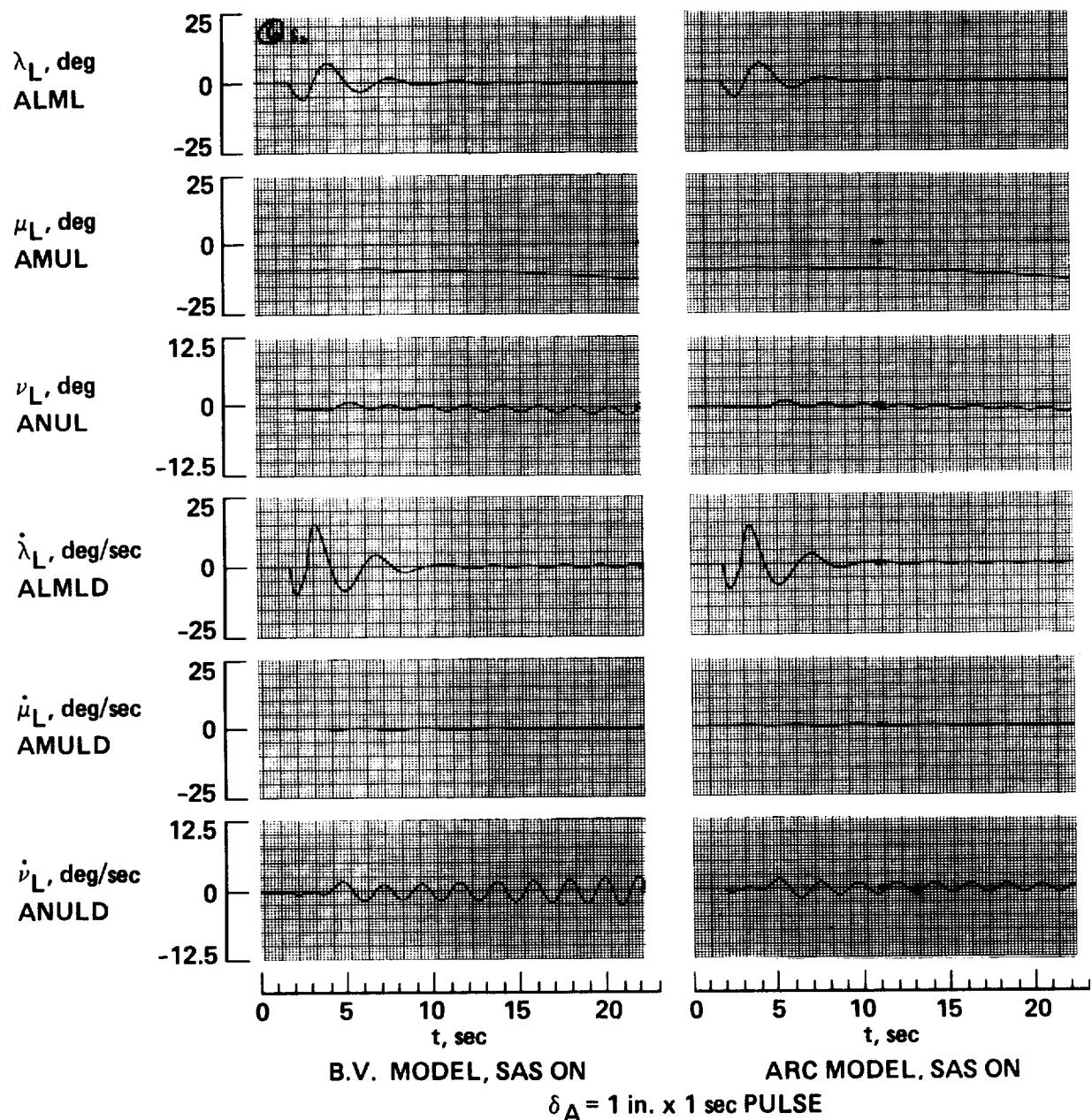


Figure 104.- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

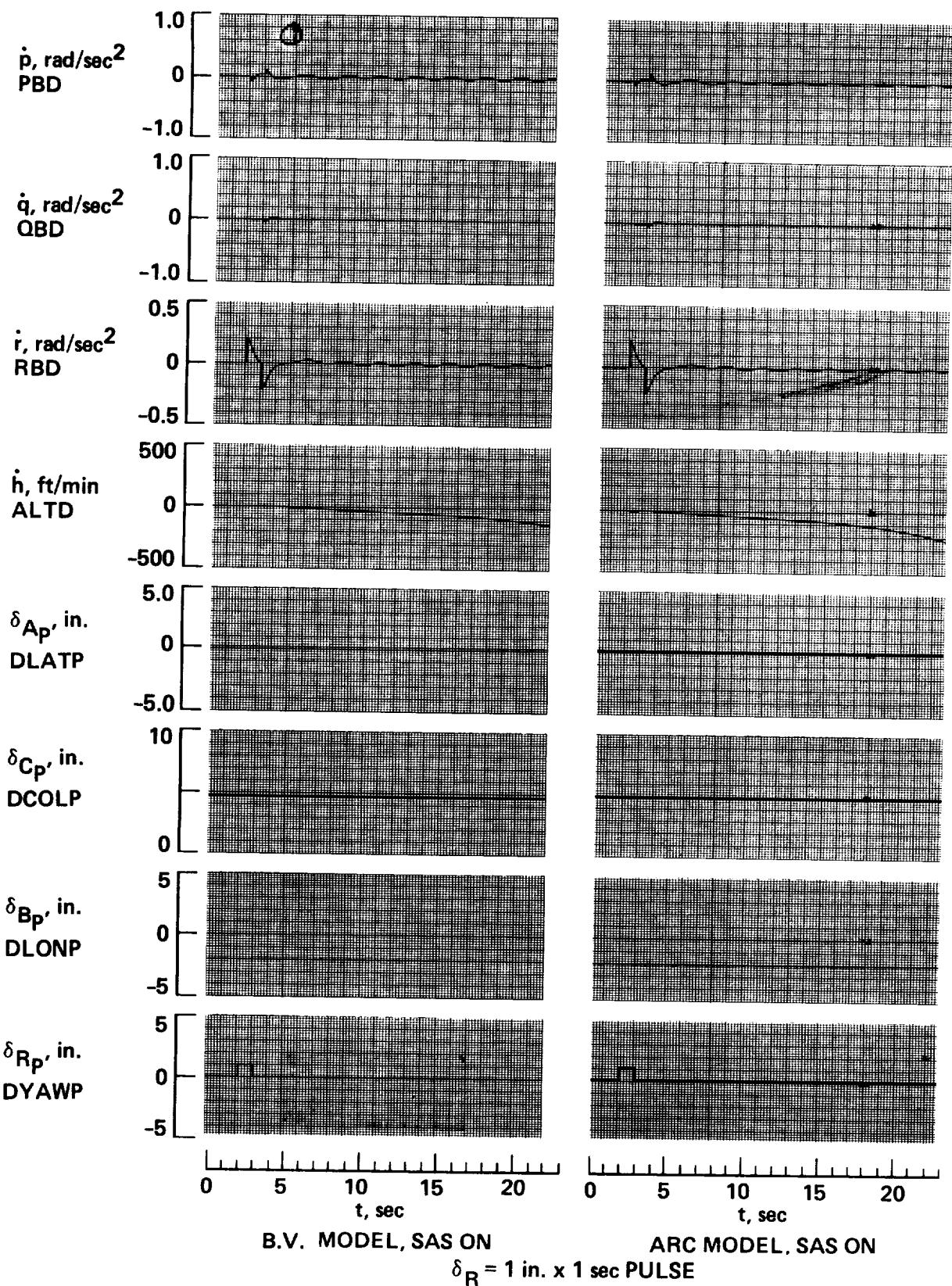


Figure 105.- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

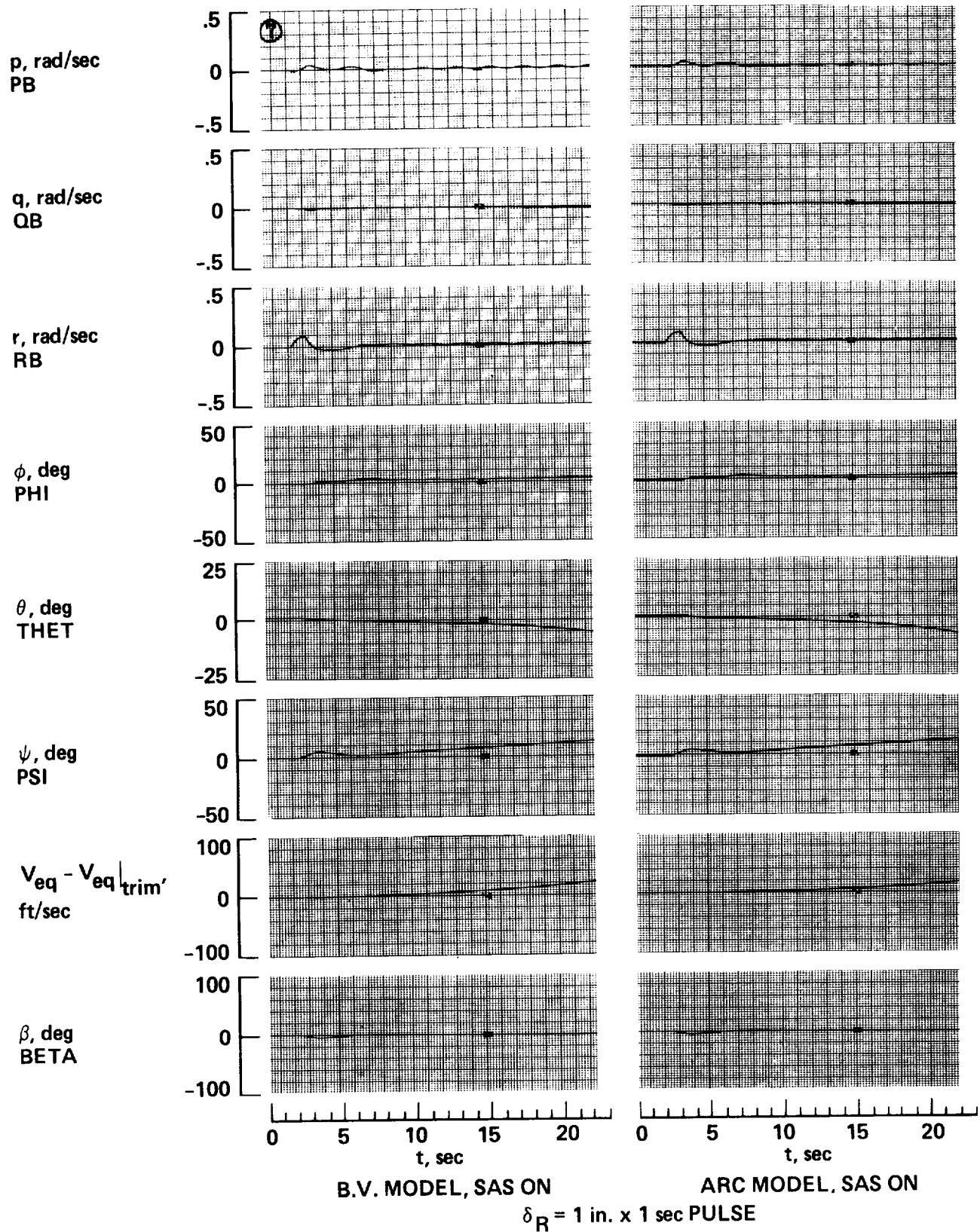


Figure 106.- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

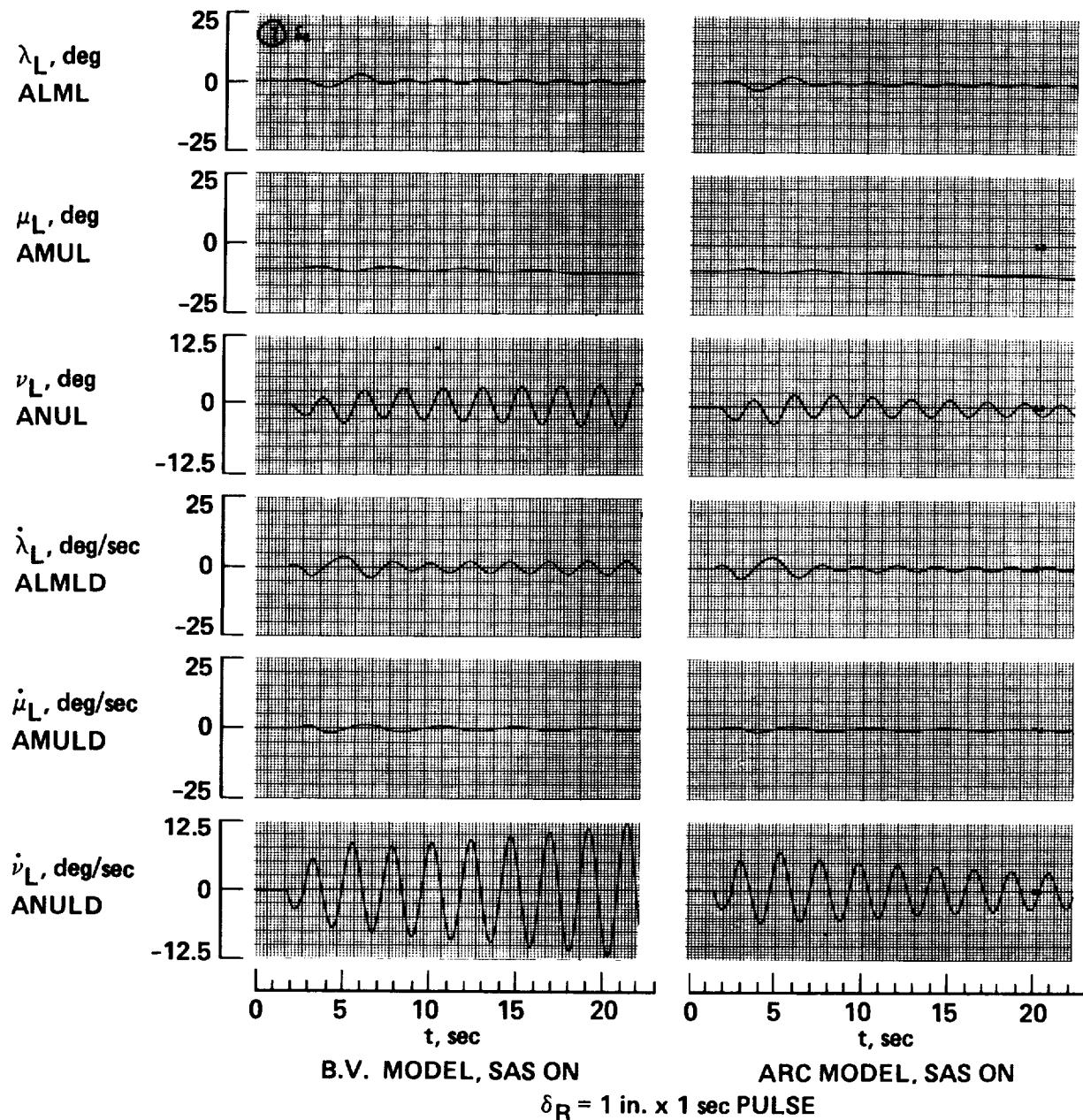


Figure 107.- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

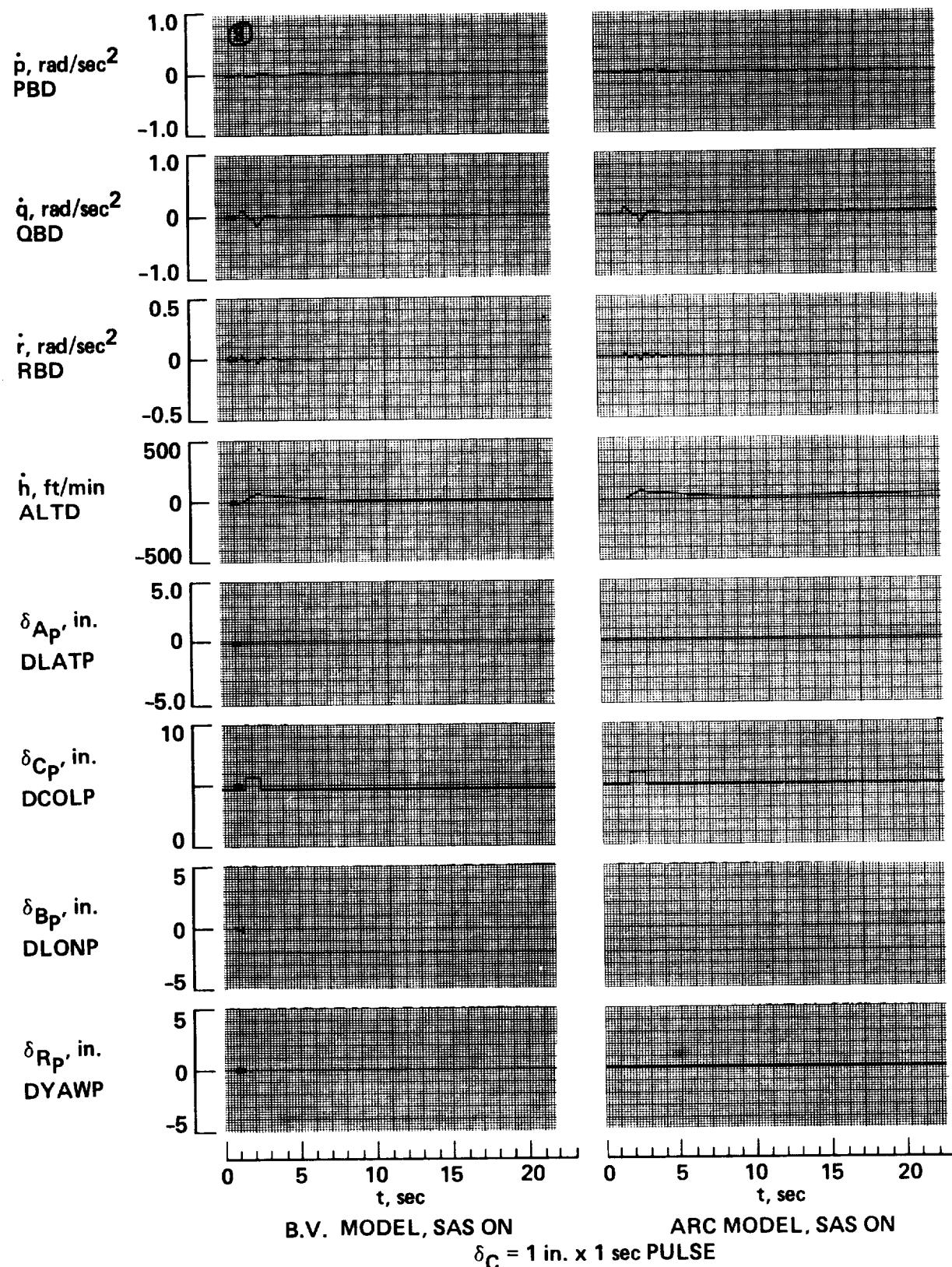


Figure 108.- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

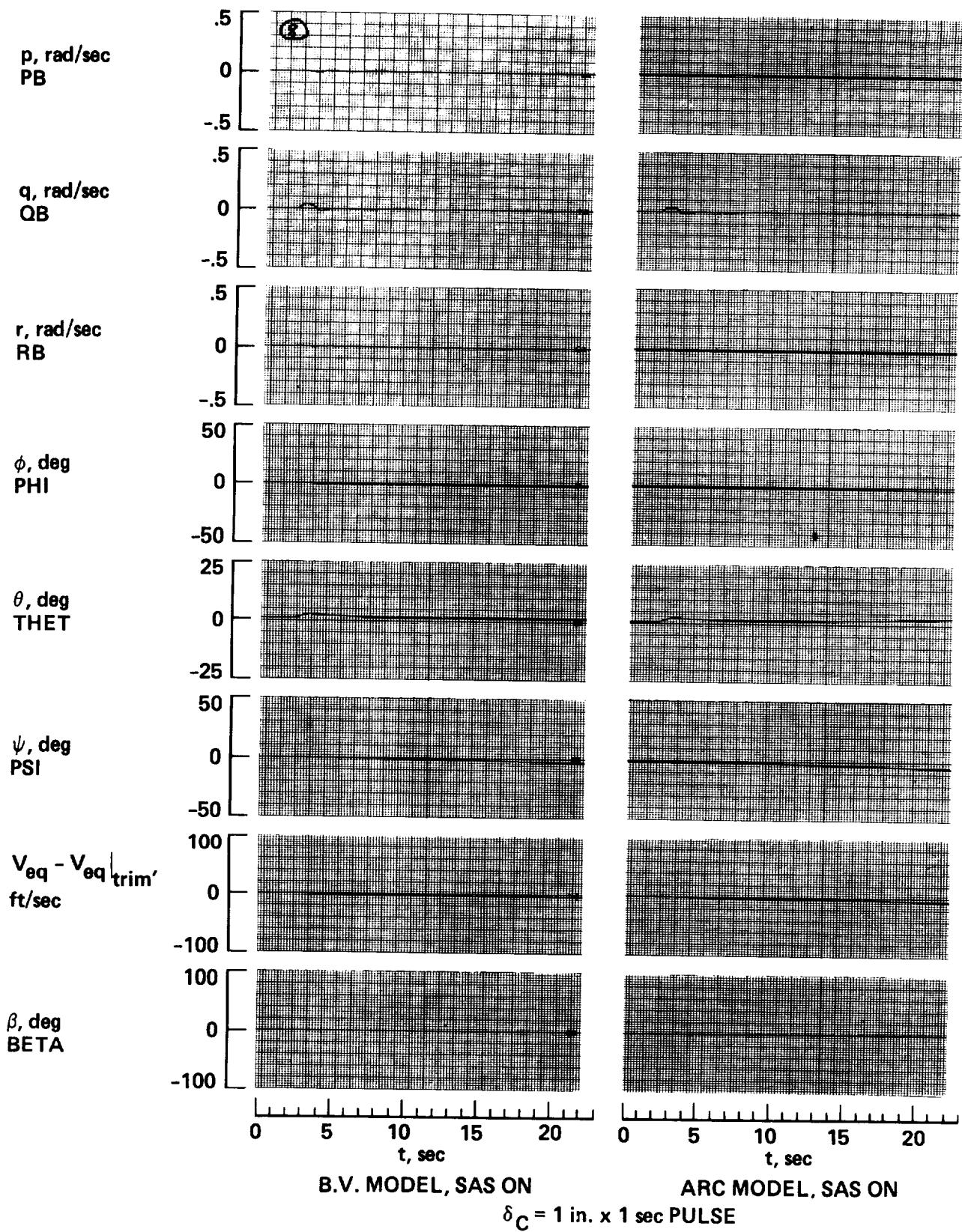


Figure 109.- BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

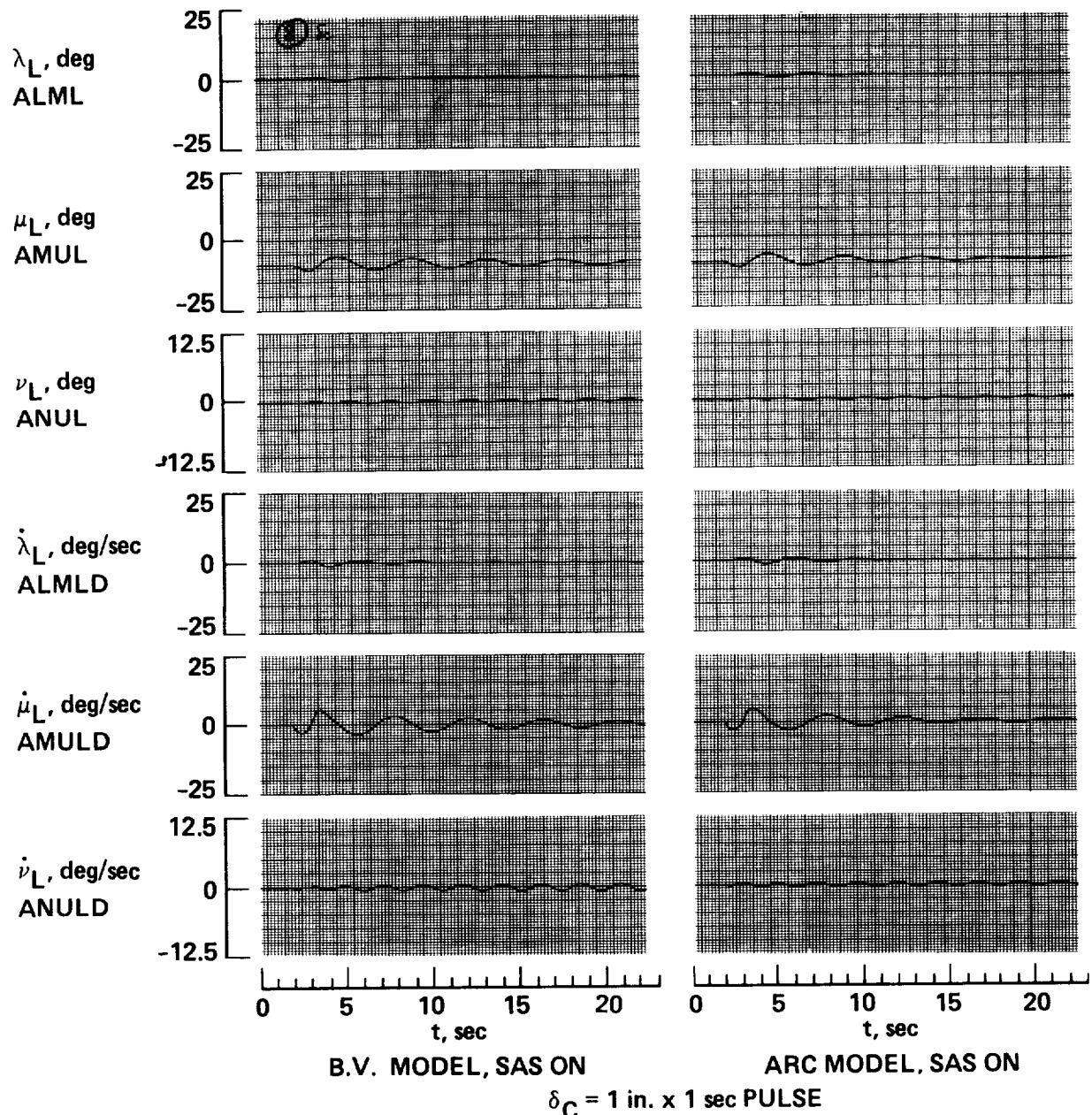


Figure 110.— BV versus ARC simulation response data, slung load attached;
 $V_{eq} = 75$ knots.

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16. Abstract A nonlinear simulation model of the CH-47B helicopter, developed by the Boeing Vertol Company (ref. 1), has been adapted for use in the NASA Ames Research Center (ARC) simulation facility. The model represents the specific configuration of the ARC variable stability CH-47B helicopter (fig. 1) and will be used in ground simulation research and to expedite and verify flight experiment design. Modeling of the helicopter uses a total force approach in six rigid body degrees of freedom. Rotor dynamics are simulated using the Wheatley-Bailey equations, including steady-state flapping dynamics. Also included in the model is the option for simulation of external suspension, slung-load equations of motion. Validation of the model (discussed in Volume II of this report) has been accomplished using static and dynamic data from the original Boeing Vertol mathematical model and flight test data from references 2 and 3, as reproduced in reference 4. The model is appropriate for use in real-time piloted simulation and is implemented on the ARC Sigma IX computer where it may be operated with a digital cycle time of 0.03 sec.			
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